

# Megawatt targets for Neutrino Super-Beams

(Apr. 4, 2013)

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+ T2K Beam Group

+ LAGUNA/LBNO/CN2PY Study Group

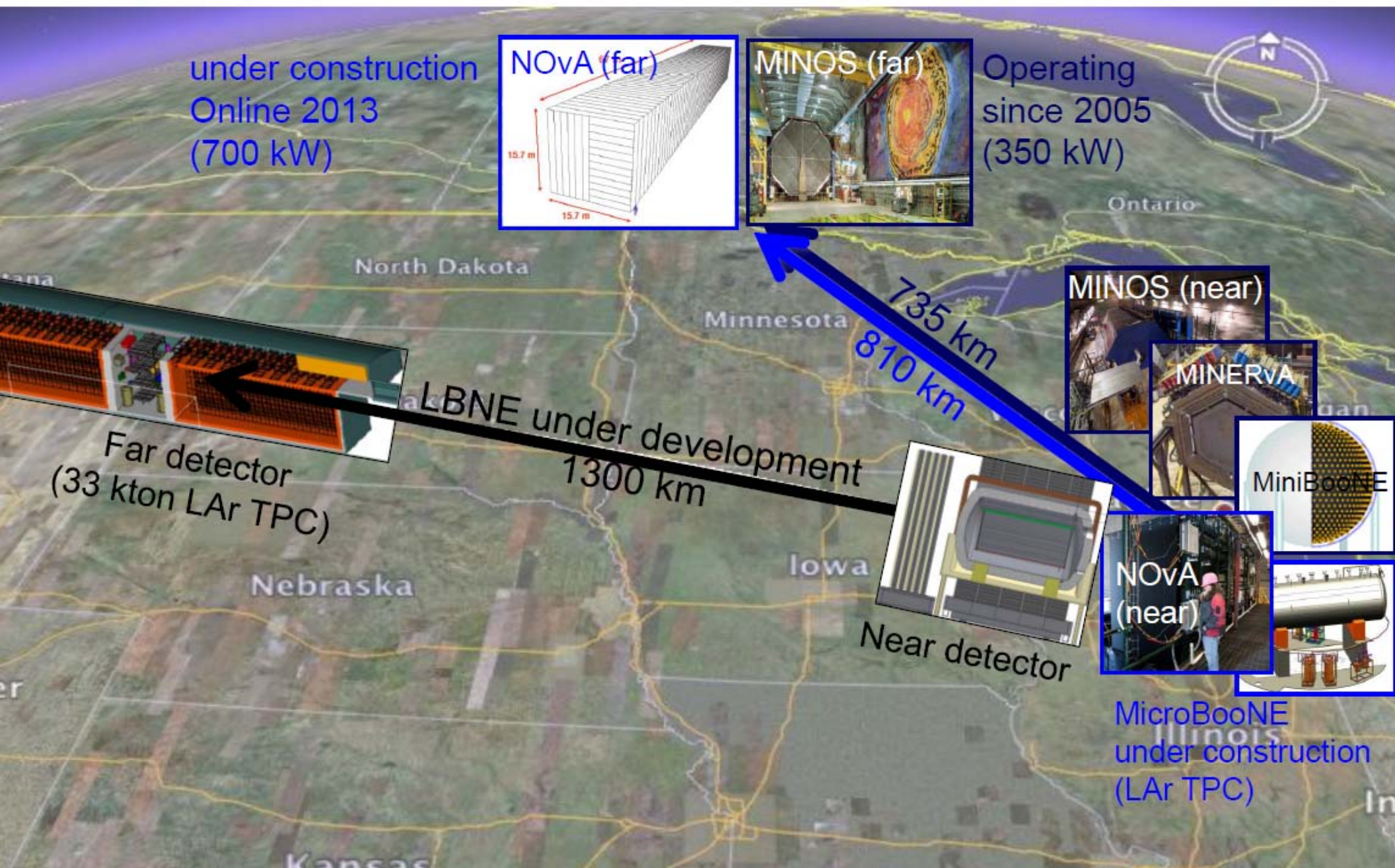
# 'Conventional' neutrino beams: where we are

	Fermilab NuMI/NOvA	JPARC T2K	CERN CNGS
Beam energy	120 GeV	30 GeV	400 GeV
Beam cycle	2.2 s	2.1 s	6 s
Spill length	10 $\mu$ s	4.2 $\mu$ s	2 x 10.5 $\mu$ s
Design beam power	400 kW	750 kW	750 kW
Maximum beam power to date	375 kW	230 kW	311 kW (448 kW over 30s)
Beam size (rms)	1.1 mm	4.2 mm	0.5 mm
Physics	$\nu_{\mu}$ disappearance	$\nu_{\mu} \rightarrow \nu_e$ appearance, $\nu_{\mu}$ disappearance	$\nu_{\mu} \rightarrow \nu_{\tau}$ appearance
First beam	2005	2009	2006

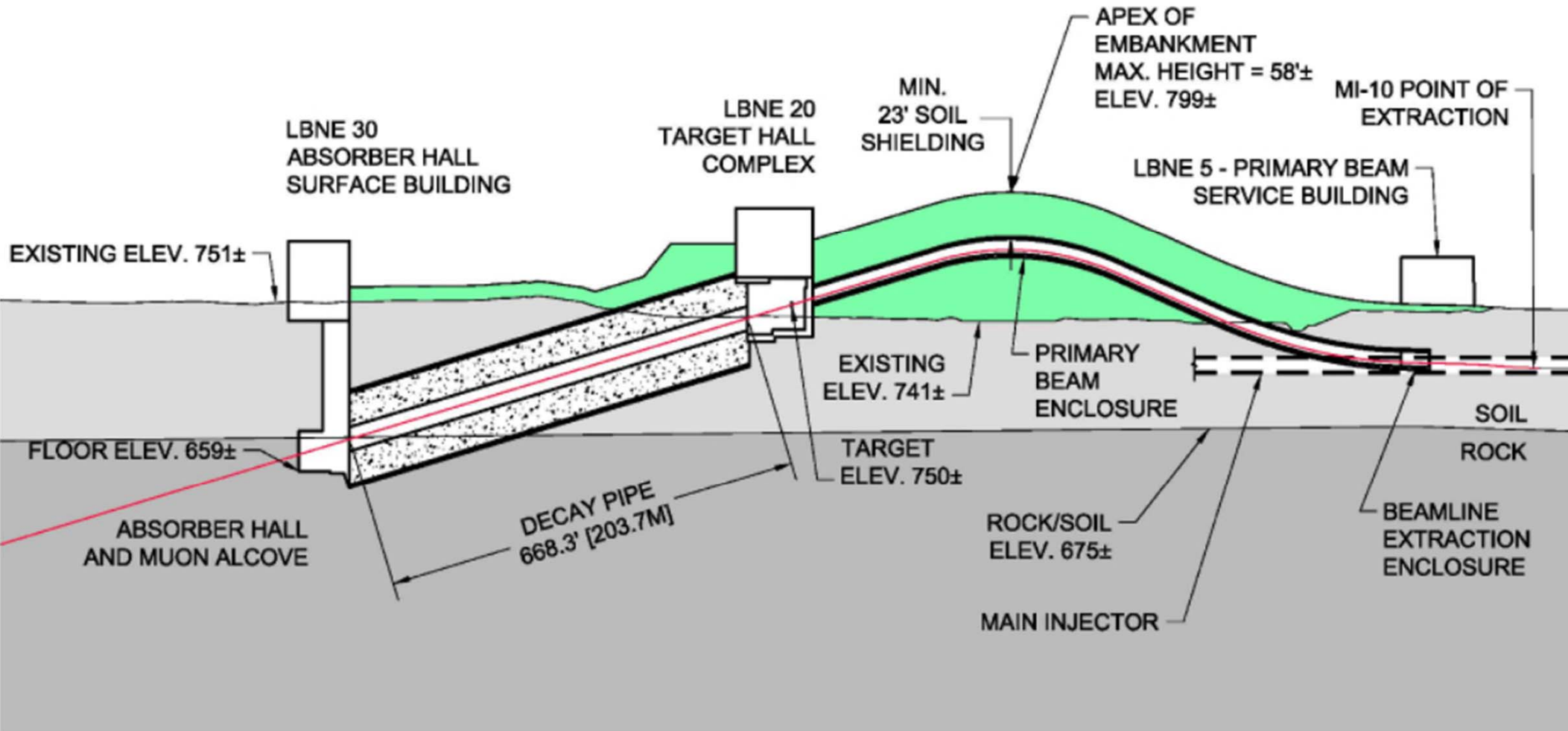
# Neutrino 'Superbeams' : where we want to go

	Fermilab LBNE (/Project X)	JPARC T2K Long term plan (2018-)	CERN CN2PY/LBNO (Phase 2)
Design beam power	2.3 MW	3.2 MW	2 MW
Beam energy	120 GeV	50 GeV	50 (70)GeV
Rep rate	0.75 Hz	1 Hz	1.33 Hz
Beam sigma (range)	1.5 - 3.5 mm	4.2 mm	
Heat load in: C Be Ti pebble bed	10.5 - 23.1 kW	~100 kW	

