

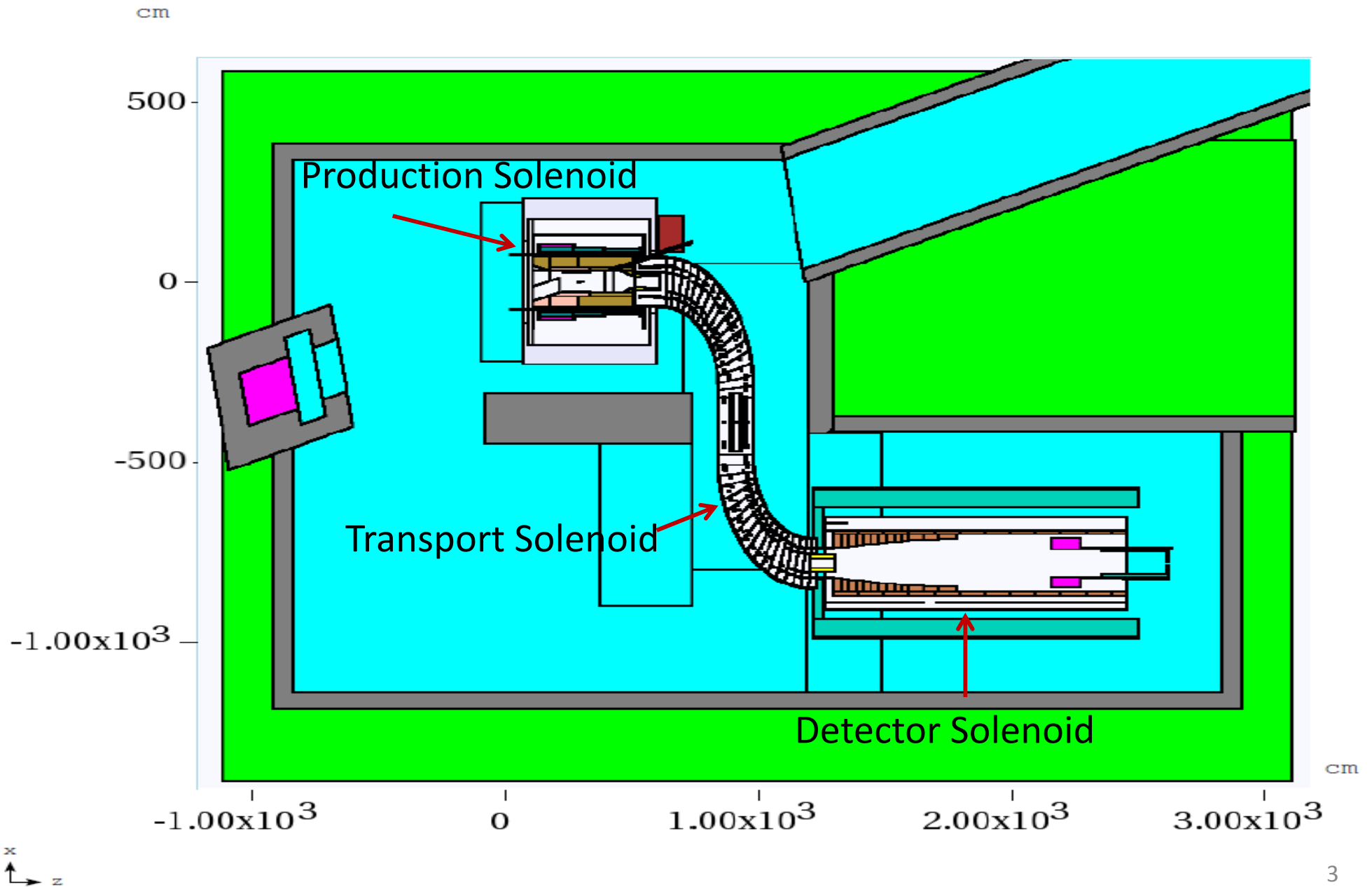
# Radiation studies for Mu2e magnets

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Fermilab  
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# Outline

- Requirements on radiation quantities for Mu2e cryogenics
  - Dynamic heat load
  - Power density
  - Absorbed dose
  - DPA
- Production Solenoid Heat and Radiation Shield design. MARS15 modeling
  - Shape optimization
  - Material optimization
  - Current model
- Preliminary Mu2e@ProjectX PS design
- Conclusions

# Mu2e hall MARS15 model

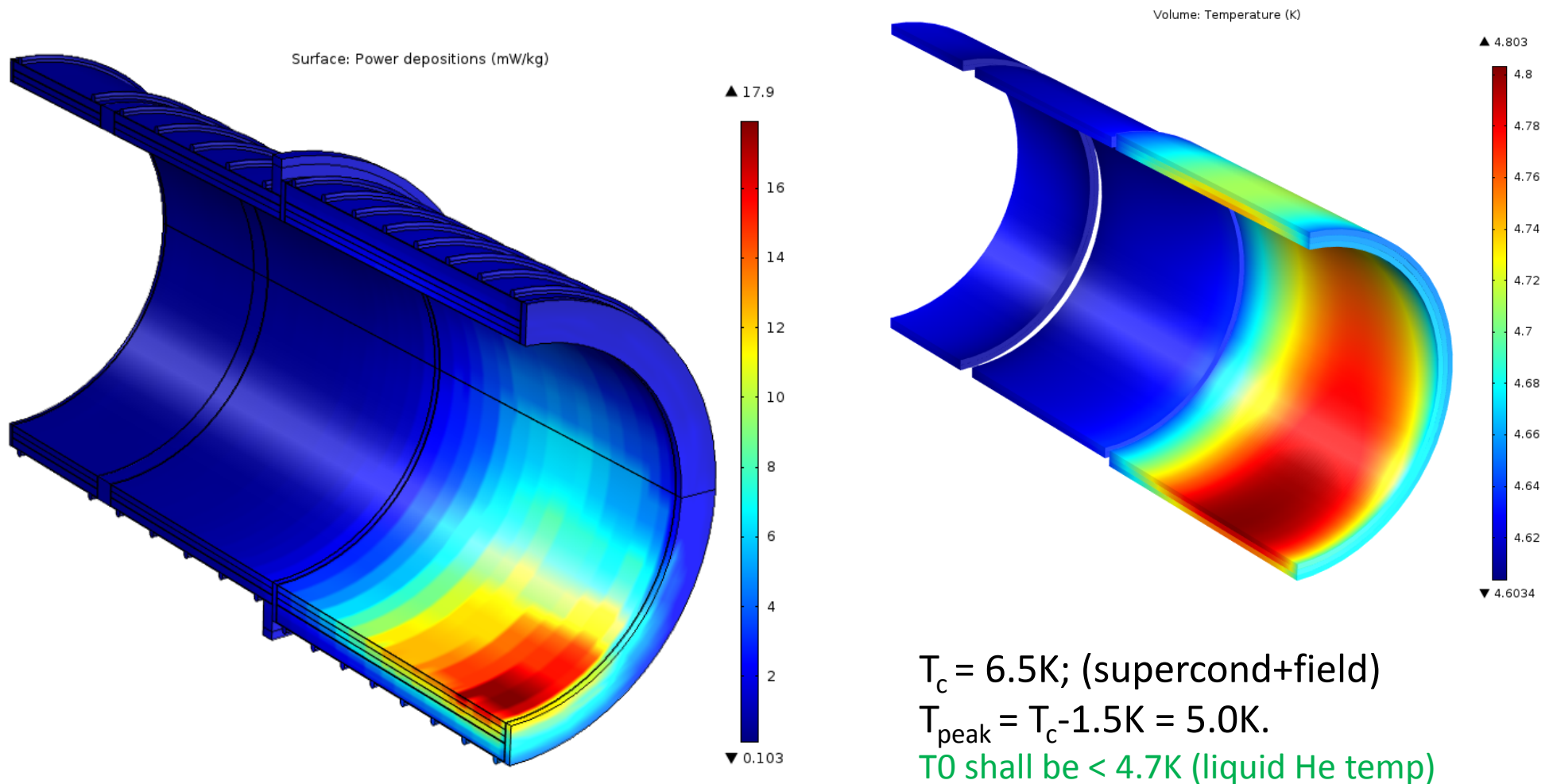


# Requirements to Heat and Radiation Shield

- Absorber (heat and radiation shield) is intended to prevent radiation damage to the magnet coil material and ensure quench protection and acceptable heat loads for the lifetime of the experiment
  - Total dynamic heat load on the coils (100 W)
  - Peak power density in the coils
  - Peak radiation dose to the insulation and epoxy
  - DPA to describe how radiation affects the electrical conductivity of metals in the superconducting cable

