

# Slab Rolling on a Rolling Cylinder

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## 1 Problem

Discuss the motion of a “slab” that rolls without slipping on a “cylinder”, when the latter rolls without slipping on a horizontal plane.<sup>1</sup>

*This problem was suggested by Alexandre Tort. For the related case of one cylinder on/inside another, see [1, 2]. For the case of a sphere on a fixed cylinder, see pp. 212-214 of [3].<sup>2</sup>*

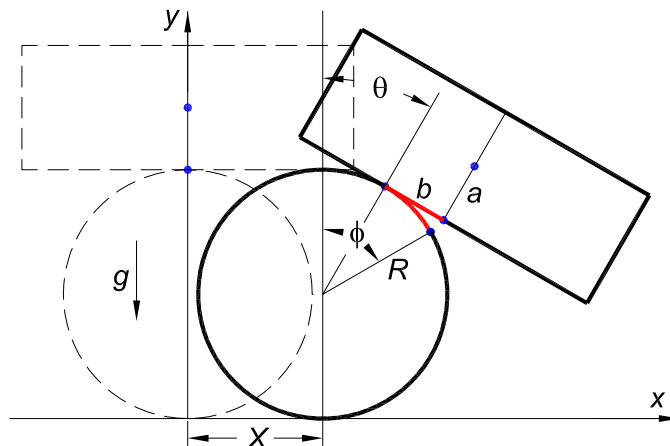
## 2 Solution

We will use a Lagrangian approach.

### 2.1 Coordinates and Constraints

When the slab, of thickness  $2a$ , mass  $m$  and moment of inertia  $kma^2$ , is directly above the cylinder, of radius  $R$ , mass  $M$  and moment of inertia  $KMR^2$ , and centered upon it, we define the line of contact of the cylinder with the horizontal plane to be the  $z$ -axis, at  $x = y = 0$ . Then, the condition of rolling without slipping for the cylinder is that when it has rolled (positive) distance  $X$ , the initial line of contact has rotated through angle  $\phi = X/R$ , clockwise with respect to the vertical, as shown in the figure below. This rolling constraint can be written as,

$$X = R\phi. \tag{1}$$



<sup>1</sup>Either the “slab” or the “cylinder” (but not both) could have a very large moment of inertia if it is in the form of a “bobbin” with flanges that extend beyond the supporting surface.

<sup>2</sup>The author’s interest in such problems was inspired in part by Bob Dylan: “It balances on your head just like a mattress balances on a bottle of wine.” (Leopardskin Pill-Box Hat, 1966).

If the slab rolls without slipping such that a line (in the  $x$ - $y$  plane) from the center of the cylinder to the point of contact with the slab angle  $\theta$  (positive clockwise) to the vertical, then the initial point of contact of the slab is at distance  $b$  from the original point, and the initial point of contact of the cylinder has rotated by angle  $\phi$ . The second rolling constraint is that distance  $b$  on the slab equals arc length  $R(\phi - \theta)$  on the cylinder,

$$b = R(\phi - \theta). \quad (2)$$

The vertical center of the cylinder is at  $Y = R$ , and the center of the slab is at,

$$x = X + (a + R) \sin \theta + R(\phi - \theta) \cos \theta, \quad y = R + (a + R) \cos \theta - R(\phi - \theta) \sin \theta. \quad (3)$$

Altogether there are 4 constraints on the 6 degree of freedom ( $x, y, X, Y, \phi, \theta$ ), of the two-dimensional motion of the system, such that there are only two independent degrees of freedom, which we take to be the angles  $\phi$  and  $\theta$ .