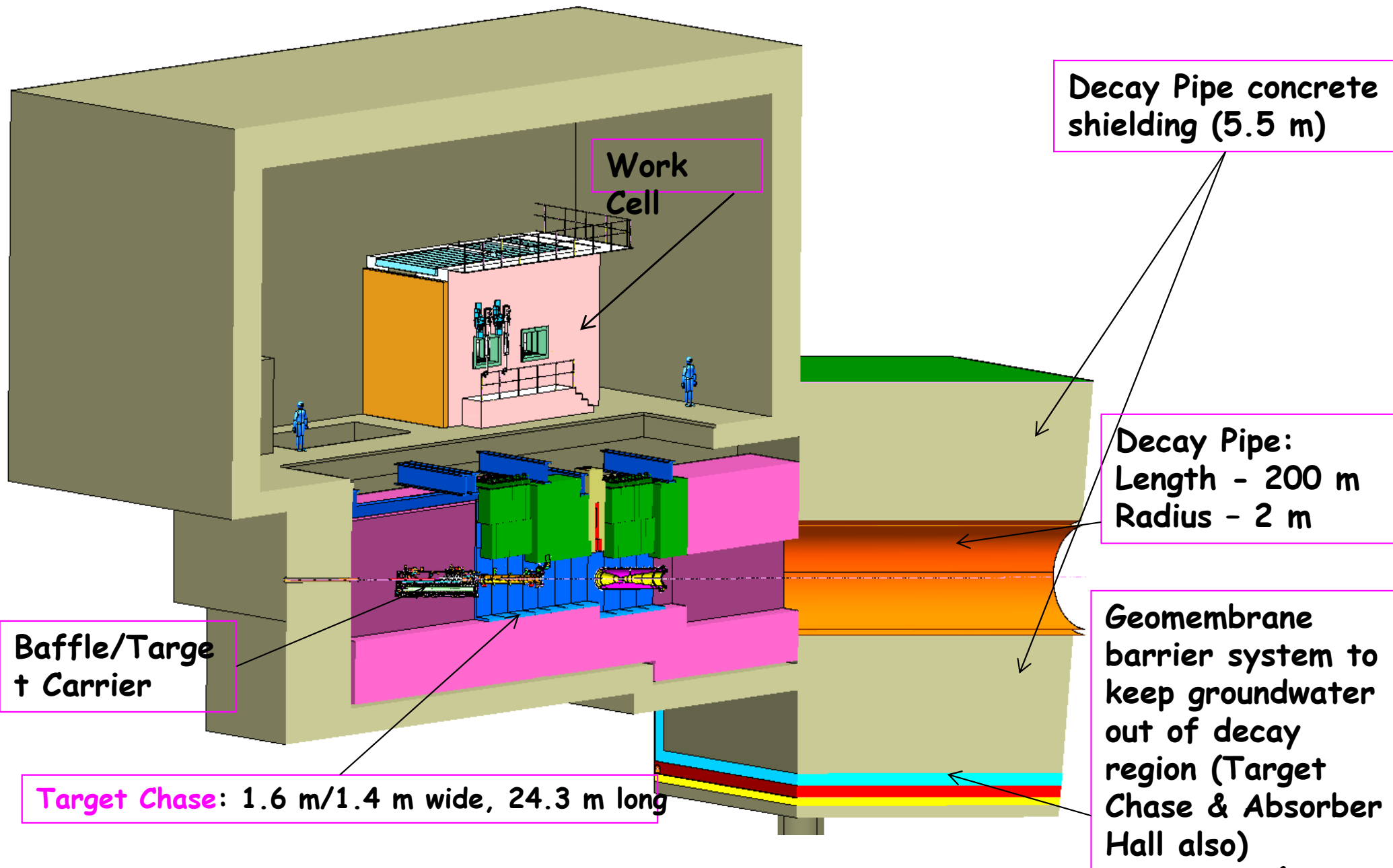
# Neutrino Program at Fermilab



# LBNE Overview



# LBNE Target Facility - for 2.3 MW operation

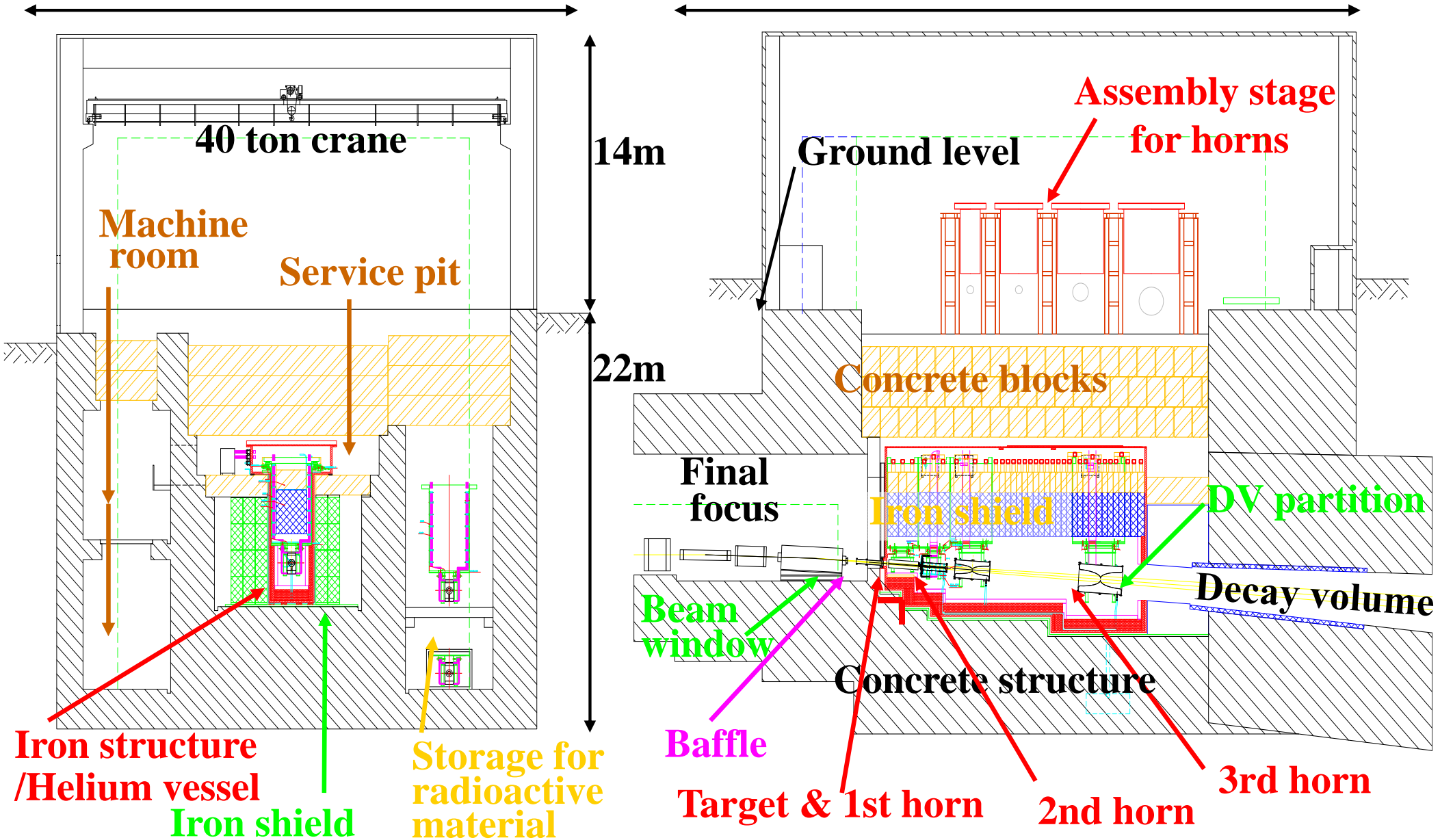


# T2K Target Station for 4 MW

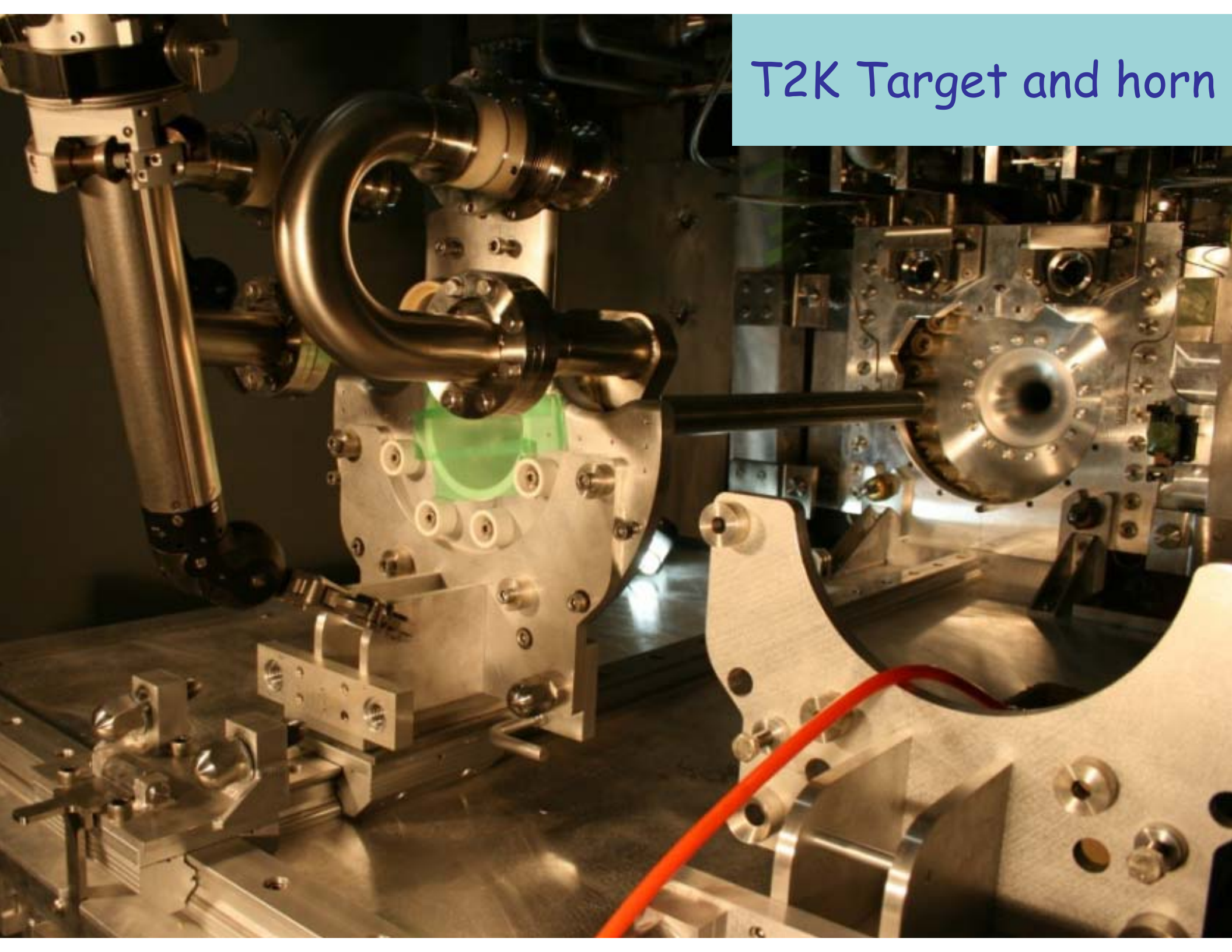
Y. Yamada

27m

34m

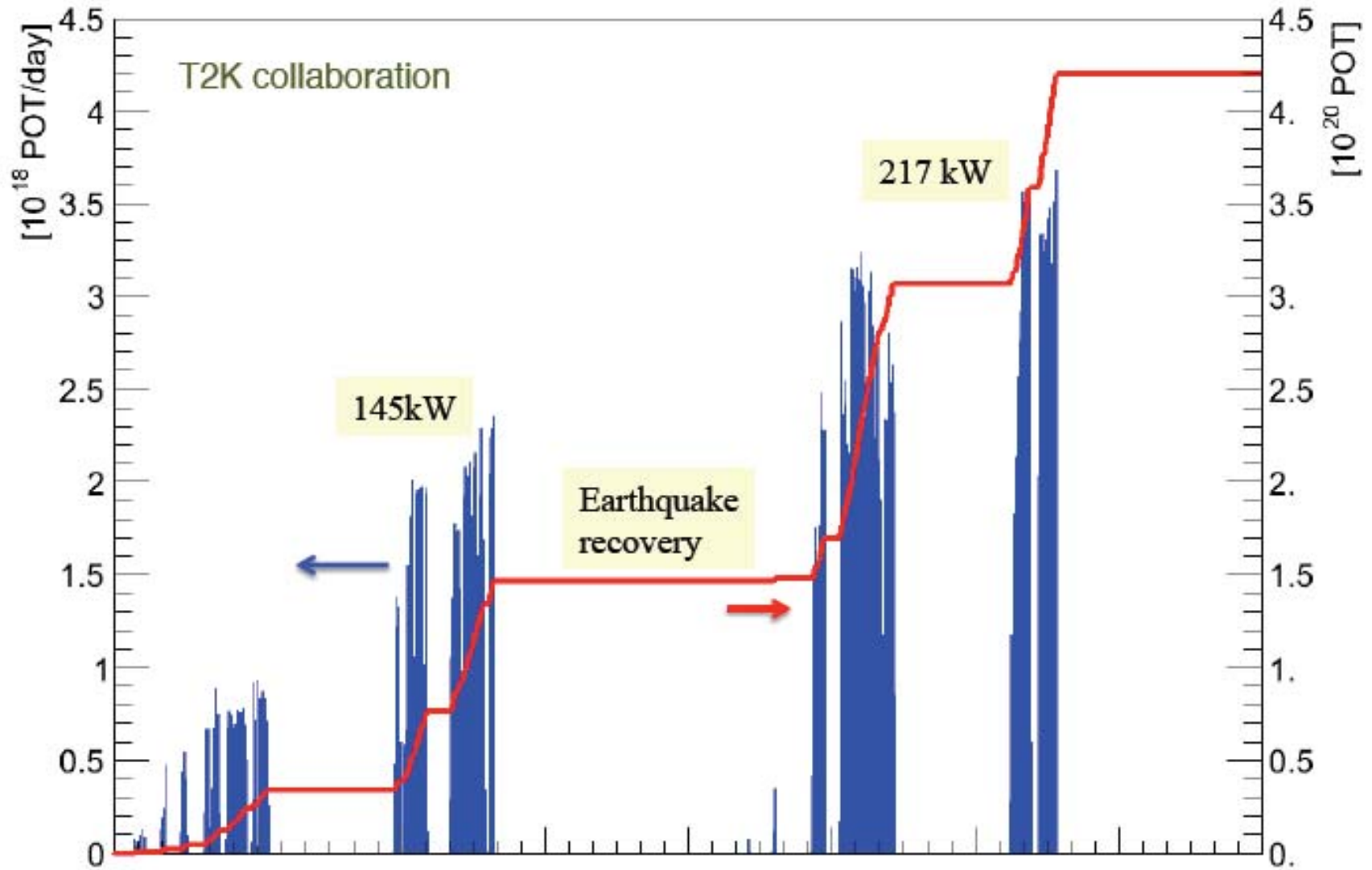


# T2K Target and horn





## History of delivered beam to the T2K experiment



Beam delivery to the T2K experiment in 2012 finished on Dec. 14.

Accumulated number of proton  $\sim 4.2 \times 10^{20}$  POT.