# Requirements.

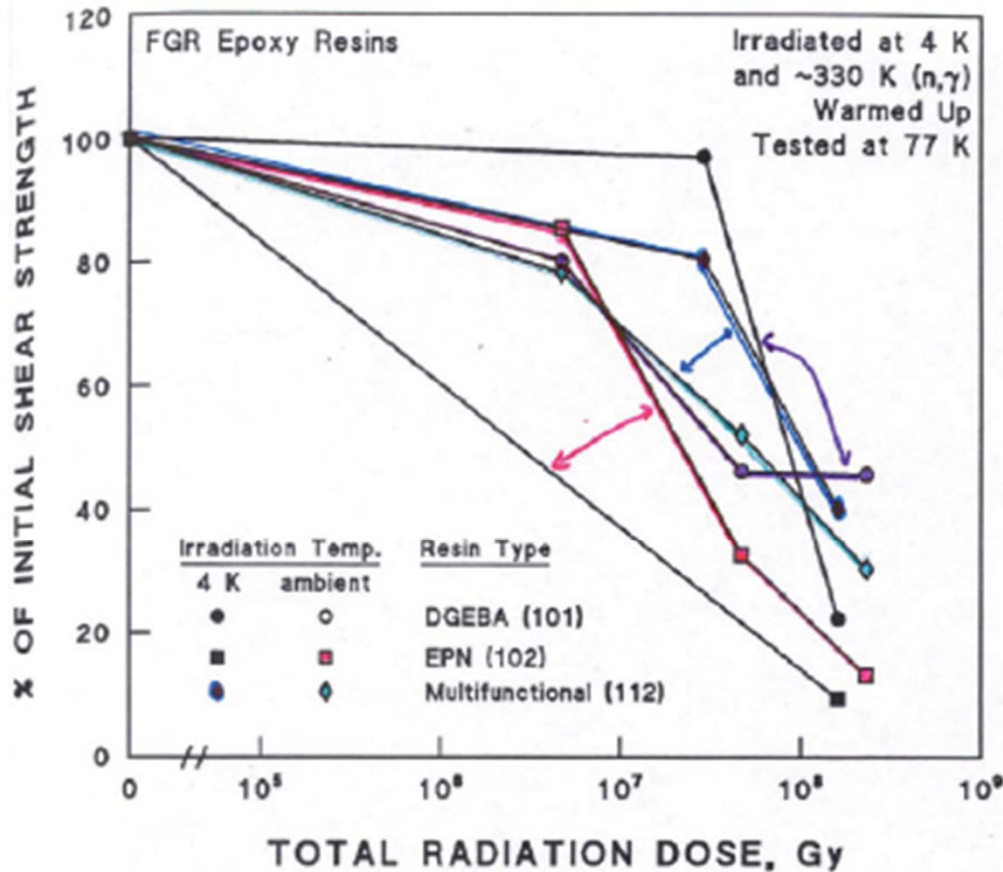
## Peak power density



See talk of Vadim Kashikhin

Absorbed dose 350kGy/yr (0.017 mW/g)

# Requirements. Absorbed dose



7 MGy before 10% degradation of shear modulus.

350 kGy/yr -> 20 years lifetime

Radiation Hard Coils, A. Zeller et al, 2003, <http://supercon.lbl.gov/WAAM>

Figure 1.25. A comparison of the shear strengths of three types of reinforced epoxy resins that were reactor-irradiated at both 4 K and at ambient temperature. See text for differences in the fast neutron spectrum in the two reactors. Data from Munshi [1991]. (Supplementary Tables A. 3-3 and A. 8-4.)

# Requirements. DPA

$$RRR(DPA) = \frac{\rho_{hi}}{\rho_0 + \Delta\rho(DPA)}$$

$$\rho_{hi} = 2.7E-6 \Omega \cdot cm$$

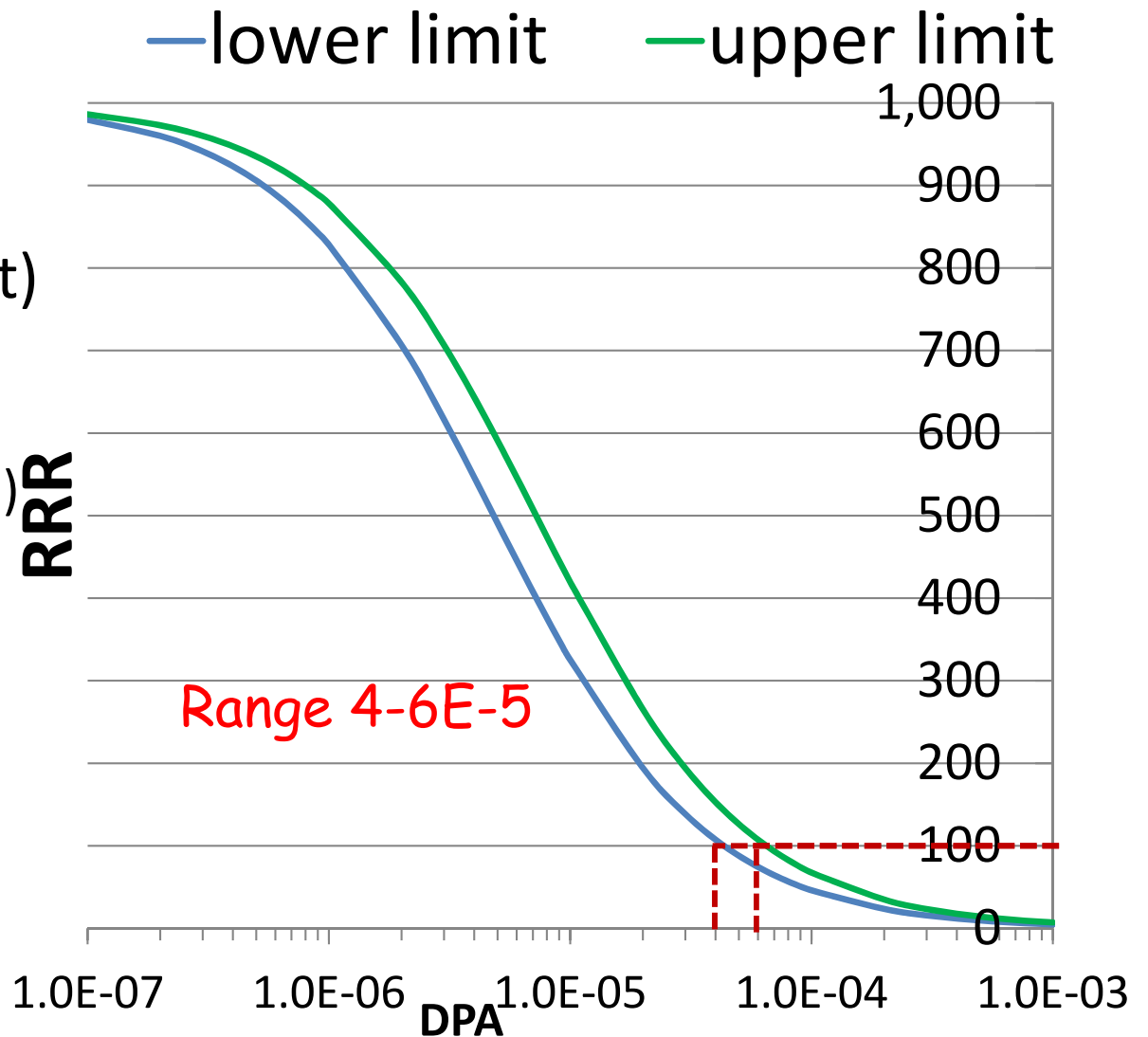
$$\rho_0 = \frac{\rho_{hi}}{1000} \text{ (Mu2e requirement)}$$

$\Delta\rho$  – from KEK measurement  
(RRR degradation from 457 to 245)