## 2.2 Energy

The total energy  $E = T + V$  is conserved, where the potential energy  $V$  (taken to be zero when  $\phi = \phi_0$  and  $\theta = \theta_0$ ),

$$V = mg(y - y_0) = mg\{(a + R)(\cos \theta - \cos \theta_0) - R[(\phi - \theta) \sin \theta - (\phi_0 - \theta_0) \sin \theta_0]\}, \quad (4)$$

depends on both coordinates  $\phi$  and  $\theta$ .<sup>3</sup>

The kinetic energy of cylinder, whose axis is at  $(X, Y)$ , is,

$$T_{\text{cyl}} = \frac{M\dot{X}^2}{2} + \frac{I_{\text{cyl}}\dot{\phi}^2}{2} = \frac{1 + K}{2}MR^2\dot{\phi}^2, \quad (5)$$

using the rolling constraint (1) and the expression  $I_{\text{cyl}} = KMR^2$  for the moment of inertia  $I_{\text{cyl}}$  in terms of parameter  $K$ .

The kinetic energy of the slab, whose axis is at  $(x, y)$ , is, using  $I_{\text{slab}} = kma^2$ ,

$$T_{\text{slab}} = \frac{m(\dot{x}^2 + \dot{y}^2)}{2} + \frac{I_{\text{slab}}\dot{\theta}^2}{2} = \frac{m(\dot{x}^2 + \dot{y}^2)}{2} + \frac{kma^2\dot{\theta}^2}{2}. \quad (6)$$

From eq. (3) we have,

$$\dot{x} = (a + R) \cos \theta \dot{\theta} - R(\phi - \theta) \sin \theta \dot{\theta} + R(\dot{\phi} - \dot{\theta}) \cos \theta, \quad (7)$$

$$\dot{y} = -(a + R) \sin \theta \dot{\theta} - R(\phi - \theta) \cos \theta \dot{\theta} - R(\dot{\phi} - \dot{\theta}) \sin \theta, \quad (8)$$

so the kinetic energy of the slab can be written as,

$$\begin{aligned} T_{\text{slab}} &= \frac{m}{2} \left[ (a + R)^2 \dot{\theta}^2 + R^2(\phi - \theta)^2 \dot{\theta}^2 + R^2(\dot{\phi} - \dot{\theta})^2 + 2R(a + R) \dot{\theta}(\dot{\phi} - \dot{\theta}) \right] + \frac{kma^2\dot{\theta}^2}{2} \\ &= \frac{m}{2} \left[ (1 + k)a^2\dot{\theta}^2 + R^2(\phi - \theta)^2 \dot{\theta}^2 + 2aR\dot{\theta}\dot{\phi} + R^2\dot{\phi}^2 \right]. \end{aligned} \quad (9)$$

The total kinetic energy  $T_{\text{cyl}} + T_{\text{slab}}$  is,

$$T = \frac{[m + (1 + K)M]R^2}{2}\dot{\phi}^2 + maR\dot{\phi}\dot{\theta} + \frac{(1 + k)ma^2 + mR^2(\phi - \theta)^2}{2}\dot{\theta}^2. \quad (10)$$

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<sup>3</sup>This contrasts with the case of a cylinder rolling on/inside another cylinder [1, 2], where the potential energy does not depend on  $\phi$ , such that there is a second conserved quantity for the system.

## 2.3 Equations of Motion

### 2.3.1 $\phi$

The  $\phi$ -equation for the Lagrangian  $\mathcal{L} = T - V$  is,

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\phi}} = [m + (1 + K)M]R^2 \ddot{\phi} + maR\ddot{\theta} = \frac{\partial \mathcal{L}}{\partial \phi} = mgR \sin \theta. \quad (11)$$

### 2.3.2 $\theta$

The  $\theta$ -equation can be written as,

$$\begin{aligned} \frac{1}{m} \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\theta}} &= aR\ddot{\phi} + [(1 + k)a^2 + R^2(\phi - \theta)^2] \ddot{\theta} + 2R^2(\phi - \theta)(\dot{\phi} - \dot{\theta}) \dot{\theta} \\ &= \frac{1}{m} \frac{\partial \mathcal{L}}{\partial \theta} = g[(a + R) \sin \theta + R(\phi - \theta) \cos \theta - R \sin \theta] \\ &= g[a \sin \theta + R(\phi - \theta) \cos \theta]. \end{aligned} \quad (12)$$

## 2.4 $\phi = \phi_0 = \text{Constant}$

Before discussing the general case, we consider the special case that the cylinder is fixed, but the initial angle  $\phi_0$  is not necessarily zero.