# T2K: Plans for 8 GeV Booster Ring for 2-3 MW



Tadashi Koseki (KEK)

# CN2PY - Layout Options

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Update since CERN Meeting -  
October'12

For the **WP4 Layout Study Group**:  
M. Calviani, I. Efthymiopoulos, B. Goddard,  
A. Kosmicki, J. Osborne, Y. Papaphilippou, R.  
Steerenberg, P. Velten. H. Vincke



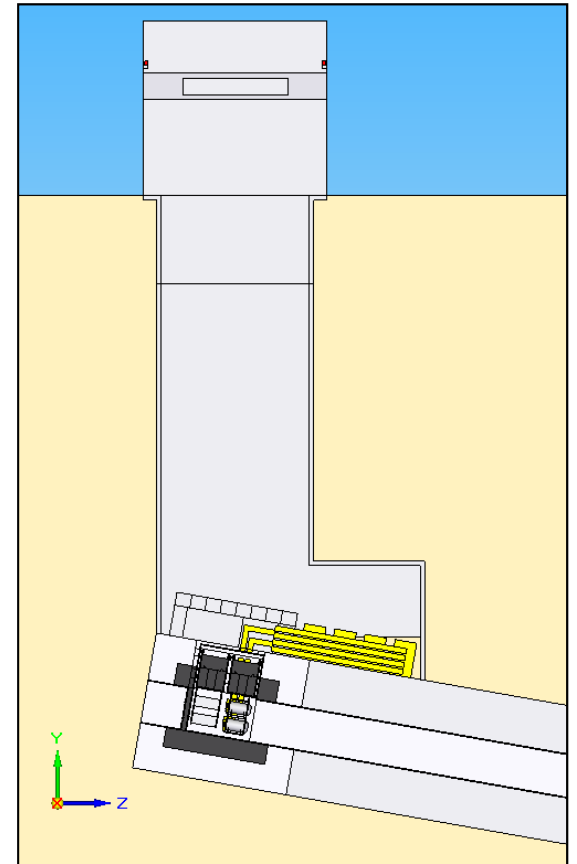
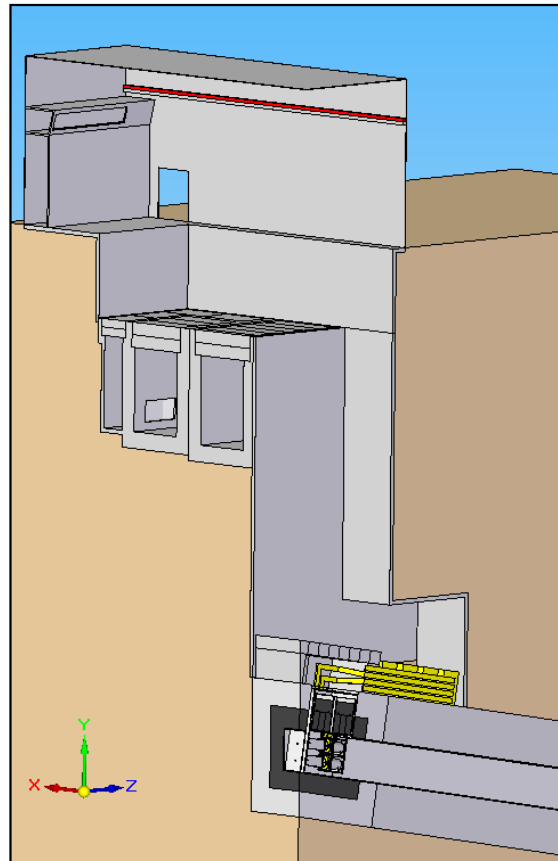
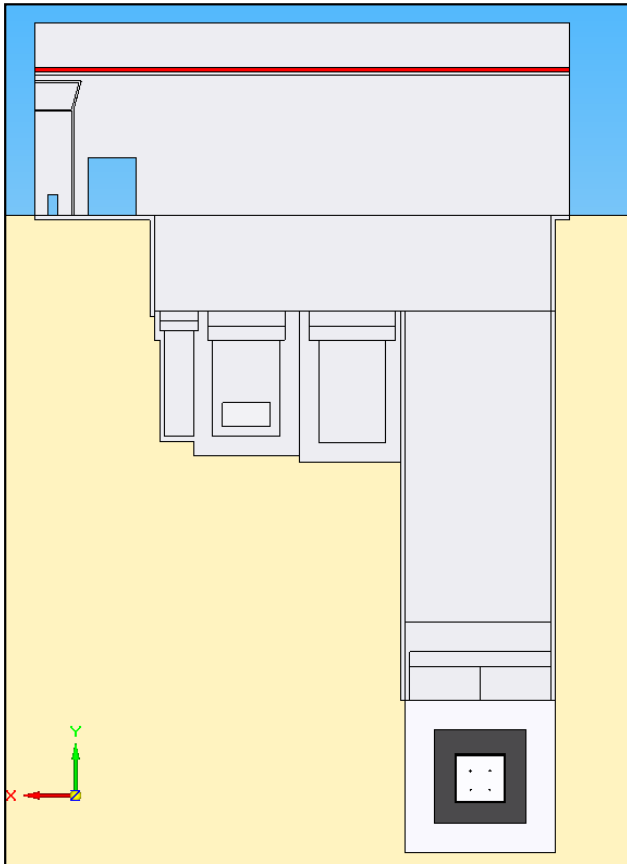
# CERN $\nu$ -beam to Pyhäsalmi - CN2PY : Option-A

- Option A:**
- 400 GeV extraction from TT60 (TI2)
  - Target cavern close to BA2
  - ND just outside Prevezsin fenced area



# Preliminary Concept for CN2PY

- Keep as many buildings as possible at the surface to keep construction costs down
  - Must have a shaft to access the horns and targets
  - Power supplies (or transformers) must be underground, close to the beamline
  - The pump house may also be underground, depending on the acceptable pressure drop



*Drawings not to scale: number and layout of horns will be different in practice, as will beamline dimensions*

Dan Wilcox



# CERN $\nu$ -beam to Pyhäsalmi - CN2PY

## CN2PY beam

- **Phase 1** : use the proton beam extracted beam from SPS
  - **400 GeV**, max  $7.0 \cdot 10^{13}$  protons every 6 sec, **750 kW** nominal beam power,  $10 \mu\text{s}$  pulse
- **Phase 2** : use the proton beam from the new HP-PS
  - **50(70) GeV**, 1.33 Hz,  $1.9 \cdot 10^{14}$  ppp, **2 MW** nominal beam power,  $4 \mu\text{s}$  pulse

## Requirements - layout

- Use the same secondary beam elements for both beams
  - sufficient shielding to contain the produced radiation
    - including muons, water and soil activation (H3 and NA22 production)
  - target and focusing elements (horns) with similar parameters
    - same layout or allow variations already from the design phase
    - don't have to be identical since anyhow are to be exchangeable
- Use the same beam decay volume, dump and near detector
  - deposited energy in target, shielding and dump would be  $\times 2.7$  higher for the Phase-II beam

-The facility layout is driven by the 400 GeV beam

- The target cavern layout (shielding) is driven by the 50(70) GeV beam and the 2MW of power

# Target Basics (J.Hylen)

Long enough ( 2 interaction lengths ) to interact most protons

Dense enough that  $2 \lambda_{\text{int}}$  fits in focusing system depth-of-field

Radius:  $R_{\text{target}} = 2.3 \text{ to } 3 R_{\text{beam}}$  (minimize gaussian tails missing target)

Narrow enough that pions exit the sides without re-absorption

(but for high  $E_{\text{proton}}$  and low  $E_{\nu}$ , secondary shower can help)

High pion yield ( but to first order,  $\nu$  flux  $\propto$  beam power )

Radiation hard

Withstand high temperature

High strength (withstand stress from fast beam pulse)

Low density (less energy deposition density, hence less stress; don't re-absorb pions)

Low  $dE/dx$  (but not much variation between materials)

High heat capacity (less stress induced by the  $dE/dx$ )

Low thermal expansion coefficient (less stress induced by the  $dE/dx$ )

Low modulus of elasticity (less stiff material does not build up stress)

Reasonable heat conductivity

Reasonable electrical conductivity ( monitor target by charge ejection)

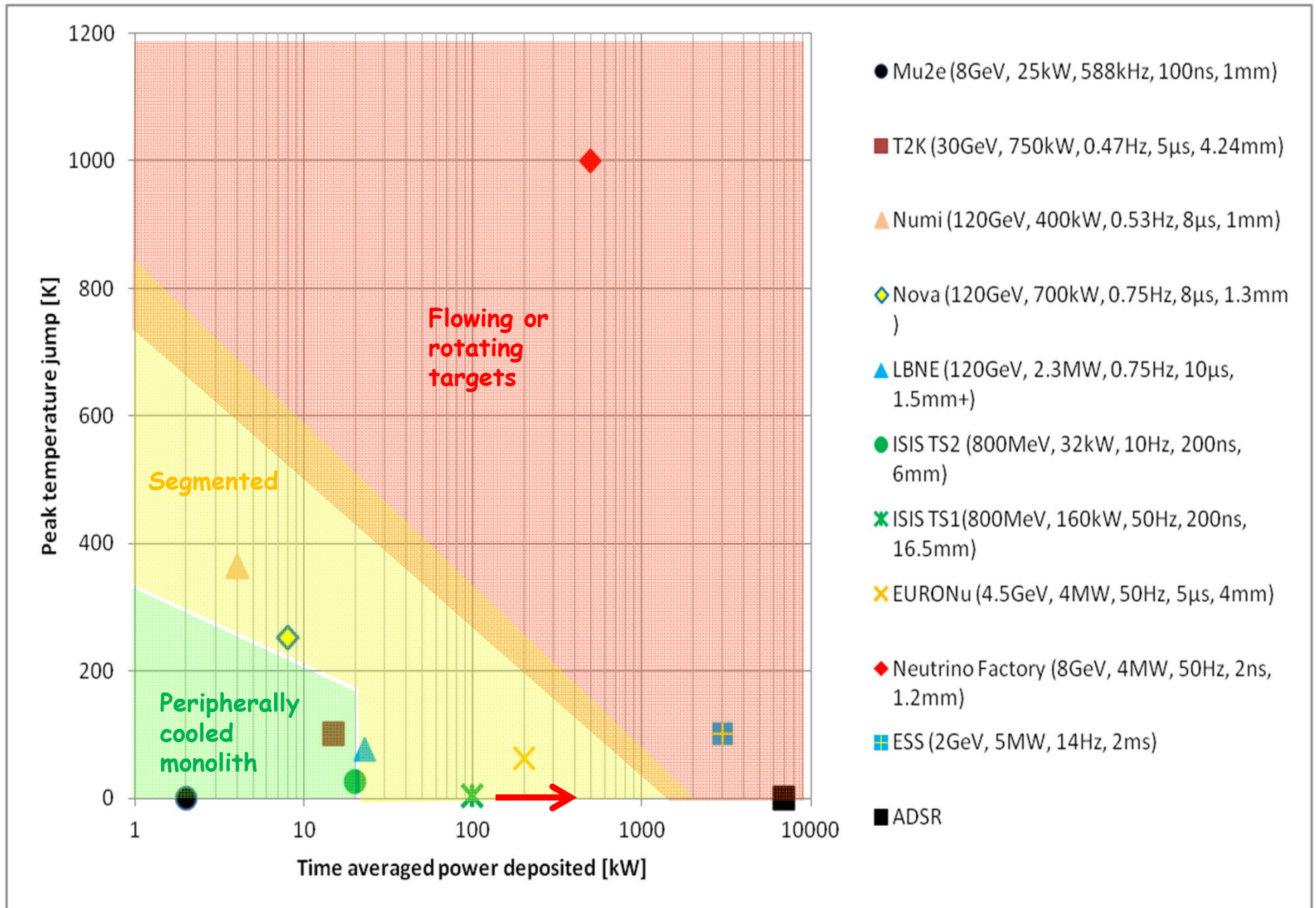
*CNGS, NuMI, T2K all using graphite*

# Existing target technologies

	NuMI/NOvA	CNGS	T2K
Target material	Graphite: POCO ZXF-5Q	Graphite and Carbon-carbon	Graphite: IG 430
Target arrangement	Subdivided	subdivided	monolithic
Cooling	Water (forced convection)	Helium (natural convection)	Helium (forced convection)
Limitations for higher power operation	<ul style="list-style-type: none"> <li>•Radiation damage</li> <li>•Water hammer, cavitation</li> <li>•Hydrogen + tritium + water activation</li> </ul>	<ul style="list-style-type: none"> <li>• Only possible for low deposited heat loads</li> </ul>	<ul style="list-style-type: none"> <li>•Heat transfer</li> <li>•Radiation damage</li> <li>•High helium volumetric flow rate (and high pressure or high pressure drops)</li> </ul>