$\frac{\Delta\rho}{DPA}$  - DPA using NRT model with  
correction for defect production  
efficiency  $\eta$

$$\eta = \frac{N_D}{N_{NRT}}; \quad 0.357 - 0.535$$

Broeders, Konobeyev, 2004



# MECO design DPA analysis

DPA, yr<sup>-1</sup>

1.0E-03

1.0E-04

1.0E-05

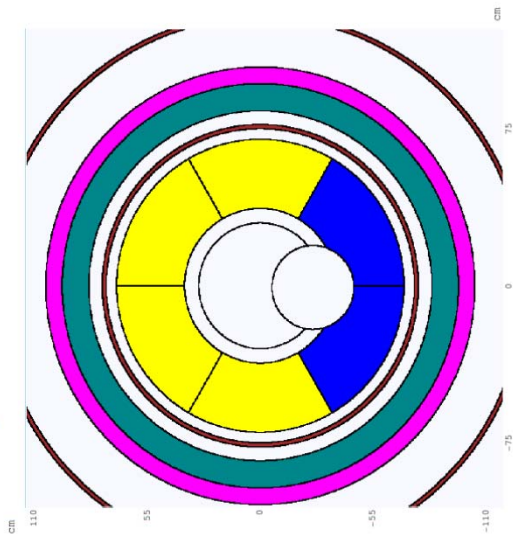
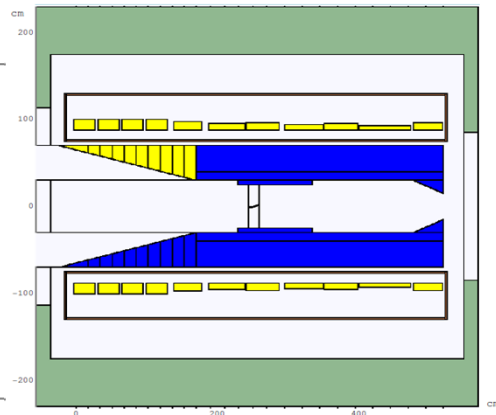
1.0E-06

0 100 200 300 400 500 600 Z, cm

Mu2e solutions:

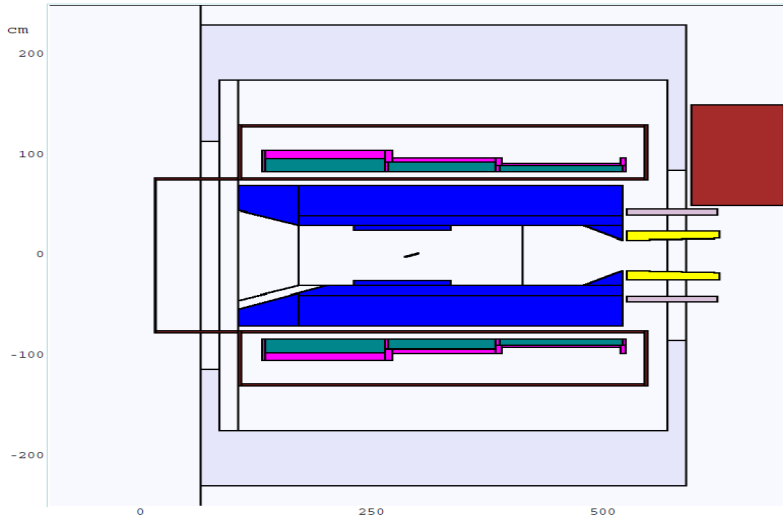
- Taper part shape optimization
- Groove (target position change)