Then, the  $\phi$ -equation of motion (11) is to be ignored, and the  $\theta$ -equation (12) becomes,

$$[(1 + k)a^2 + R^2(\phi_0 - \theta)^2] \ddot{\theta} - 2R^2(\phi_0 - \theta) \dot{\theta}^2 = g[a \sin \theta + R(\phi_0 - \theta) \cos \theta]. \quad (13)$$

The potential energy (4) becomes,

$$\frac{V}{m} = g\{(a + R)(\cos \theta - \cos \theta_0) - R[(\phi_0 - \theta) \sin \theta - (\phi_0 - \theta_0) \sin \theta_0]\}, \quad (14)$$

the kinetic energy (10) becomes,

$$\frac{T}{m} = \frac{(1 + k)a^2 + R^2(\phi_0 - \theta)^2}{2} \dot{\theta}^2, \quad (15)$$

and the total energy becomes,

$$\begin{aligned} \frac{E}{m} &= \frac{(1 + k)a^2 + R^2(\phi_0 - \theta_0)^2}{2} \dot{\theta}_0^2 = \frac{(1 + k)a^2 + R^2(\phi_0 - \theta)^2}{2} \dot{\theta}^2 \\ &\quad + g\{(a + R)(\cos \theta - \cos \theta_0) - R[(\phi_0 - \theta) \sin \theta - (\phi_0 - \theta_0) \sin \theta_0]\}. \end{aligned} \quad (16)$$

### 2.4.1 Small Oscillations

We first seek an oscillatory solution, of the form,

$$\theta = \theta_0 + \alpha e^{i\omega t}, \quad \dot{\theta} = i\alpha\omega e^{i\omega t}, \quad \ddot{\theta} = -\alpha\omega^2 e^{i\omega t}, \quad (17)$$

where  $\alpha$  is small. Using this trial solution in eq. (13), and keeping terms only to order  $\alpha$ , we have,

$$\sin \theta \approx \sin \theta_0 + \alpha e^{i\omega t} \cos \theta_0, \quad \cos \theta \approx \cos \theta_0 - \alpha e^{i\omega t} \sin \theta_0, \quad (18)$$

$$\begin{aligned} & -\alpha \omega^2 [(1+k)a^2 + R^2(\phi_0 - \theta_0)^2] e^{i\omega t} \\ \approx & g [a (\sin \theta_0 + \alpha e^{i\omega t} \cos \theta_0) + R(\phi_0 - \theta_0 - \alpha e^{i\omega t} \sin \theta_0) (\cos \theta_0 - \alpha e^{i\omega t} \sin \theta_0)] \\ \approx & g [a \sin \theta_0 + R(\phi_0 - \theta_0) \cos \theta_0] + \alpha g [a \cos \theta_0 - R(\phi_0 - \theta_0) \sin \theta_0 - R \cos \theta_0] e^{i\omega t}. \end{aligned} \quad (19)$$

The constant term must be zero, which tells us that,

$$\tan \theta_0 = \frac{R}{a}(\theta_0 - \phi_0) = -\frac{b_0}{a}, \quad (20)$$

recalling eq. (2).

The terms in  $\alpha e^{i\omega t}$  must be the same on both sides of eq. (19), which tells us that the angular frequency  $\omega$  of small oscillations is related by,

$$\omega = \sqrt{\frac{g\{R[\cos \theta_0 - (\theta_0 - \phi_0) \sin \theta_0] - a \cos \theta_0\}}{(1+k)a^2 + R^2(\phi_0 - \theta_0)^2}} = \sqrt{\frac{g(R \cos \theta_0 - a/\cos \theta_0)}{a^2(1+k + \tan^2 \theta_0)}}. \quad (21)$$

Oscillatory solutions exist only for,

$$R > \frac{a}{\cos^2 \theta_0}, \quad \cos \theta_0 < \sqrt{\frac{a}{R}}, \quad (22)$$

which always requires that  $R > a$ .