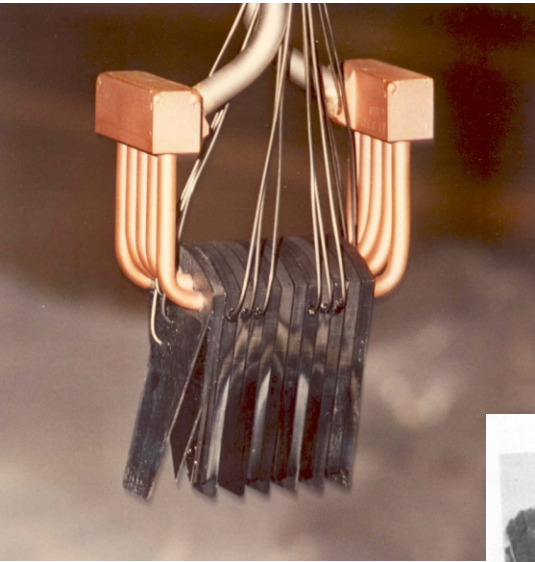


# Limitations of target technologies



# Ashes to ashes, dust to dust...

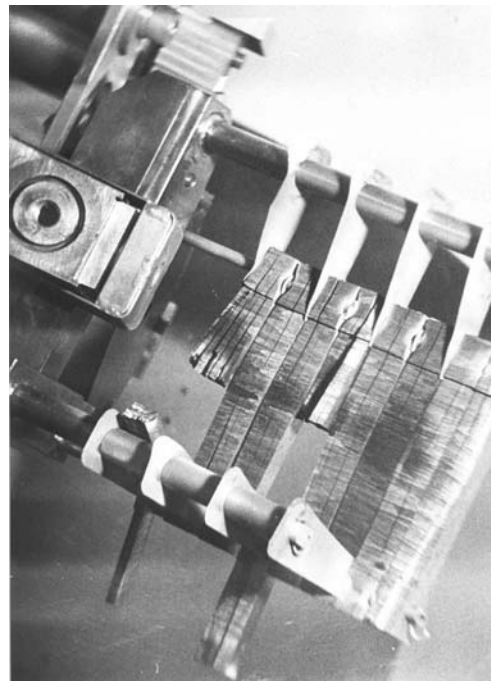
Effect of proton beams on some graphite targets



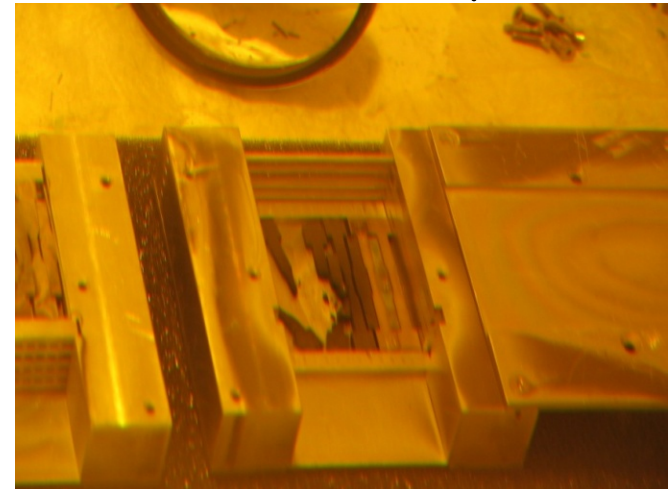
**LAMPF**  
fluence  
 $10^{22}$   
p/cm<sup>2</sup>



**PSI** fluence  
 $10^{22}$  p/cm<sup>2</sup>



**BNL tests:**  
fluence  $\sim 10^{21}$  p/cm<sup>2</sup>



# Physics vs Engineering Optimisation ?

## Target and Beam Dimensions

- For pion yield - smaller is better
  - Maximum production and minimum absorption (shown by FoM)
- For target lifetime - bigger is better
  - Lower power density - lower temperatures, lower stresses
  - Lower radiation damage density
- For integrated neutrino flux, need to take both neutrino flux and lifetime factors into account
  - Want to make an assessment of trade off between target lifetime vs beam and target dimensions
  - Answer will depend on Target Station engineering (time to change over target and horn systems)

# Target configurations considered for Superbeams

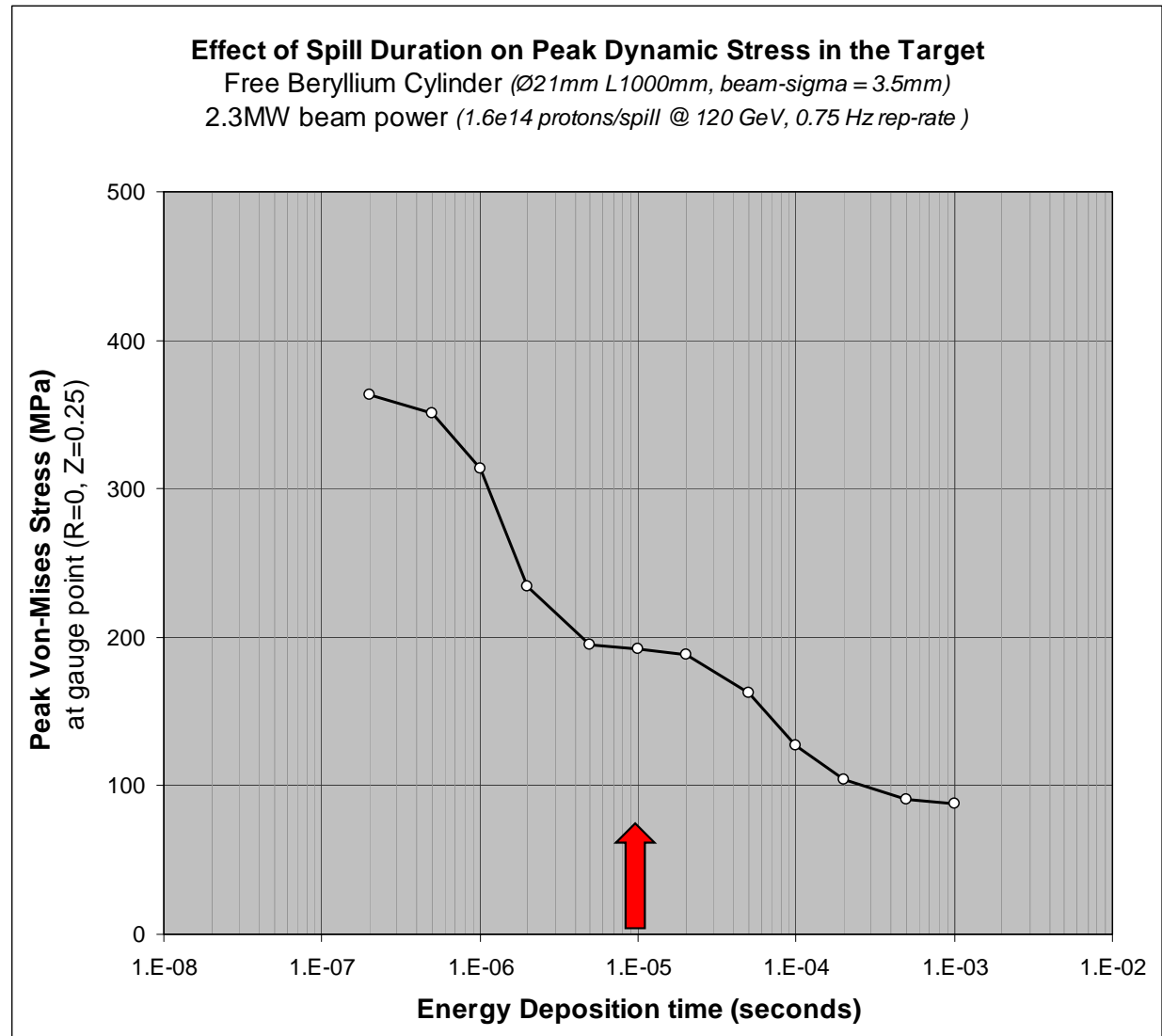
## 1. LBNE at Fermilab

- Integral target and horn inner conductor
  - Solid Be rod
  - water spray cooled
- Separate target installed inside bore of horn inner conductor
  - Graphite, water cooled (IHEP study (baseline))
  - Be: subdivided in z, water cooled
  - Be: spheres, helium cooled

## 2. EUROnu SuperBeam using high power SPL at CERN 4-horn system (4 x 12.5 Hz)

- 'Pencil' shaped beryllium rod
- 'Packed bed' of titanium beads
- Integral target and horn inner conductor
- (Graphite excluded due to radiation damage concerns)

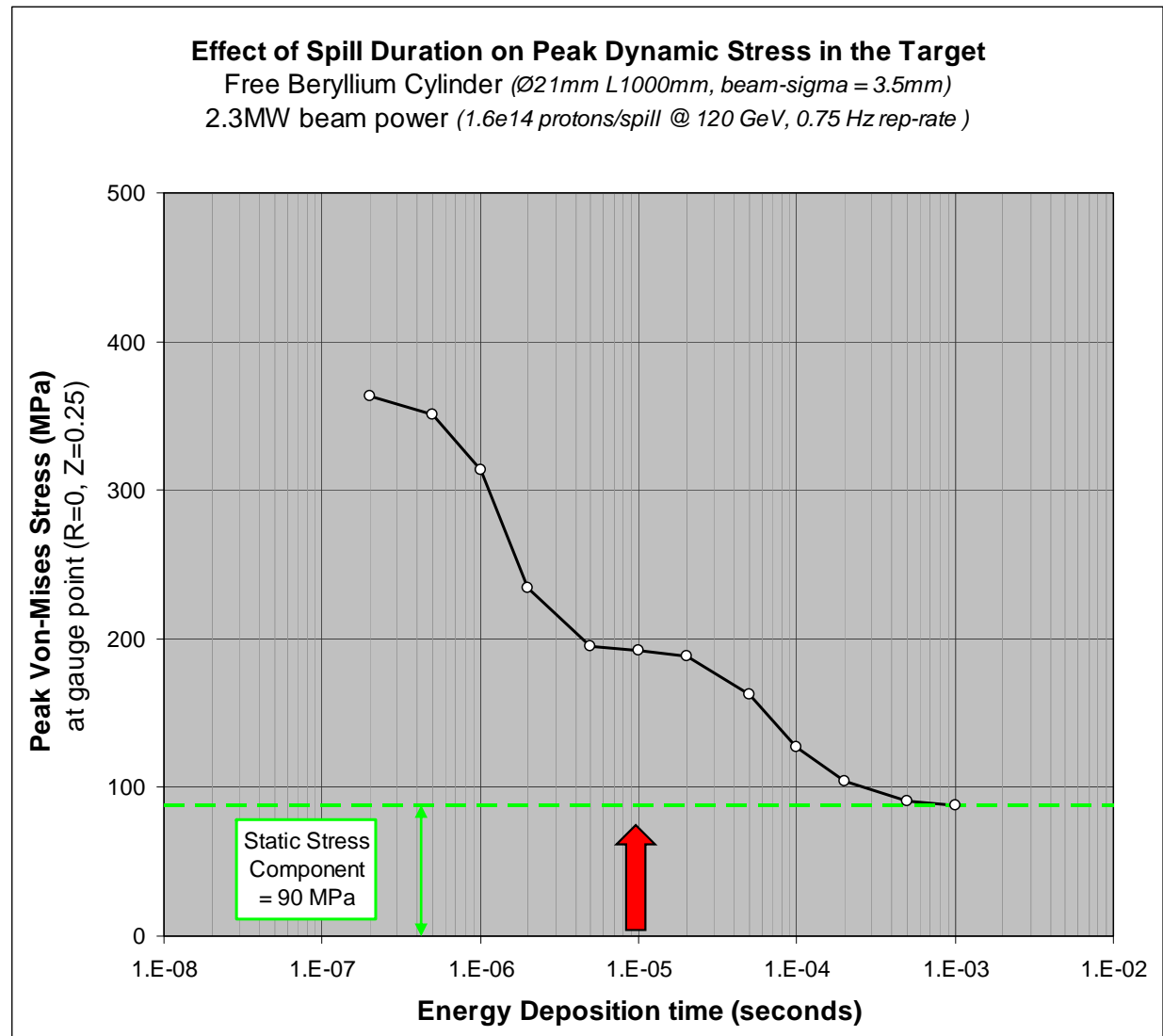
# LBNE Beryllium rod target: Stress-Waves