@ 50 kW

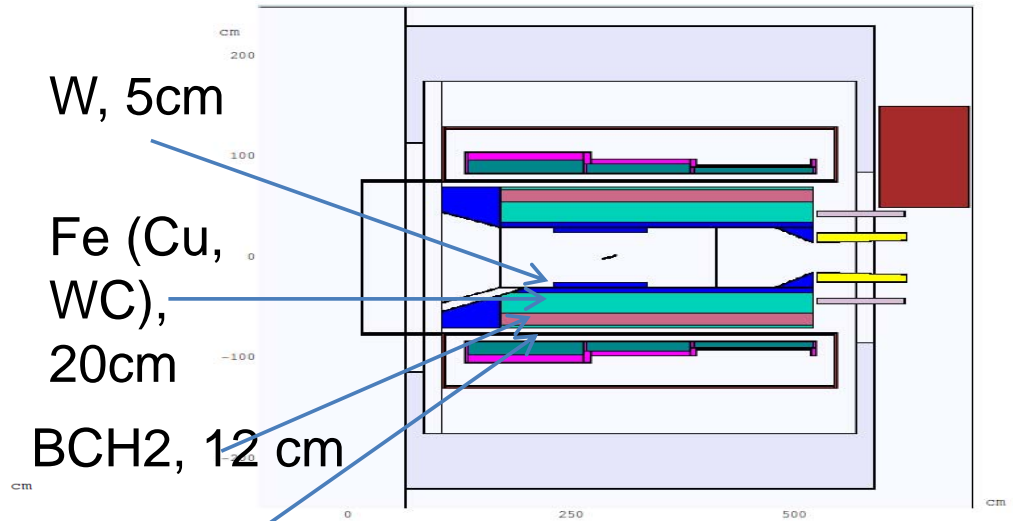




# Material optimization

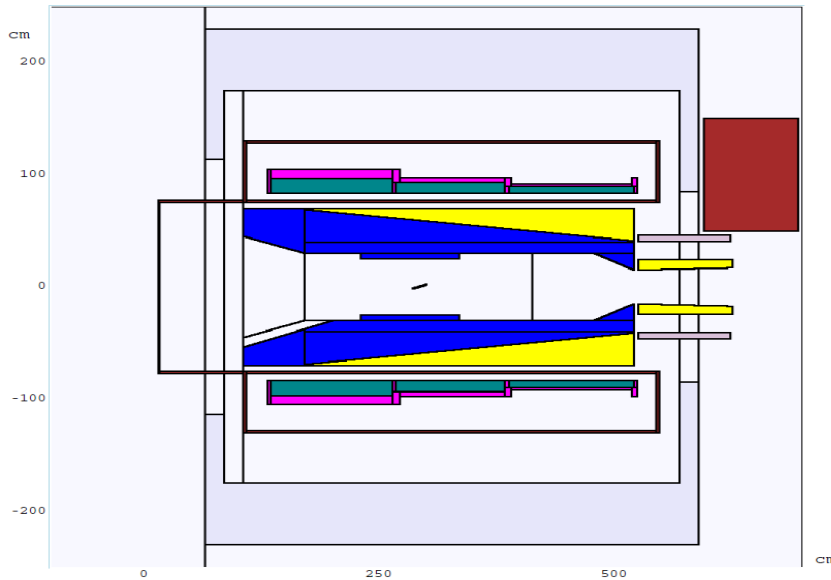


Tungsten, WC, U-238



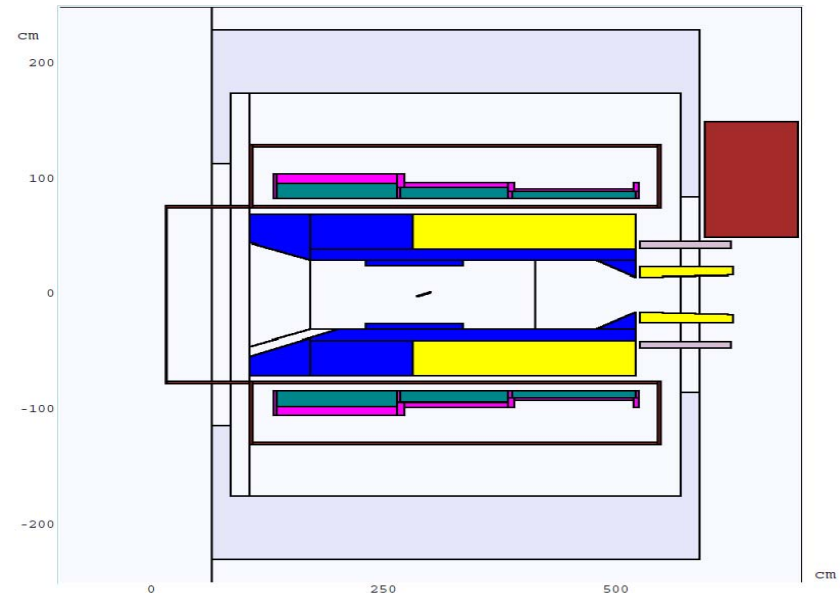
Fe (Cu, Cd), 3cm

5 multilayer cases

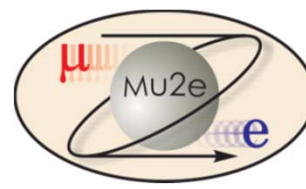


Tungsten/copper

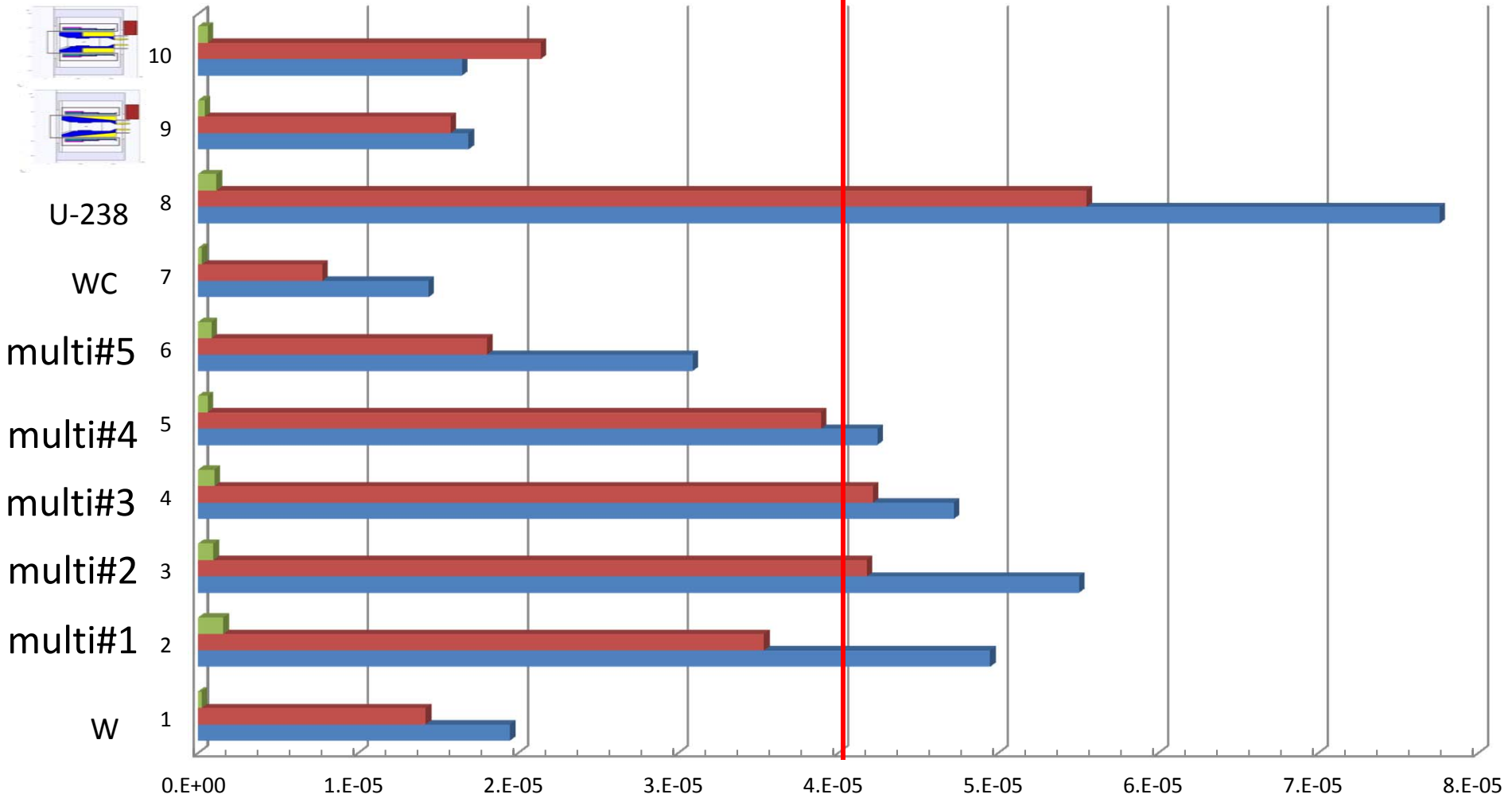
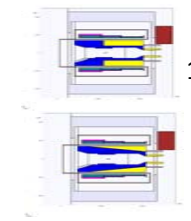
Cases #1-#10



Tungsten/copper

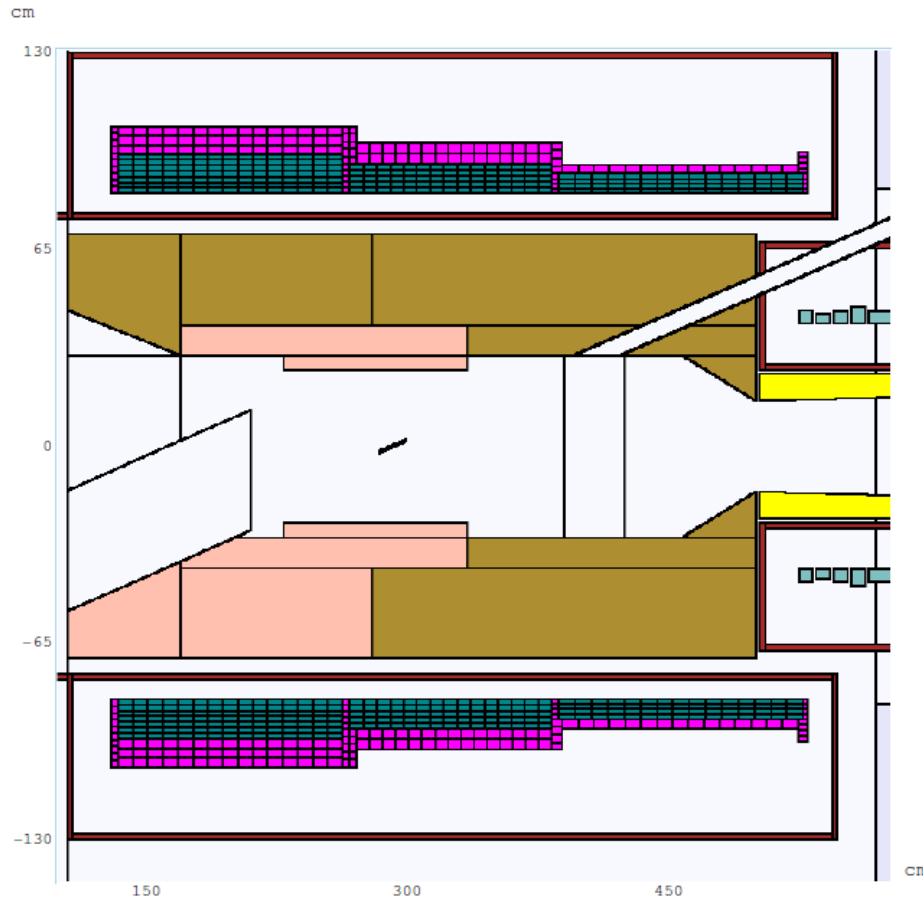


# Peak DPA in Coils, yr<sup>-1</sup>

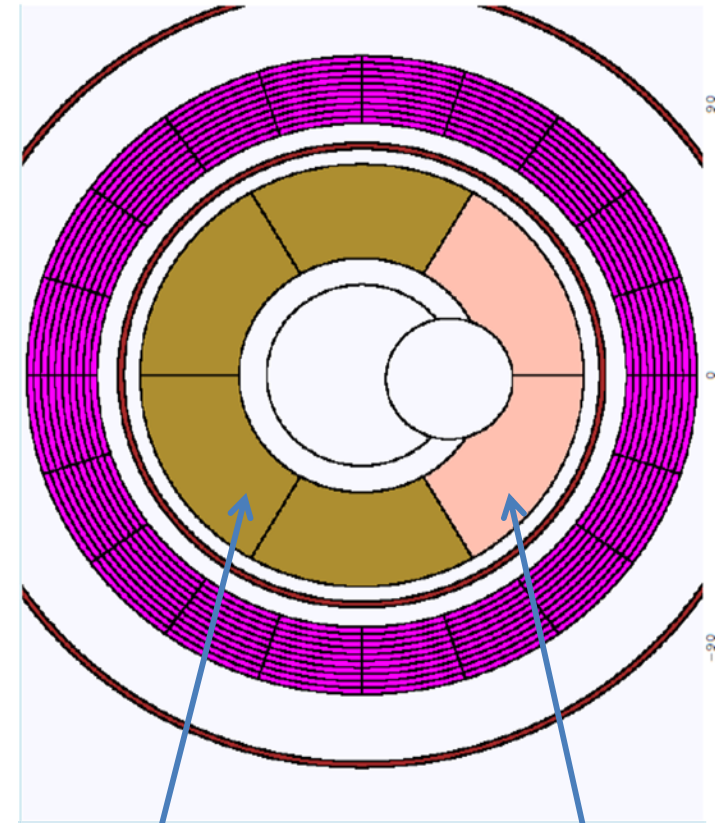


	1	2	3	4	5	6	7	8	9	10
3a	2.23E-07	1.59E-06	9.62E-07	1.02E-06	5.94E-07	8.54E-07	2.42E-07	1.16E-06	4.18E-07	5.93E-07
2a	1.42E-05	3.54E-05	4.18E-05	4.22E-05	3.89E-05	1.81E-05	7.77E-06	5.55E-05	1.58E-05	2.14E-05
1a	1.95E-05	4.95E-05	5.50E-05	4.72E-05	4.25E-05	3.09E-05	1.44E-05	7.76E-05	1.69E-05	1.65E-05