In particular,  $\omega = \sqrt{g(R-a)/a^2(1+k)}$  for  $\phi_0 = 0 = \theta_0$ . For this case, the constant energy is,

$$\frac{E}{m} = \frac{(1+k)a^2}{2} \dot{\theta}_0^2 = \frac{(1+k)a^2}{2} \dot{\theta}^2 - g(a+R)(1-\cos \theta), \quad (23)$$

and we record the full equation of motion,

$$[(1+k)a^2 + R^2 \theta^2] \ddot{\theta} + 2R^2 \theta \dot{\theta}^2 = g [a \sin \theta - R \theta \cos \theta]. \quad (24)$$

For reference, we also record that in this case,

$$\dot{\theta}^2 = \dot{\theta}_0^2 + \frac{2g(a+R)(1-\cos \theta)}{(1+k)a^2}, \quad (25)$$

$$[(1+k)a^2 + R^2 \theta^2] \ddot{\theta} = g(a \sin \theta - R \theta \cos \theta) - 2R^2 \theta \left( \dot{\theta}_0^2 + \frac{2g(a+R)(1-\cos \theta)}{(1+k)a^2} \right) \quad (26)$$

For a solid slab of half width  $c$ ,  $k = (1 + c^2/a^2)/3$ , so for  $\phi_0 = 0 = \theta_0$ ,

$$\omega = \sqrt{\frac{3g(R-a)}{4a^2 + c^2}} \xrightarrow[\text{cube}]{\text{solid}} \sqrt{\frac{3g(R-a)}{5a^2}}. \quad (27)$$

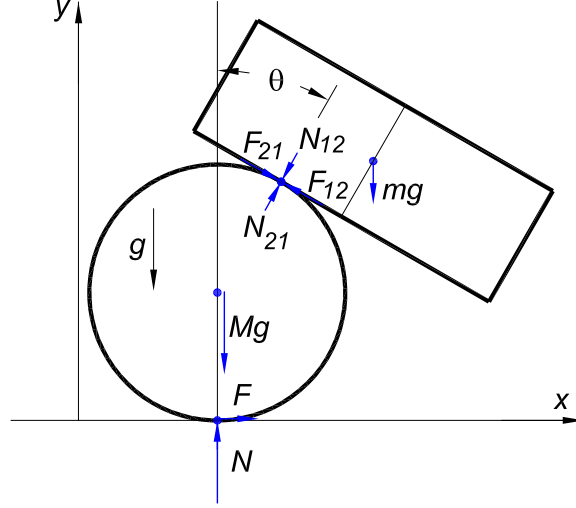
Note that it is possible to have small oscillations about a nonzero value of  $\theta_0$ , if the slab is appropriately off center with respect to the initial point of contact with the cylinder. For example, a cube of half length  $a = R/2$  would oscillate about an initial configuration with  $b_0 = -\sqrt{3}R/6$ ,  $\theta_0 = 30^\circ$  and  $\phi_0 = 15^\circ$  at angular frequency  $\omega = \sqrt{2g/\sqrt{3}R} = 1.075\sqrt{g/R}$ . This is about 2% less than the angular frequency  $\omega = \sqrt{6g/5R} = 1.095\sqrt{g/R}$  for  $\theta_0 = 0$ .

### 2.4.2 Angle $\theta_s$ at which the Slab Falls off the Cylinder

As the slab rotates it may lose contact with (separate from) the cylinder, say at angle  $\theta_s$ .