*Effect of beam spill time on the peak dynamic stress in the target*

# LBNE Beryllium rod target: Stress-Waves

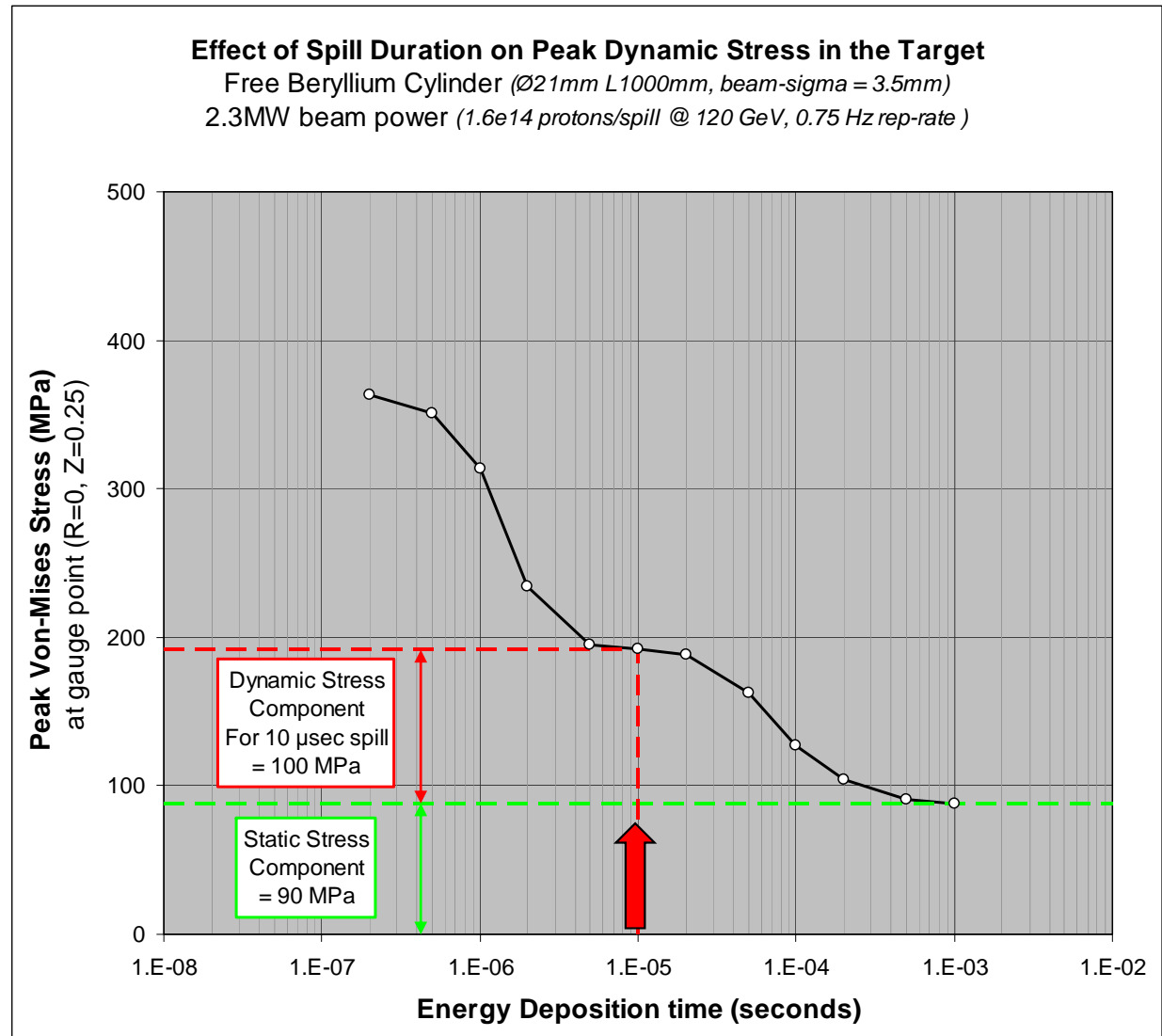
- “static” stress component is due to thermal gradients
  - Independent of spill time



*Effect of beam spill time on the peak dynamic stress in the target*

# LBNE Beryllium rod target: Stress-Waves

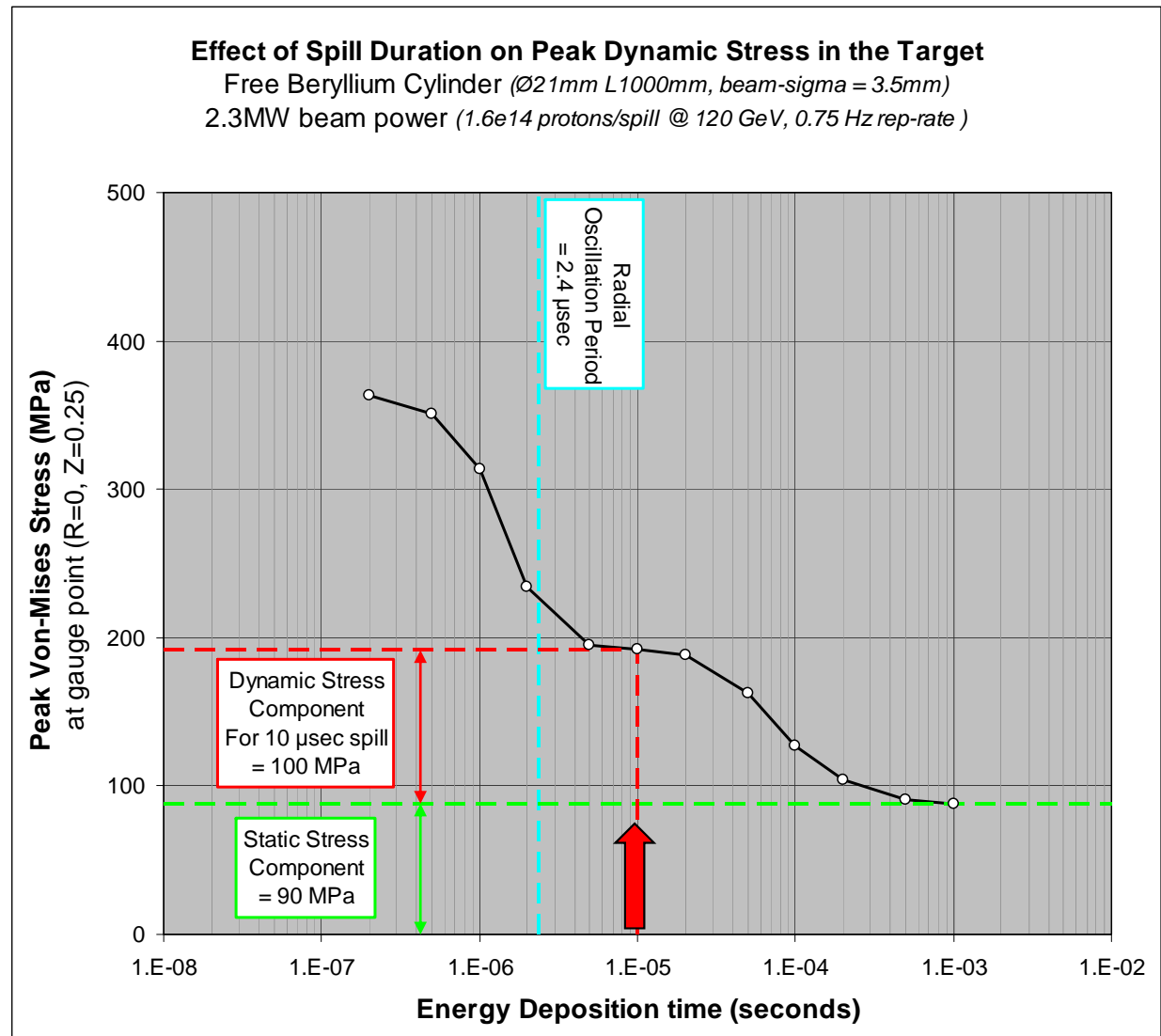
- “static” stress component is due to thermal gradients
  - Independent of spill time
- “dynamic” stress component is due to stress waves
  - Spill time dependent



*Effect of beam spill time on the peak dynamic stress in the target*

# LBNE Beryllium rod target: Stress-Waves

- “static” stress component is due to thermal gradients
  - Independent of spill time
- “dynamic” stress component is due to stress waves
  - Spill time dependent
- $T_{\text{spill}} > \text{Radial period}$ 
  - Radial stress waves are not significant