# HRS model for nominal beam power



8300 zones for thermal analysis



Thresholds:

$\mu$ , ch.hadr  $> 1$  MeV, neutrons  $> 0.001$  eV

gamma  $> 200$  keV,  $e^+$   $> 200$  keV

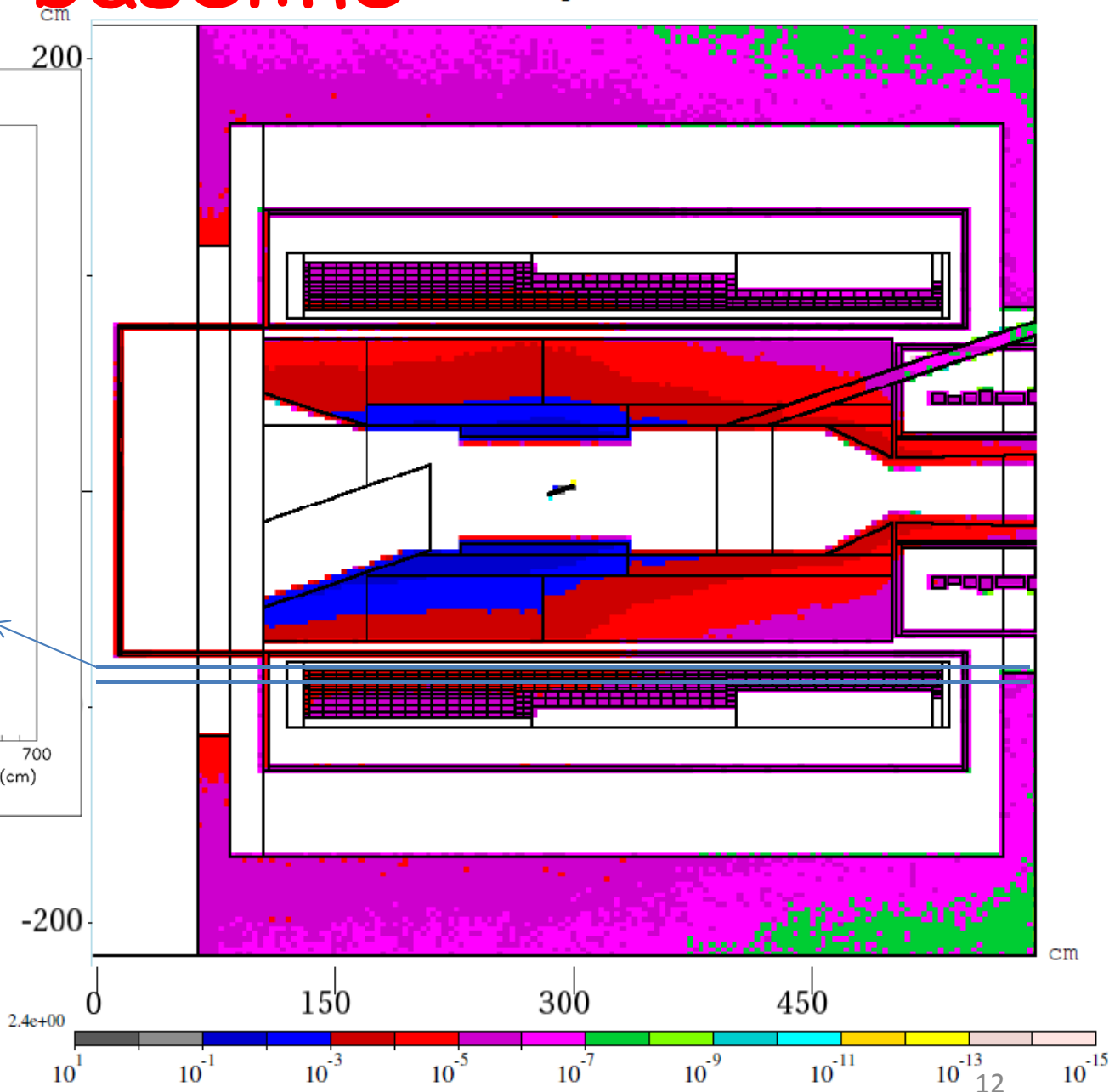
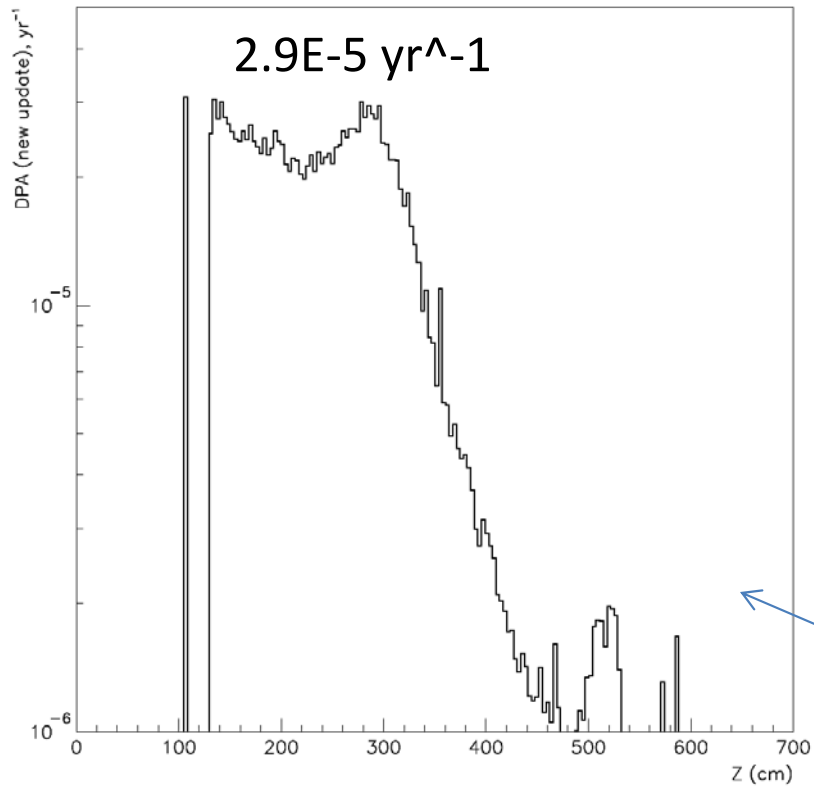
Wedges are used in the downstream part of HS

# DPA for nominal beam power baseline

DPA, yr<sup>-1</sup>

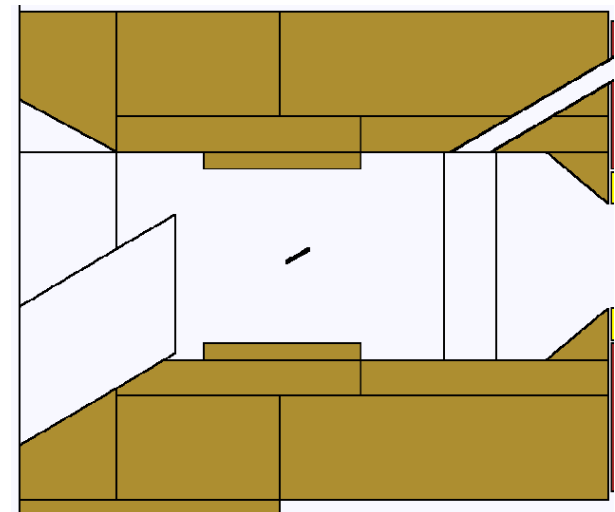
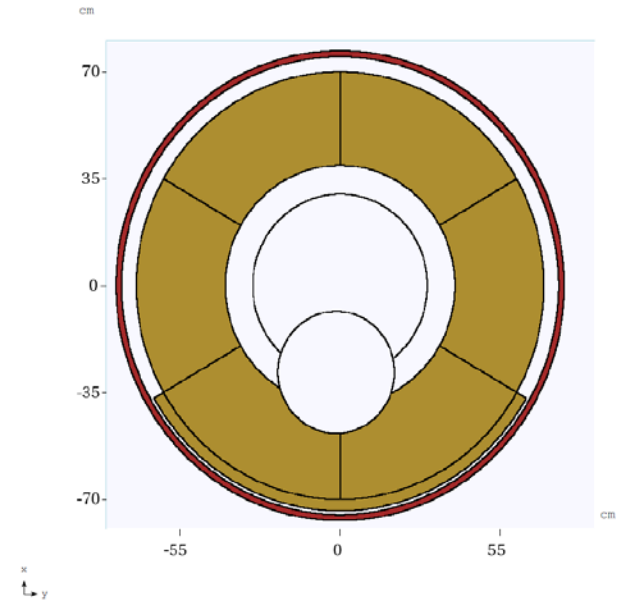
Limit 4-6E-5 yr<sup>-1</sup>

