

MERcury Intense Target (MERIT) Overview

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Background



- Proof-of-principle experiment to investigate the interaction of a proton beam with a Hg jet inside a highstrength magnetic field
 - If successful, method might be used as production target in new physics facility
- Primary diagnostic for the beam-jet interaction is optical
 - Multiple high-speed cameras will be used to record interaction
- Collaborative effort among multiple national laboratories, universities, and research facilities
- Experiment to be conducted at CERN (Geneva) in April 2007

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Prior Work

E951 Tests (H.Kirk - BNL)

- 1cm dia, 2.5m/s Hg jet
- 24 GeV 4TP beam
- No magnetic field
- Jet dispersal observed

CERN/Grenoble Tests (A.Fabich,J.Lettry -NuFACT'02)

- 4cm dia, 12m/s Hg jet
- 0,10,20T magnetic field
- No proton beam
- Jet stabilization with increasing field

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Experiment Profile



Hg Jet

- 1-cm diameter, 20 m/s, delivered to coincide with magnet peak field
- Required flow rate of 1.57 liter/s (25gpm)

Magnet

- 16-cm diameter bore that Hg system must fit within
- 15 Tesla magnetic field
- Peak field duration ~1 sec
- Magnet cool-down time ~30 minutes
- Environment
 - 24 GeV proton beam, up to 28x10¹² (TP) per 2µs spill
 - 1-atm air environment inside target delivery system primary containment
 - Total integrated dose 10⁴ rads

Geometry

- Hg jet 100 milliradians off magnet axis
- Proton beam 67 milliradians off magnet axis
- Jet intersects beam at magnet Z=0
- Up to 100 beam pulses for the CERN test delivered in a pulse-on-demand mode

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Experiment Geometric Configuration

Experiment is prototypic of a N.F. facility target layout

- Magnet tilt (wrt beam) = 66 mrad (3.8°)
- Hg jet tilt (wrt magnet axis) = 100 mrad (5.7°)
- Hg jet center intersects beam center at Z=0
- Jet in same direction as beam



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Experiment Layout



- Hg target is a self-contained module inserted into the magnet bore
- Two containment barriers between the Hg and the tunnel environment



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MERIT Layout



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LabView-Based Control System

- Remote control over long distance limited choices
 - Analog I/O modules need to be close to equipment and power supplies
- LabView controller on laptop computer was chosen
 - National Instruments recommends CompactPCI I/O modules
 - Communicates to laptop via EtherNet cable
 - Allows custom operator interface, data logging if required during development
 - Should allow straightforward integration with other control systems
- Control system development to begin late October

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MERIT Side View

- Tilt limited syringe length
- CERN facility constraints limited syringe width



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Hg System Schematic





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Hg Syringe System





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Hg Syringe System

- Hg flow rate 1.6liter/s (24.9gpm)
- Piston velocity 3.0cm/s (1.2in/sec)
- Hg cylinder force 525kN (118kip)





Primary Containment

- Hg supply flow path
 - 1-inch Sch 40 pipe
 - 1-inch flex metal hose w/sanitary fittings (want smooth wall can hydraulic hose be used?)
 - 1-inch, 0.065-wall rigid tubing
 - 5-inch diameter plenum
 - 12mm-dia, 1mm-wall rigid tubing

- Hg jet return path
 - 1/4-inch plate weldment chamber
 - 6-inch to 2-1/2-inch eccentric reducer
 - 2-1/2-inch flex metal hose w/sanitary fittings
 - Sump tank

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Fathom Flow Simulation



- System diagram for Hg flow
- Results indicate maximum pressure requirement of ~780 psi (50 bar) for baseline plenum/nozzle configuration
- Design system for max pressure of 1000 psig (70 bar)