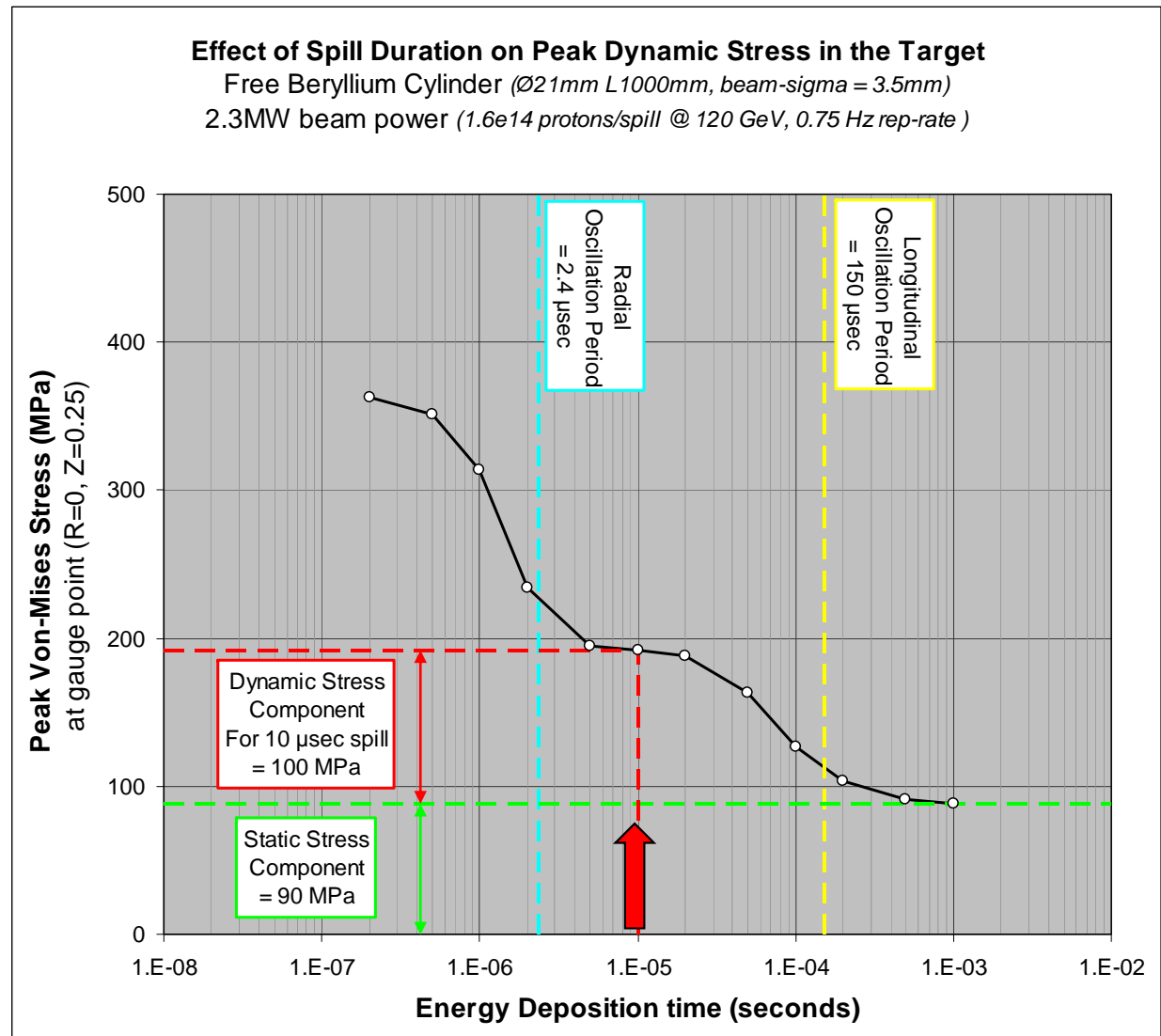


*Effect of beam spill time on the peak dynamic stress in the target*



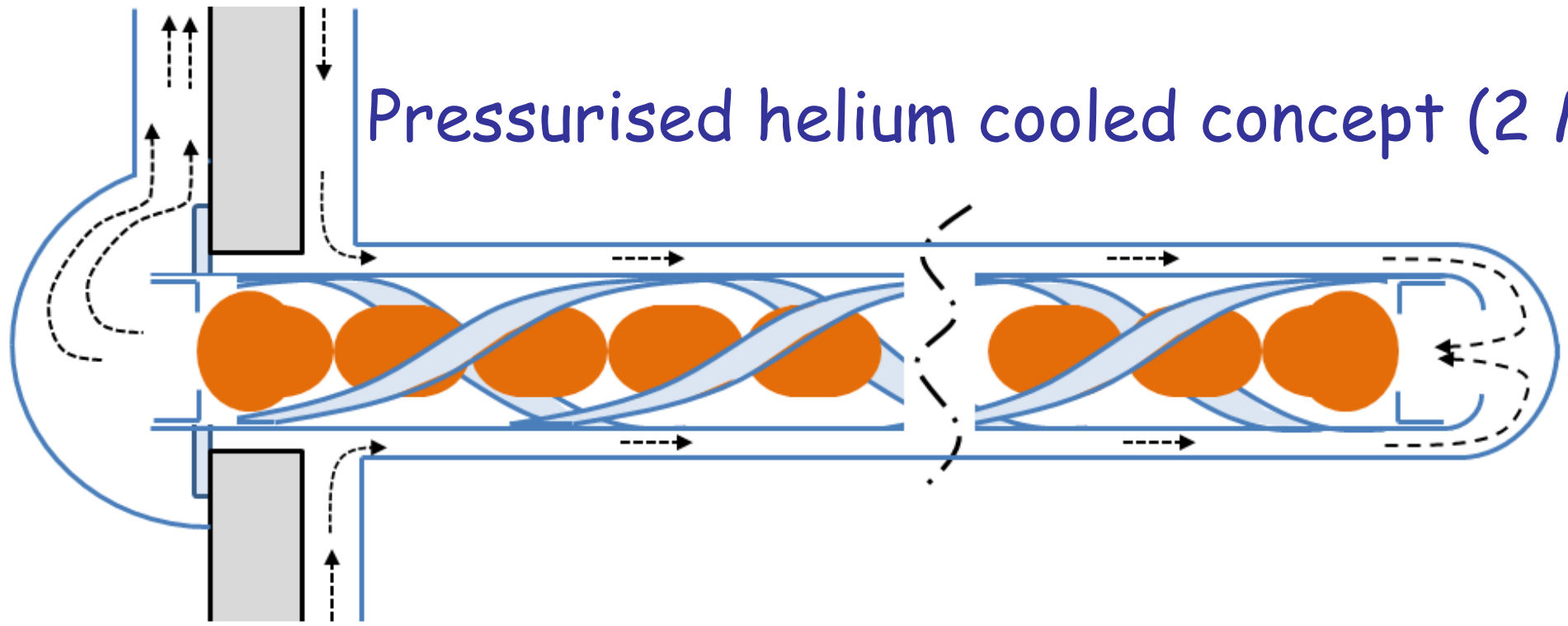
# LBNE Beryllium rod target: Stress-Waves

- “static” stress component is due to thermal gradients
  - Independent of spill time
- “dynamic” stress component is due to stress waves
  - Spill time dependent
- $T_{spill} > T_{radial}$  period
  - Radial stress waves are not significant
- $T_{spill} < T_{longitudinal}$  period
  - Longitudinal stress waves are important!

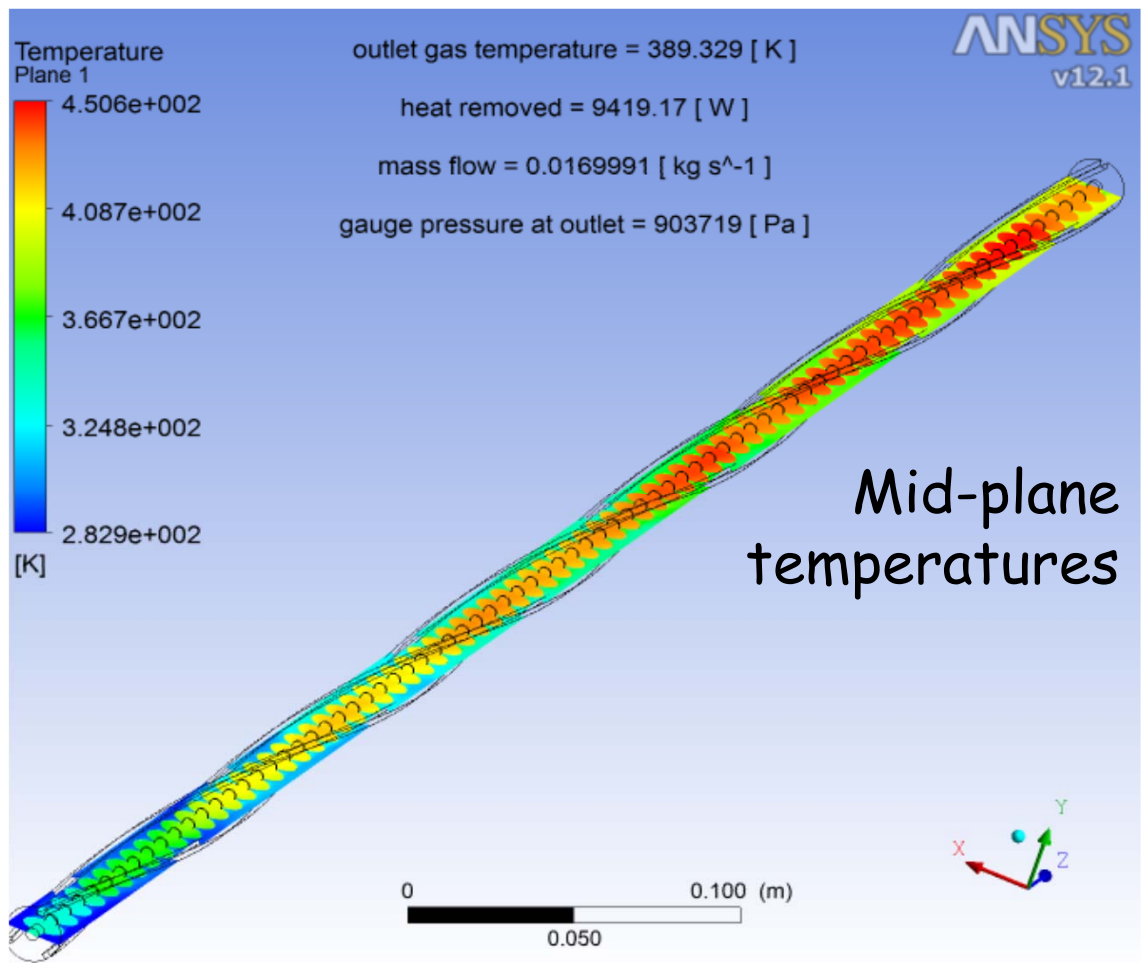
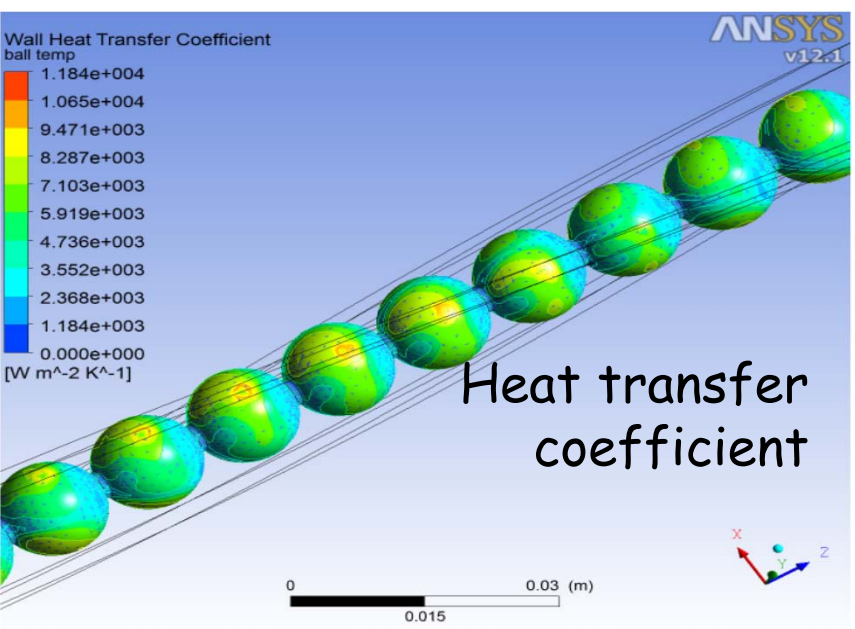
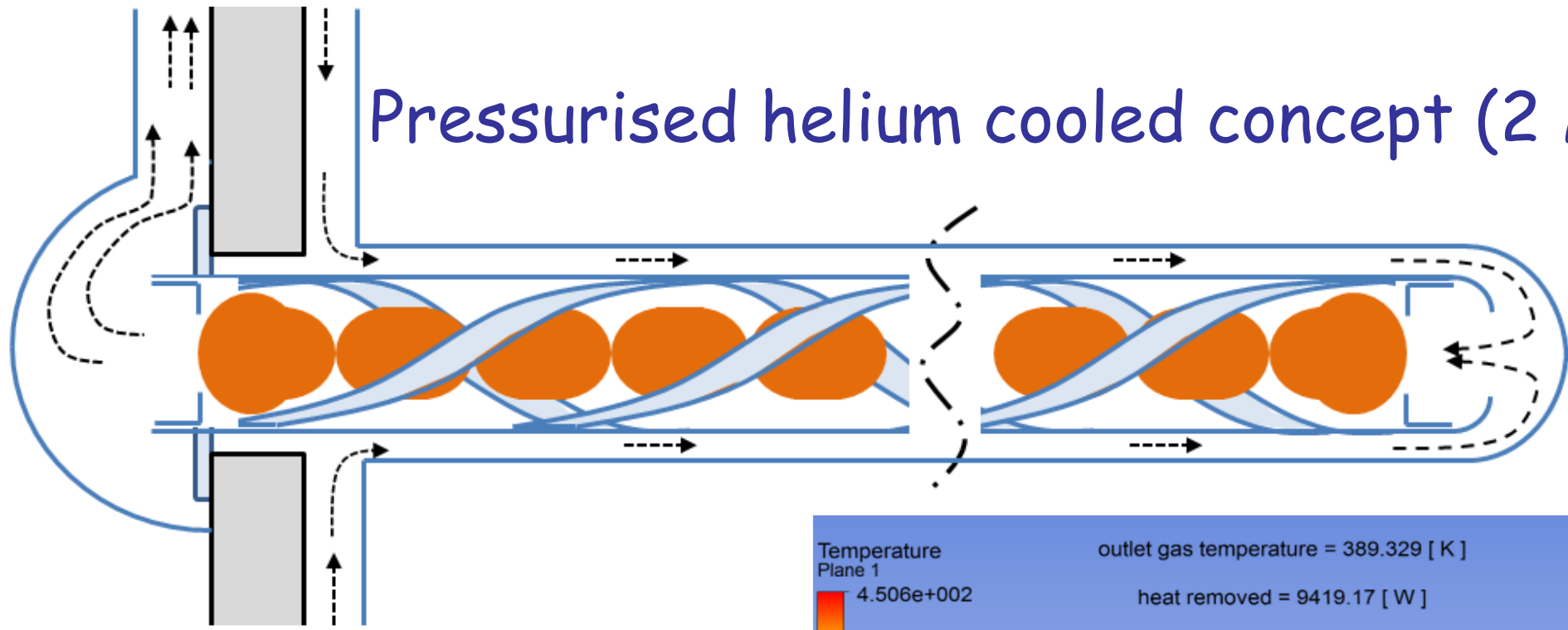