2.9E-5 yr<sup>-1</sup>



# Changes to the current model

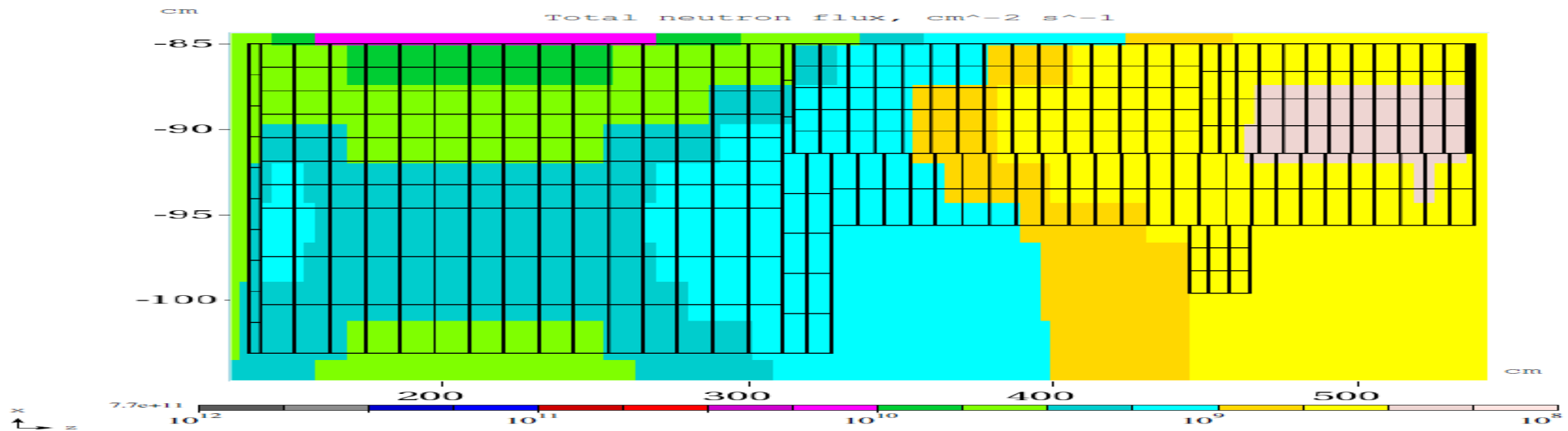
- All-bronze absorber (7.64 g/cm<sup>3</sup>)
- The exclusive model combination LAQGSM @ > A/65+1 GeV and CEM below is used
- New coil geometry
- Concrete yoke
- Fields V7 MIN (4.1 T) and MAX (5.0 T)
- Beam power 1/3 of nominal



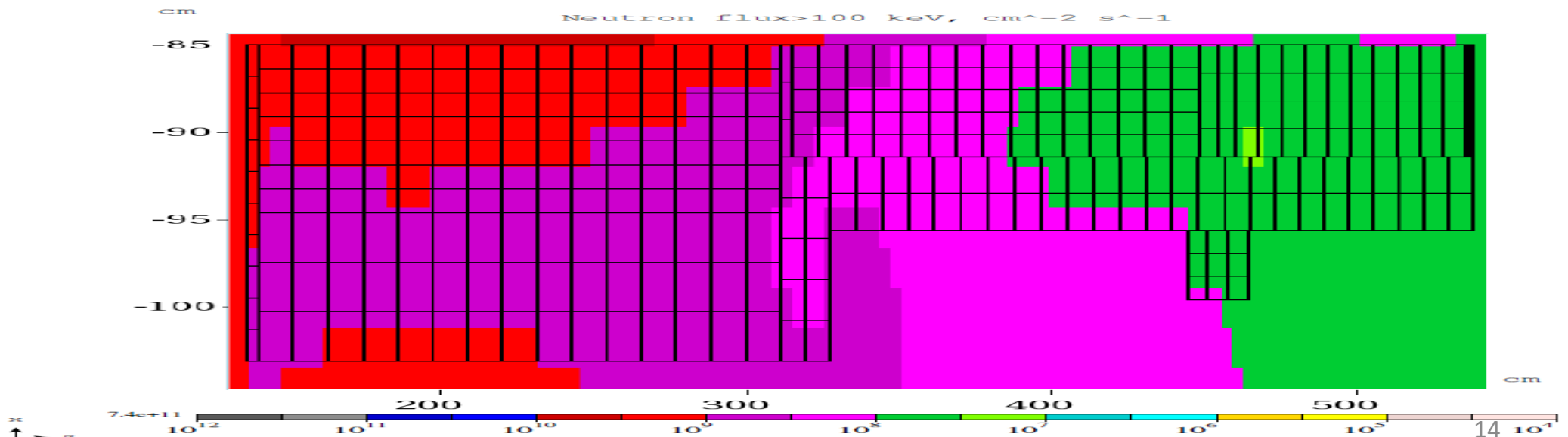
# Neutron flux, total and >100 keV

Flux =  $8.3E9 \text{ cm}^{-2} \text{ s}^{-1}$

$<1E22 \text{ m}^{-2}$



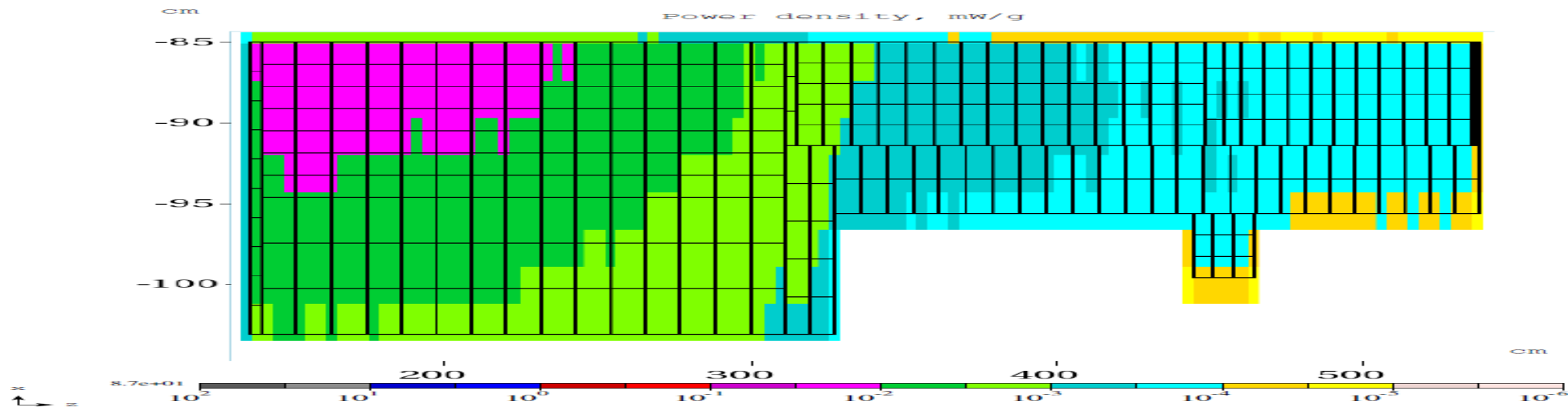
Flux =  $3.0E9 \text{ cm}^{-2} \text{ s}^{-1}$