This happens when the normal force  $N_{12}$  of the cylinder on the slab vanishes, which occurs when the component of the gravitational force  $mg$  equals the component of  $m\mathbf{a}$  along an axis that makes angle  $\theta_s$  to the vertical,

$$mg \cos \theta_s = m(-\ddot{x}_s \sin \theta_s - \ddot{y}_s \cos \theta_s). \quad (28)$$



From eqs. (7)-(8), we find,

$$\begin{aligned} \ddot{x} &= (a + R)(\cos \theta \ddot{\theta} - \sin \theta \dot{\theta}^2) - R[(\phi - \theta)(\sin \theta \ddot{\theta} + \cos \theta \dot{\theta}^2) + \sin \theta \dot{\theta}(\dot{\phi} - \dot{\theta})] \\ &\quad + R[\cos \theta(\ddot{\phi} - \ddot{\theta}) - \sin \theta \dot{\theta}(\dot{\phi} - \dot{\theta})], \end{aligned} \quad (29)$$

$$\begin{aligned} \ddot{y} &= -(a + R)(\sin \theta \ddot{\theta} + \cos \theta \dot{\theta}^2) - R[(\phi - \theta)(\cos \theta \ddot{\theta} - \sin \theta \dot{\theta}^2) + \cos \theta \dot{\theta}(\dot{\phi} - \dot{\theta})] \\ &\quad - R[\sin \theta(\ddot{\phi} - \ddot{\theta}) + \cos \theta \dot{\theta}(\dot{\phi} - \dot{\theta})], \end{aligned} \quad (30)$$

$$\begin{aligned} \ddot{x} \sin \theta + \ddot{y} \cos \theta &= -(a + R)\dot{\theta}^2 - R[(\phi - \theta)\ddot{\theta} + \dot{\theta}(\dot{\phi} - \dot{\theta})] - R\dot{\theta}(\dot{\phi} - \dot{\theta}) \\ &= -R(\phi - \theta)\ddot{\theta} + (R - a)\dot{\theta}^2 - 2R\dot{\phi}\dot{\theta}. \end{aligned} \quad (31)$$

For constant angle  $\phi_0$ , the relation (28) becomes,

$$g \cos \theta_s = R(\phi_0 - \theta_s)\ddot{\theta}_s - (R - a)\dot{\theta}_s^2. \quad (32)$$

Equations (13) and (16) can be used in eq. (32) to determine  $\ddot{\theta}_s$  and  $\dot{\theta}_s$ , but the resulting expression is lengthy. Even for the particular case that  $\phi_0 = 0 = \theta_0$ , the resulting expression for  $\theta_s$  is complicated,

$$\begin{aligned} g \cos \theta_s &= \frac{R\theta_s}{(1+k)a^2 + R^2\theta_s^2} \left[ 2R^2\theta_s \left( \dot{\theta}_0^2 + \frac{2g(a+R)(1-\cos\theta_s)}{(1+k)a^2} + g(R\theta_s \cos\theta_s - a \sin\theta_s) \right) \right] \\ &\quad - (R-a) \left( \dot{\theta}_0^2 + \frac{2g(a+R)(1-\cos\theta_s)}{(1+k)a^2} \right). \end{aligned} \quad (33)$$

One conclusion that can be drawn is that for  $R \gg a$  the (thin) slab will not fall off the (large) cylinder (which is perhaps obvious without the preceding analysis).

## 2.5 Both $\phi$ and $\theta$ Vary

### 2.5.1 Coupled Oscillations

We first consider the possibility of small, coupled oscillations in both  $\phi$  and  $\theta$ , with equilibrium angles  $\phi_0$  and  $\theta_0$ .

We seek an oscillatory solution of the form (17)-(18) for  $\theta$ , and,

$$\phi = \phi_0 + \beta e^{i\omega t}, \quad (34)$$

where  $\beta$  is small, for  $\phi$ . To use these trial solutions in eqs. (11)-(12), we have in addition to eq. (18) that,

$$\sin \phi \approx \sin \phi_0 + \beta e^{i\omega t} \cos \phi_0, \quad \cos \phi \approx \cos \phi_0 - \beta e^{i\omega t} \sin \phi_0. \quad (35)$$