*Effect of beam spill time on the peak dynamic stress in the target*

# Pressurised helium cooled concept (2 MW)



# Pressurised helium cooled concept (2 MW)



Otto Caretta & Tristan Davenne

# Pressurised helium cooled concept (2 MW)



Beryllium sphere diameter	13 mm
Beam sigma	2.2 mm
Helium mass flow rate	17 g/s
Inlet helium pressure	11.1 bar
Outlet helium pressure	10 bar
Inlet velocity	40 m/s
Maximum velocity	185 m/s
Total heat load	9.4 kW
Maximum beryllium temperature	178 C
Helium temperature rise, $\Delta T$ ( $T_{in} - T_{out}$ )	106 C

# Conclusions: 'Divide and Rule' for increased power

Dividing material is favoured since:

- Better heat transfer
- Lower static thermal stresses
- Lower dynamic stresses from intense beam pulses

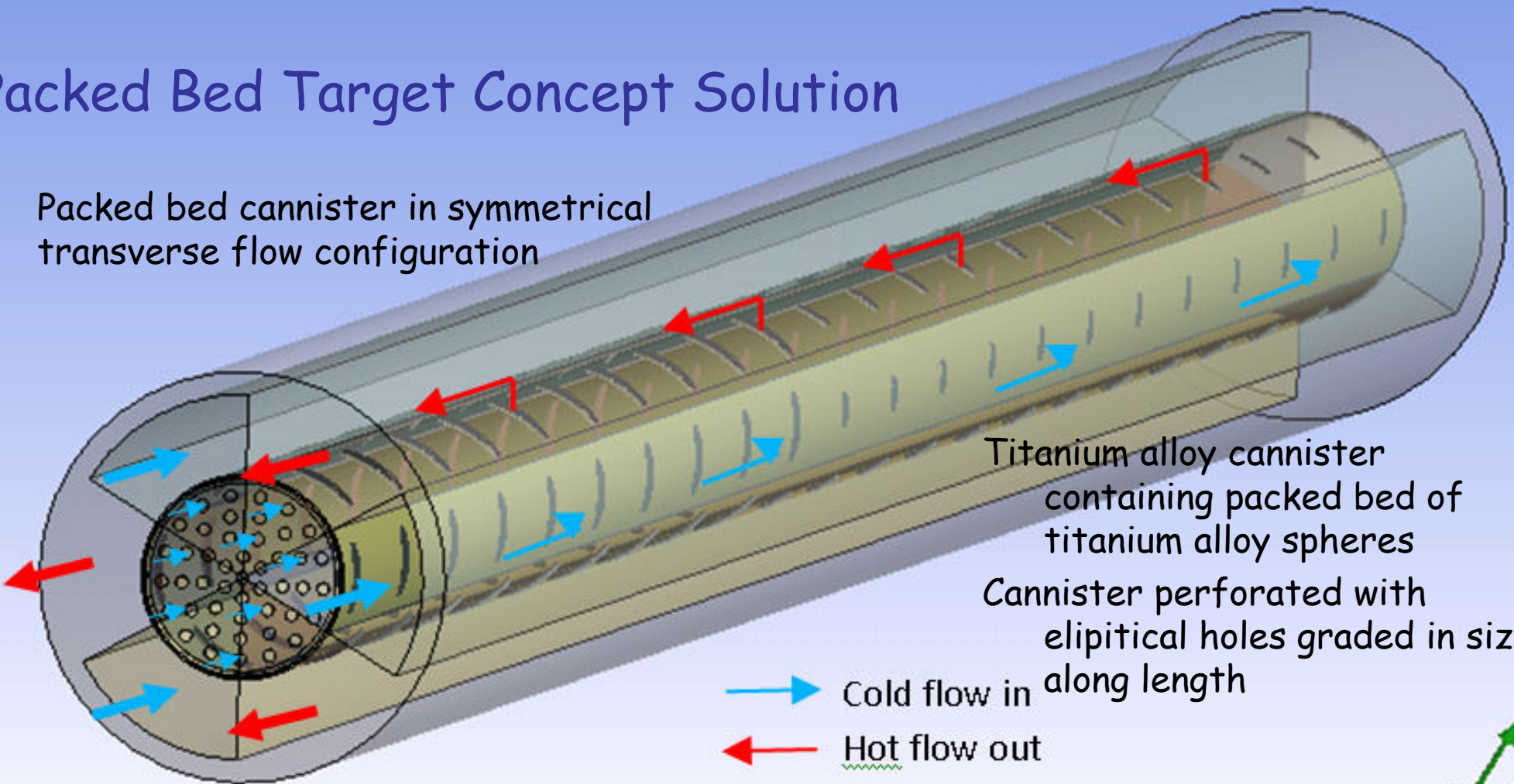
Helium cooling is favoured (cf water) since:

- No 'water hammer' or cavitation effects from pulsed beams
- Lower coolant activation, no radiolysis
- Negligible pion absorption - coolant can be within beam footprint
- For graphite, higher temperatures anneal radiation damage

**Static, low-Z target concepts proposed**

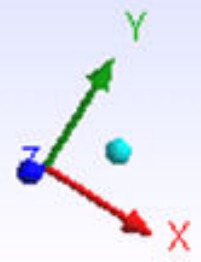
# Packed Bed Target Concept Solution

Packed bed cannister in symmetrical transverse flow configuration

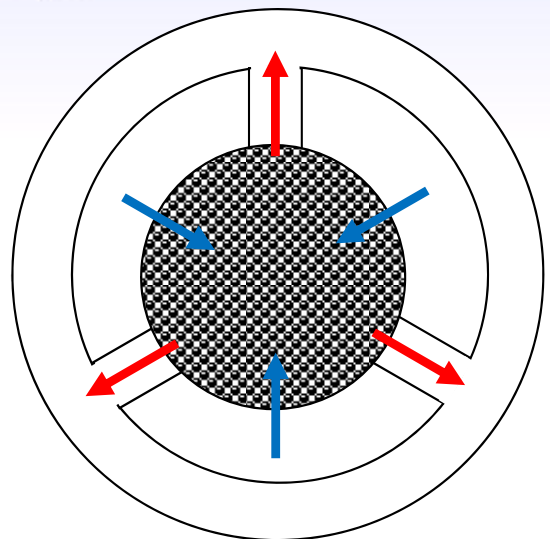


Titanium alloy cannister containing packed bed of titanium alloy spheres  
Cannister perforated with elliptical holes graded in size along length

→ Cold flow in  
← Hot flow out



T. Davenne



- Model Parameters**
- Proton Beam Energy = 4.5GeV
  - Beam sigma = 4mm
  - Packed Bed radius = 12mm
  - Packed Bed Length = 780mm
  - Packed Bed sphere diameter = 3mm
  - Packed Bed sphere material : Titanium Alloy
  - Coolant = Helium at 10 bar pressure

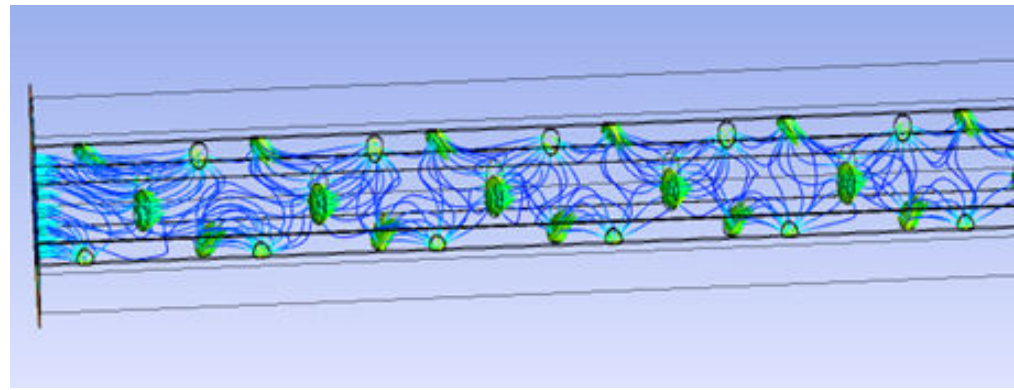
## Particle bed advantages

- Large surface area for heat transfer
- Coolant can pass close to maximum energy deposition
- High heat transfer coefficients
- Low quasi static thermal stress
- Low dynamic stress (for oscillation period  $\ll$  beam spill time)

## ... and challenges

- High pressure drops, particularly for long thin superbeam target geometry
  - Need to limit gas pressure for beam windows
- Transverse flow reduces pressure drops - but
  - Difficult to get uniform temperatures and dimensional stability of container

# Packed Bed Model (FLUKA + CFX v13)



## Streamlines in packed bed

Packed bed modelled as a porous domain

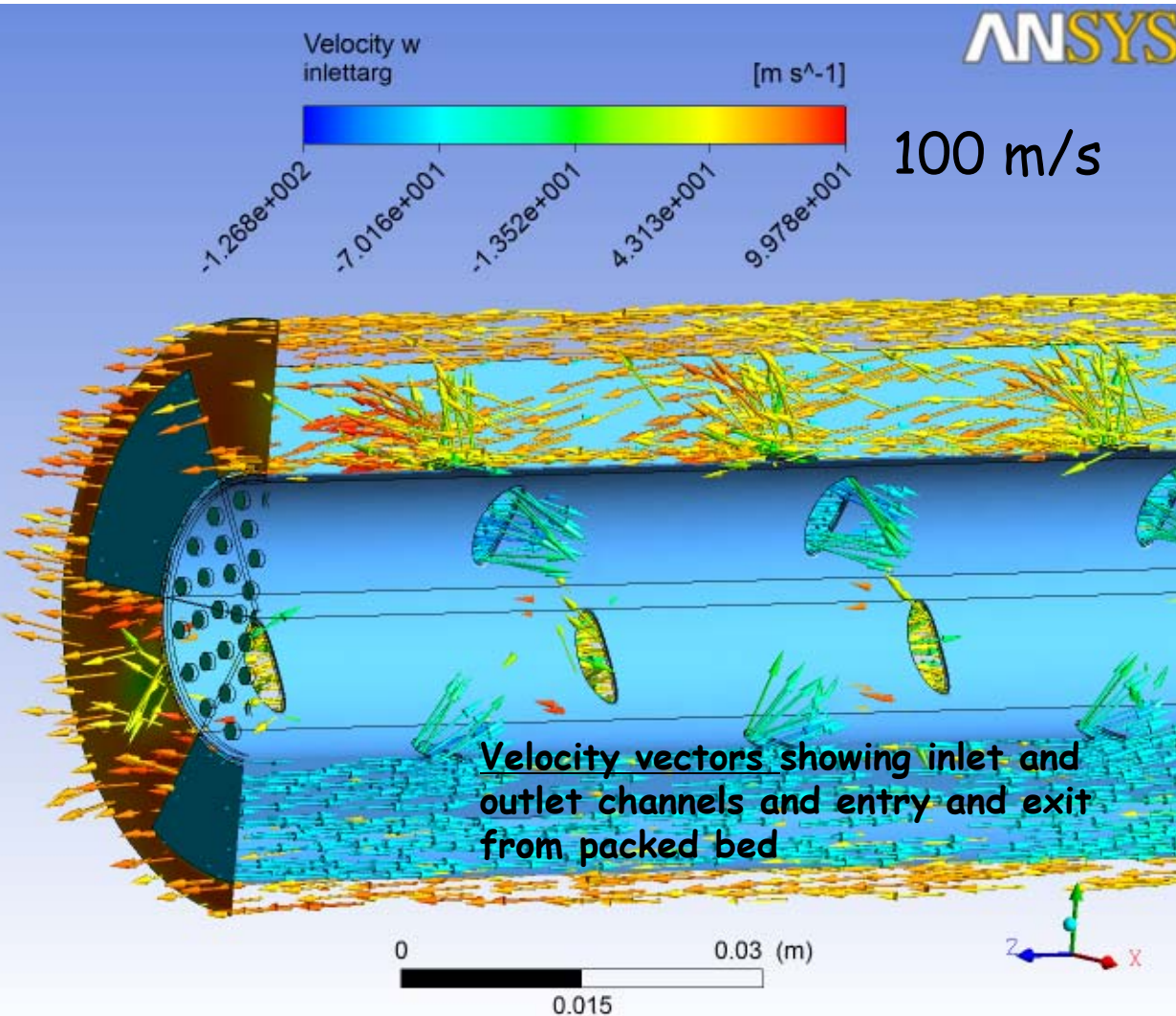
Permeability and loss coefficients calculated from Ergun equation (dependant on sphere size)

Overall heat transfer coefficient accounts for sphere size, material thermal conductivity and forced convection with helium