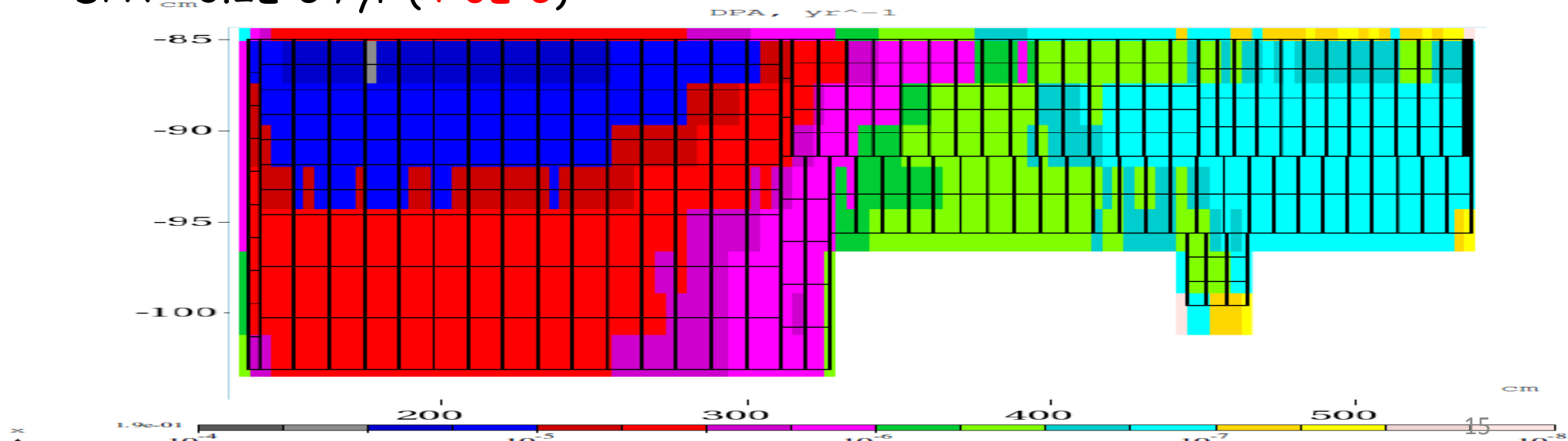
# Power density, mW/g

17  $\mu\text{W/g}$

Dynamic heat load  $Q=20\text{ W}$  (100 W)



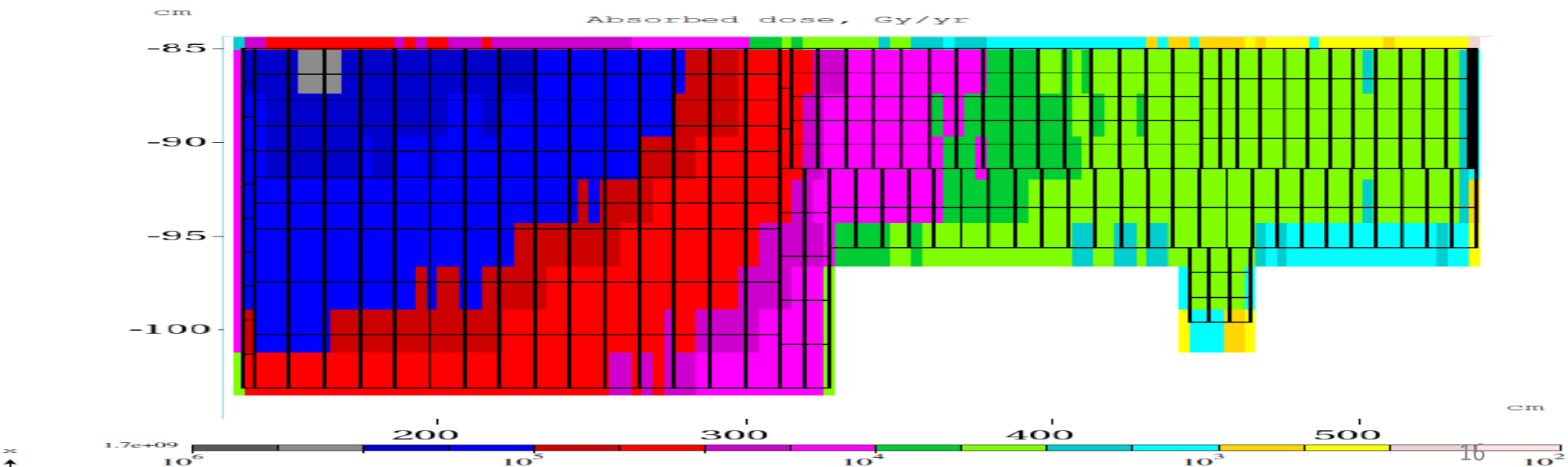
DPA =  $3.2\text{E-}5$  /yr (4-6E-5)



# Absorbed dose. Summary table

Quantity\Model	LAQGSM+CEM, MIN f.	LAQGSM+CEM,MAX f.	Default, MIN
T. Neutron flux n/cm2/s	8.5E9	8.3E9	7.9E9
HE Neutron flux n/cm2/s	3.1E9	3.0E9	2.4E9
Power density, uW/g	16	17	9
DPA, /yr	3.1E-5	3.2E-5	2.4E-5
Absorbed dose, kGy/yr	330	330	170

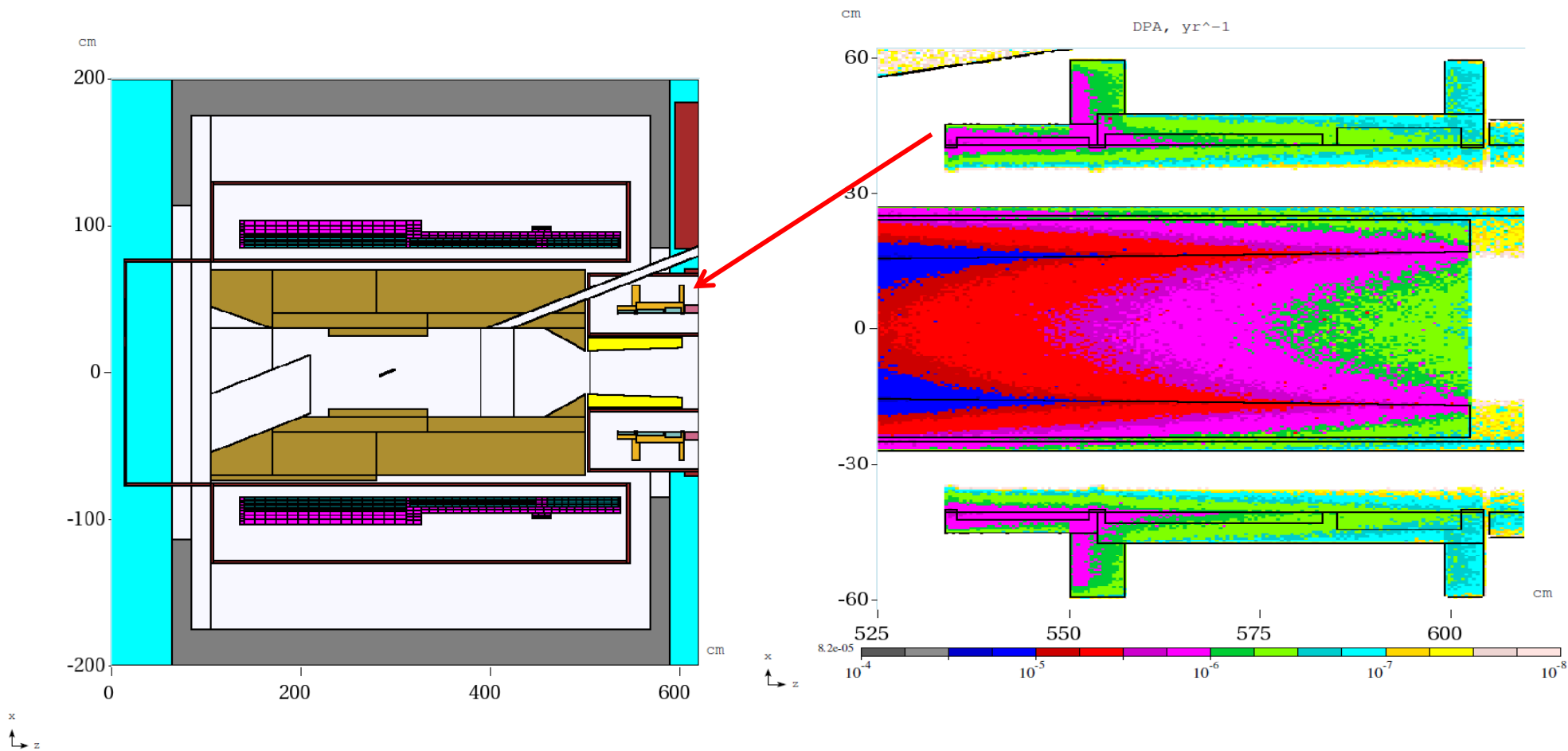
Dose = 330 kGy/yr (350 kGy/yr)