Then, keeping terms only that are constant or proportional to  $e^{i\omega t}$ ,<sup>4</sup> the  $\theta$ -equation of motion (12) becomes,

$$\begin{aligned} & -\omega^2 \beta a R e^{i\omega t} - \omega^2 \alpha e^{i\omega t} [(1+k)a^2 + R^2(\phi_0 - \theta_0)^2] \\ \approx & g \{ a(\sin \theta_0 + \alpha e^{i\omega t} \cos \theta_0) + R[\phi_0 - \theta_0 + (\beta - \alpha) e^{i\omega t}] (\cos \theta_0 - \alpha e^{i\omega t} \sin \theta_0) \}. \end{aligned} \quad (36)$$

The constant term in eq. (36) must be zero, which again tells us that,

$$\tan \theta_0 = \frac{R}{a}(\theta_0 - \phi_0) = -\frac{b_0}{a}. \quad (37)$$

The terms in  $e^{i\omega t}$  must be the same on both sides of eq. (36), which tells us that,

$$\begin{aligned} & \omega^2 [\beta a R + \alpha(1+k)a^2 + \alpha R^2(\phi_0 - \theta_0)^2] \\ = & g \{ R[(\alpha - \beta) \cos \theta_0 - \alpha(\theta_0 - \phi_0) \sin \theta_0] - \alpha a \cos \theta_0 \} \\ = & g [R(\alpha - \beta) \cos \theta_0 - \alpha a / \cos \theta_0]. \end{aligned} \quad (38)$$

To go further, we now consider the  $\phi$ -equation (11),

$$-\omega^2 e^{i\omega t} \{ \beta [m + (1+K)M] R^2 + \alpha m a R \} \approx m g R (\sin \theta_0 + \alpha e^{i\omega t} \cos \theta_0). \quad (39)$$

The constant term in eq. (39) must vanish, which implies that coupled oscillations are only possible for  $\theta_0 = 0$ . Then, from eq. (37) we have that  $\phi_0 = b_0$  also, and eq. (38) becomes

$$\omega^2 [\beta a R + \alpha(1+k)a^2] = g [R(\alpha - \beta) - \alpha a]. \quad (40)$$

In addition, the terms in  $e^{i\omega t}$  on the left and right sides of eq. (39) must be the same, which implies that,

$$-\omega^2 \{ \beta [m + (1+K)M] R^2 + \alpha m a R \} = \alpha m g R. \quad (41)$$

This condition cannot be satisfied, so **there is no coupled oscillatory motion when the cylinder is free to roll**; it will always roll out from under the slab, which rotates until it falls off the cylinder at some angle  $\theta_s$  of separation. An analysis of angle  $\theta_s$  could be given via an extension of the discussion in sec. 2.4.2, but we will not pursue this here.

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<sup>4</sup>We will not consider terms in  $e^{2i\omega t}$  since the approximations (18) and (35) have omitted terms of this type.

### 2.5.2 Small Oscillations of the Slab

We next consider the possibility that as the cylinder rolls the slab executes small oscillatory motion in  $\theta$ , with an angular frequency that varies “slowly” with time. In the “instantaneous” approximation, the angular frequency  $\omega(t)$  is just that associated with that found in sec. 2.4 for  $\phi_0 = \phi(t)$ .

It does not appear that analytic techniques are especially helpful in the next approximation, such that it is best to use numerical integration of the equations of motion (11)-(12) to carry the discussion further.

## References

- [1] K.T. McDonald, *Cylinder Rolling on a Rolling Cylinder*, (Oct. 2, 2014), <http://kirkmcd.princeton.edu/examples/2cylinders.pdf>
- [2] K.T. McDonald, *Cylinder Rolling inside Another Rolling Cylinder*, (Oct. 21, 2014), [http://kirkmcd.princeton.edu/examples/2cylinders\\_in.pdf](http://kirkmcd.princeton.edu/examples/2cylinders_in.pdf)
- [3] K.T. McDonald, *Motion of a Rigid Body Which is Rolling without Slipping*, Princeton U. Ph205 Lecture 20 (1980), <http://kirkmcd.princeton.edu/examples/Ph205/ph205l20.pdf>