Interfacial surface area depends on sphere size

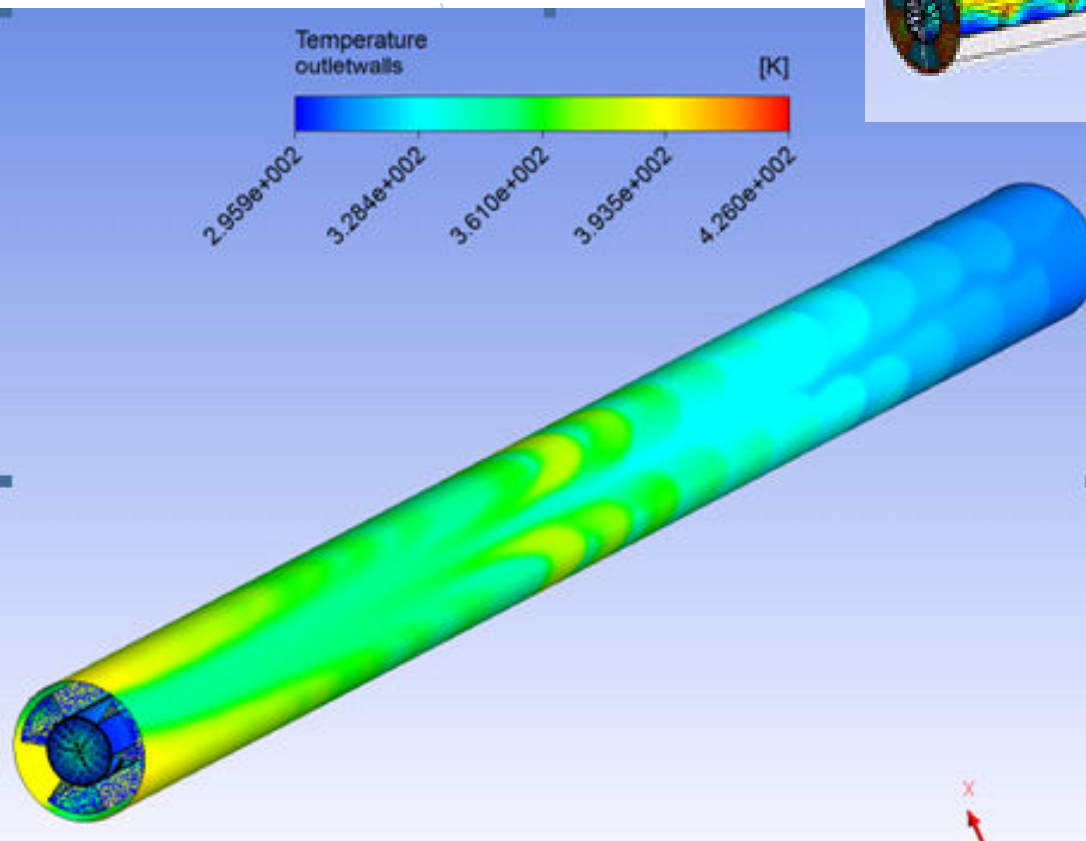
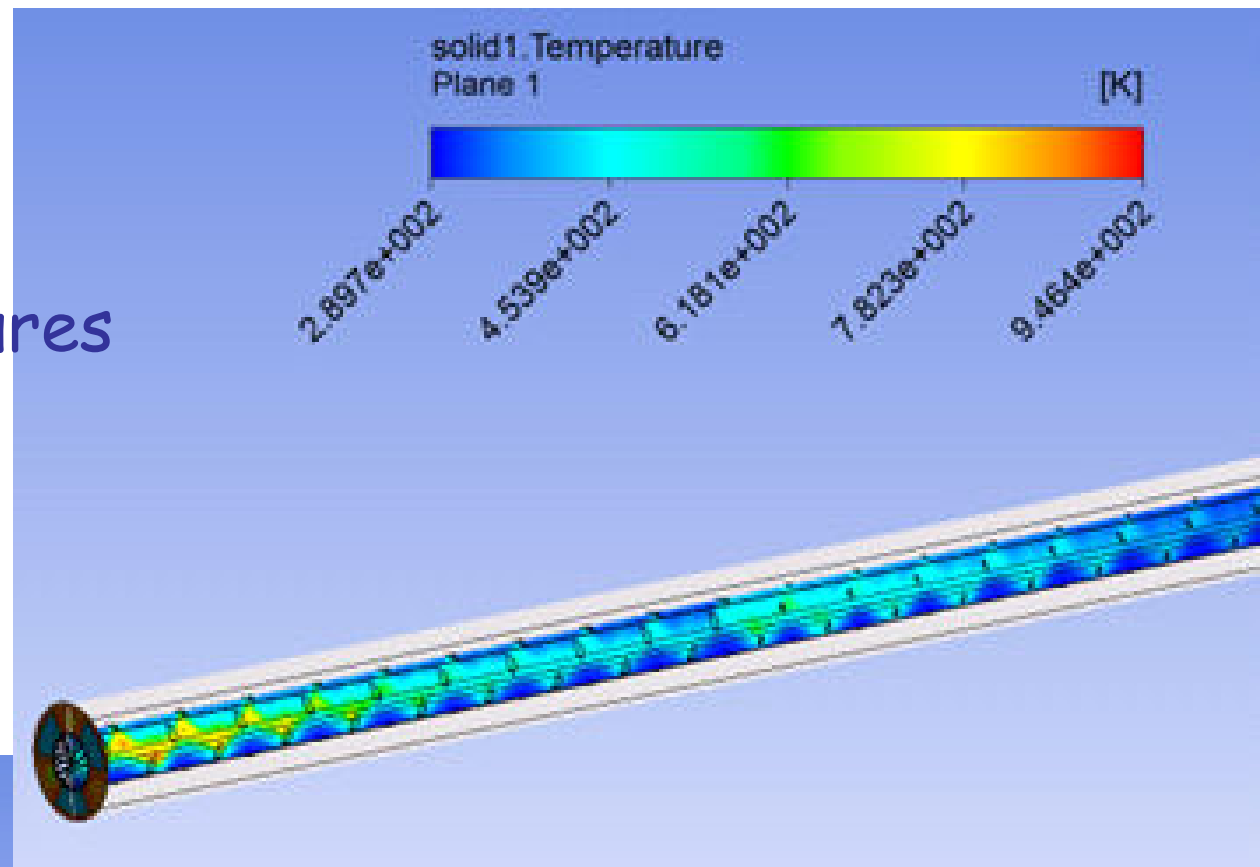
Acts as a natural diffuser flow spreads through target easily

T. Davenne





# Packed Bed temperatures



## Outer Can Surface Temp

Almost Symmetric Temperature contours  
Maximum surface Temperature = 426K =  
153° C

NB windows not included in model yet  
- Double skin Be should withstand both  
heat and pressure loads

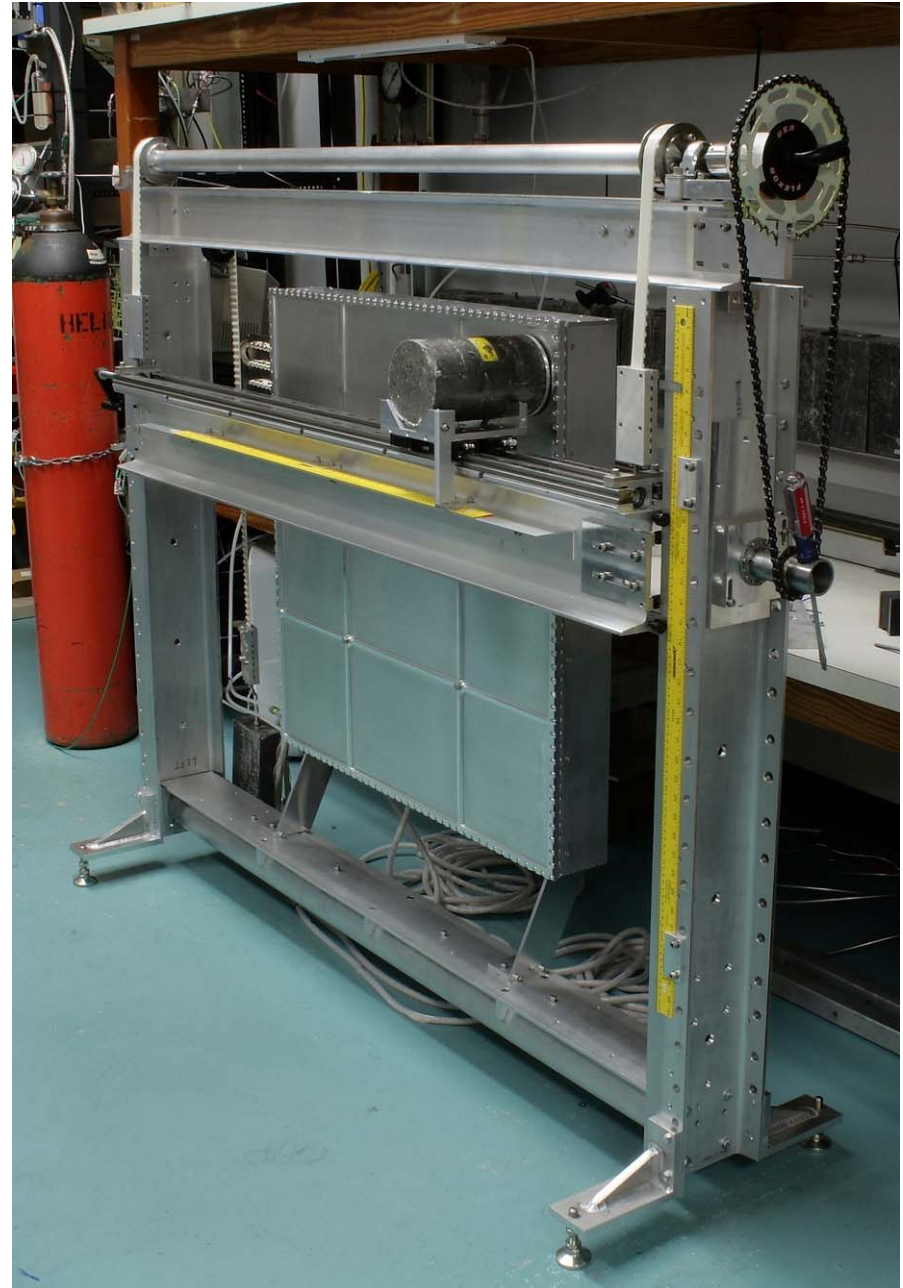


# Future LBNE Collaborative Opportunities?

- Further prototyping on **LBNE 700 kW target** (Be or Ti outer tube replacing Al)
  - Eventual manufacture of spare target?
  - Requires good design/analysis and manufacturing capabilities
- Pre-conceptual scoping of **2.3 MW target** (graphite or Be)
  - Requires good design/analysis capabilities
- Conceptual design and prototyping of **LBNE beam windows**:
  - Especially for 2+ MW beam power
  - Possibility of **Decay Pipe windows** (challenge even at 700 kW)
  - Requires good design/analysis capabilities
- **Hadron Monitor** design and prototyping (eventual manufacture?)
  - Need new radiation hardened version for LBNE
  - Requires good design/analysis and manufacturing capabilities

## Hadron Monitor

- Measures position and intensity of secondary particles at the end of the decay pipe (in absorber shield pile)
- LBNE has shorter decay pipe than NuMI
  - More heating
  - More radiation damage
  - 5x better resolution
- Current conceptual design is parallel plate ionization chambers with low pressure helium
- Used during beam/target/horn alignment & diagnostic scans and monitoring degradation of target material
- Good project to take from design to construction



NuMI Hadron Monitor being calibrated at University of Texas 4/4/13

# Target collaboration for the first Neutrino Superbeam

- Whichever facility - LBNE/LBNO/T2HK - is first to be approved for construction/upgrade to operate in the MW region, there will be little time to develop a target system
- There is very significant commonality/synergy between the target/horn system and target station for all proposed facilities
- Now is a good time to get ready by collaborating over the necessary research and development
- Common challenges/areas for collaboration:
  - Target station design (T2K already constructed for 3-4 MW)
  - Beam window
  - Low Z target, 1-3  $\lambda$  long
    - heat transfer, stress waves, lifetime - radiation damage effects, performance optimisation
  - Integration of target with horn to capture low energy pions
  - Horn - lifetime, radiation damage effects
  - Instrumentation - OTR, beam