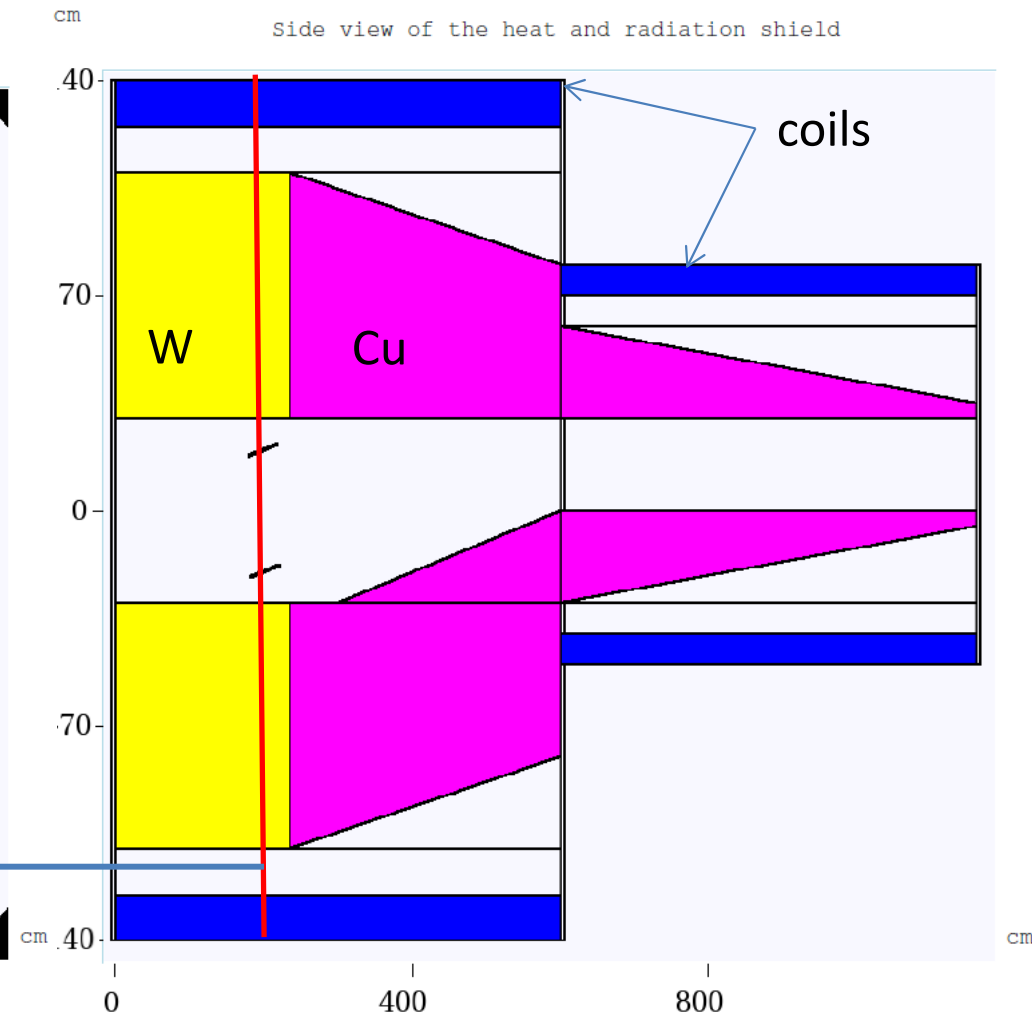
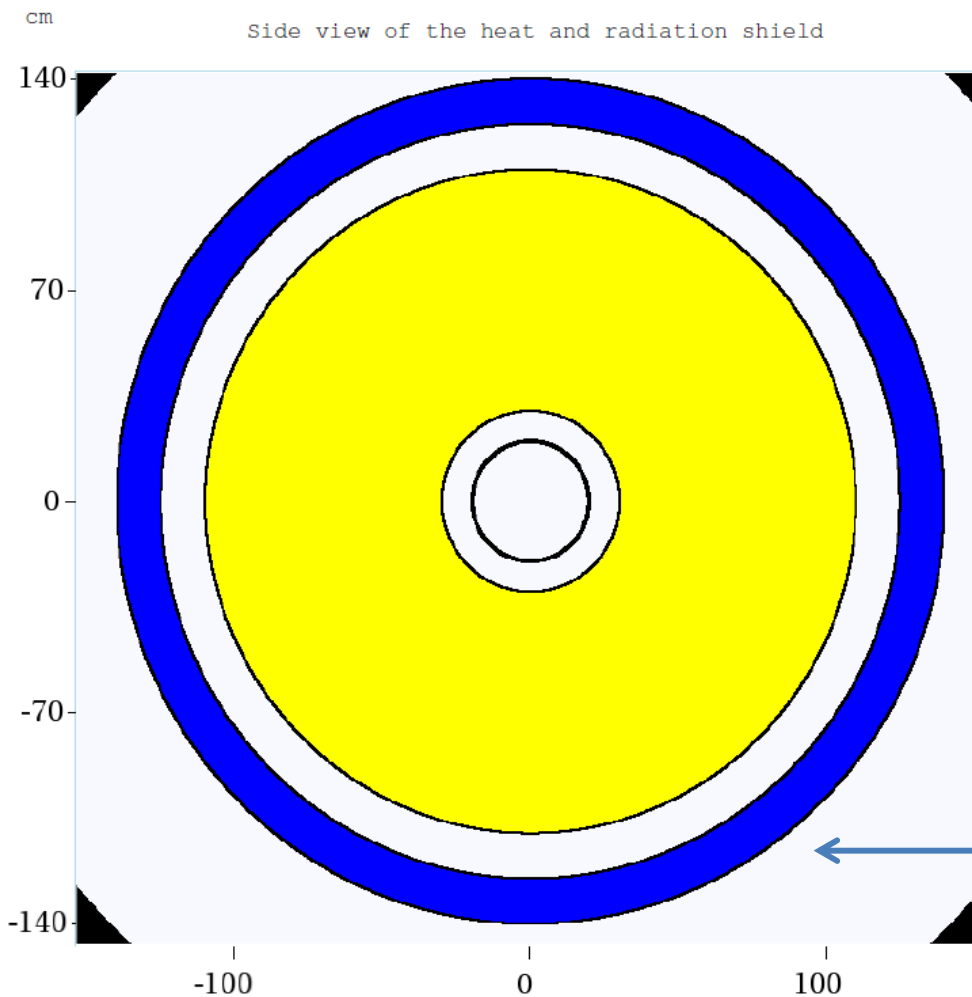


# Radiation quantities at TS1

DPA=2.2E-6/yr, Power density= 0.5E-3 mW/g,  
Absorbed dose = 1.1E4 Gy/yr,



# Preliminary MARS model of Mu2e@PX heat and radiation shield. Shape optimization

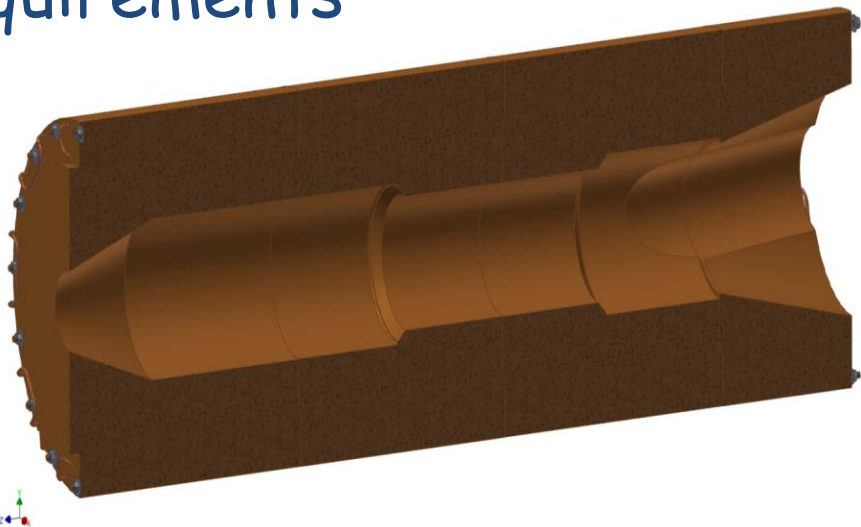


$L(W)=235$  cm,  $L(Cu1)=365$  cm,  $L(Cu2)=560$  cm

1 MW, C target:  $\sim 190$  tonnes of W/130 tonnes of Cu

# Conclusions

- Current Heat and Radiation Shield design based on thorough MARS15 simulations satisfies all the requirements for 1/3 of the nominal beam power
- An engineering design based on the model has been developed
- A model of Heat and Radiation Shield is also proposed for the case of nominal beam power, also satisfying all requirements



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