Fathom Details



Pipe C	Output Tabl	e												Maria
		Pipe			Flow				-	P Stag	dP Stag		P Static	dP Static
		Nominal		Longth	Area	Velocity	Povpolde		D Stag	Out	Total	P Static		Total
Dino	Name	Sizo	(aal/min)	(inches)	(inches 2)	(foot/soc)	No		In (nsig)	(psig)	(neid)	In (neig)	(psig)	(psid)
ripe		linde 10 inch	(yai/1111) 24 0	(110105)	78 854	0 101	6 86E±04	0.0206	78/	(psig) 784	2 77E-05	783 0	(psig) 784	2 77E_0
	2 Cylinder D 1 inch		24.3	15	0.864	0.101	6.56E±05	0.0290	704	704	0.100770	703.9	704	0 100770
	2 Cyline	der D 1 inch	24.3	1.5	0.004	9.24	0.30L+03	0.0230	700	700	0.199779	760	760	0.199776
		anifol 1 inch	24.9	16.1	0.004	9.24	0.50E+05	0.0130	774	764	0.302700	765.0	709	0.302700
			24.9	10.1	0.004	9.24	0.000000	0.2745	714	704	9.112201	765.9	700	9.11220
			24.9	Z. I	0.804	9.24	0.0000000	0.0358	701	760	0.279691	752.0	752	0.27969
	6 Flex I		24.9	10.5	0.945	8.449	0.2/E+05	0.17	760	759	1.110492	753.7	753	1.110492
	7 Hg St	upply 1 inch	24.9	1.80	0.594	13.433	7.91E+05	0.0284	755	755	0.469346	738.7	738	0.469346
	8 Hg Si	upply 1 Inch	24.9	6.7	0.594	13.433	7.91E+05	0.1024	752	750	1.690654	735.3	734	1.690654
	9 Hg Si	upply 1 inch	24.9	44	0.594	13.433	7.91E+05	0.6726	747	736	11.1028	730.8	720	11.1028
	10 Plenu	m 5 inch	24.9	3	20.006	0.399	1.36E+05	0.0105	721	721	0.000153	720.6	721	0.000153
	11 Nozzl	e 1/2 inch	24.9	4	0.108	74.271	1.86E+06	0.1491	469	394	75.21312	-35.3	-110	75.21312
All Jur	nction Tabl	e												
_														
			Elevation				P Stag.	dP Stag.		P Static	dP Static		11-1-1	
		Junction	Inlet	Loss	dH	P Stag.	Out	Total	P Static	Out	Total	T Inlet		
Jct	Name	е Туре	(inches)	Factor (K)	(inches)	In (psig)	(psig)	(psid)	In (psig)	(psig)	(psid)	(deg. F)		
	1 Syringe Pi Assigned		0	0	0	784	784	0	784	783.9	0	68		
	2 Area	Chan Area Chan	0	4,128.12	7.895	784	780	3.8729	784	772.2	11.682	68.2		
	3 Bend	1 Bend	0	0.33841	5.388	780	777	3.011	772	769	3.011	68.2		
	4 Bend	2 Bend	1.15	0.27347	4.354	776	774	2.7736	769	765.9	2.774	68.2		
	5 Bend	3 Bend	18	0.33841	5.388	764	761	3.3789	756	752.8	3.379	68.3		
	6 Pipe f	to Fle Area Chan	19.5	0.00733	0.117	760	760	0.0572	752	753.7	-1.223	68.3		
	7 Flex t	o Tul Area Chan	19.5	0.60087	7.999	759	755	3.924	753	738.7	13.901	68.3		
	8 Tubin	g Ber Bend	19.5	0.17406	5.857	755	752	2.8734	738	735.3	2.873	68.3		
	9 Tubin	9 Tubing Ber Bend 19.5 0.17406 5.85		750	747	2.8734	734	730.8	2.873	68.3				
	10 Plenu	m Inl Area Chan	19.5	0.94145	31.682	736	721	15.5414	720	720.6	-0.952	68.3		
	11 Nozz	e Inle Area Chan	19.5	17,240.17	512.271	721	469	251.2909	721	-35.3	755.894	68.3		
	12 Spray	Spray Disc	19.5	0.78106	802,957	394	0	393,8837	-111	-504.6	393,884	75		

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Other Fathom Simulations

- 1/2" tubing bend
 - Cylinder pressure 1200 psi (83 bar)
- No-bend short 1/2" tube
 Cylinder pressure 710 psi (48 bar)
- 1" tubing bend
 - Cylinder pressure 780 psi (54 bar)
- All 1/2" tubing from end of flex metal hose, no plenum
 - Cylinder pressure 1910 psi (130 bar)
- Any non-plenum design should minimize number of bends & length of nozzle tubing
- Don't let syringe pump limit nozzle configuration – desire to change syringe design pressure to 1500 psi (103 bar) to match Hg cylinder rating

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Primary Containment Cross Section



Secondary Containment

- SS and Lexan enclosure around entire primary system
- Contains Hg vapors/leaks, provides access to monitor Hg vapors
- Provides access to optical diagnostics, hydraulics, and sensors
- Incorporates beam windows



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Secondary Containment Access Ports

- Optical diagnostics
- Instrumentation
- Hydraulics
- Hg drain & fill (without opening secondary)
- Hg extraction (in event of major leak in primary containment)



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Hg Delivery System Procurement Plan



- Syringe system procured first because of expected long lead time on cylinders
- Details of primary/secondary containments & baseplate being finalized
 - Expect to begin procurement process in Nov/Dec
- Syringe system to be integrated by containment fabricator



	- Will	PROL
Test Plan	π	21
Magnet testing at MIT	Oct - Dec 4	Control
Hg nozzle tests at Princeton –Iterate nozzle design as needed	Oct - Dec 2005	
Hg target system testing at ORNL -Includes optical diagnostics -Initially test with water to develop syringe control system -Incorporate Princeton nozzle design, iterate if necessary -Practice Hg fill and extraction -Hg jet characterized	April - June 2006	
Integrated test at MIT –Practice CERN installation sequence –Hg jet in magnetic field characterized	Aug - Sept 2006	
Ship system to CERN	Nov 2006	
Experiment scheduled at CERN	April 2007	

