

# **SUPERCONDUCTING SOLENOIDS - SHIELDING STUDIES 1.**

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BNL  
(Oct. 5, 2010)**

**Energy deposition from MARS and MARS+MCNP codes.**

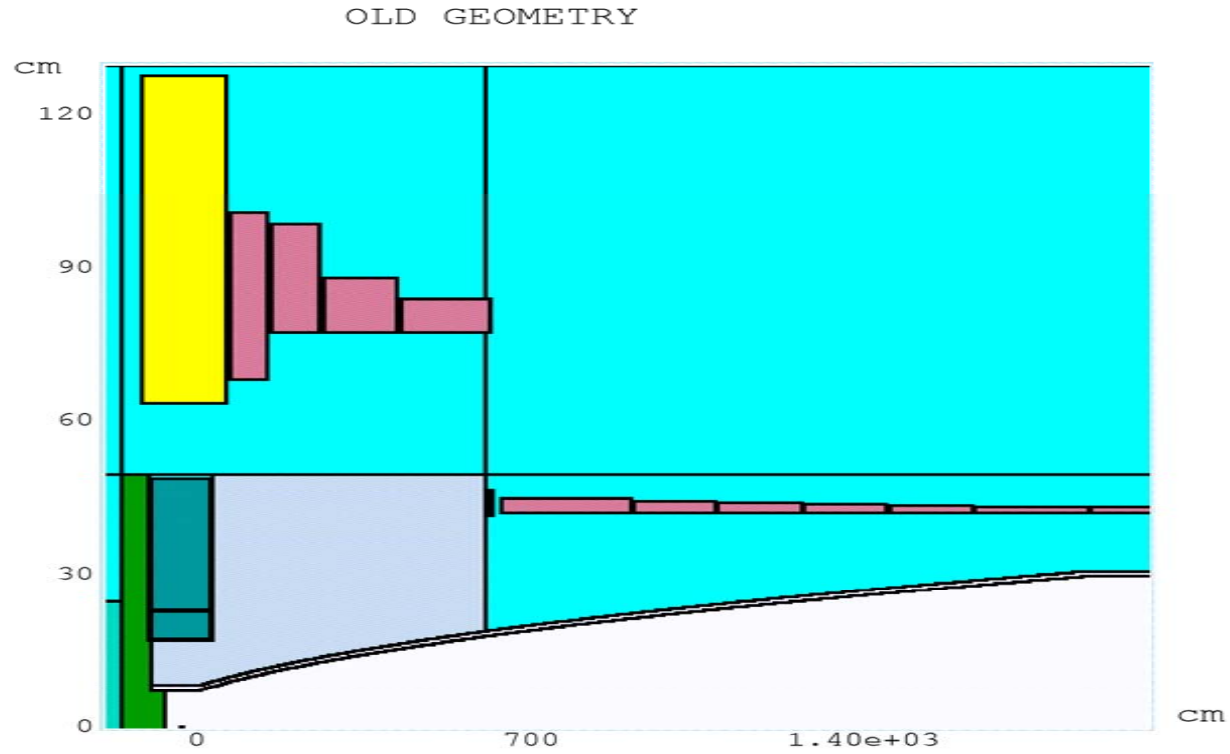
**STANDARD GEOMETRY, STANDARD SHIELDING(80%WC+20% H2O)**

**GAUSSIAN PROFILE:  $\sigma_x = \sigma_y = 0.12$  cm**

**E=8 GeV, 4MW proton beam**

**also introducing a 20 MeV neutron energy cutoff.**

# STANDARD (OLD) SOLENOID GEOMETRY

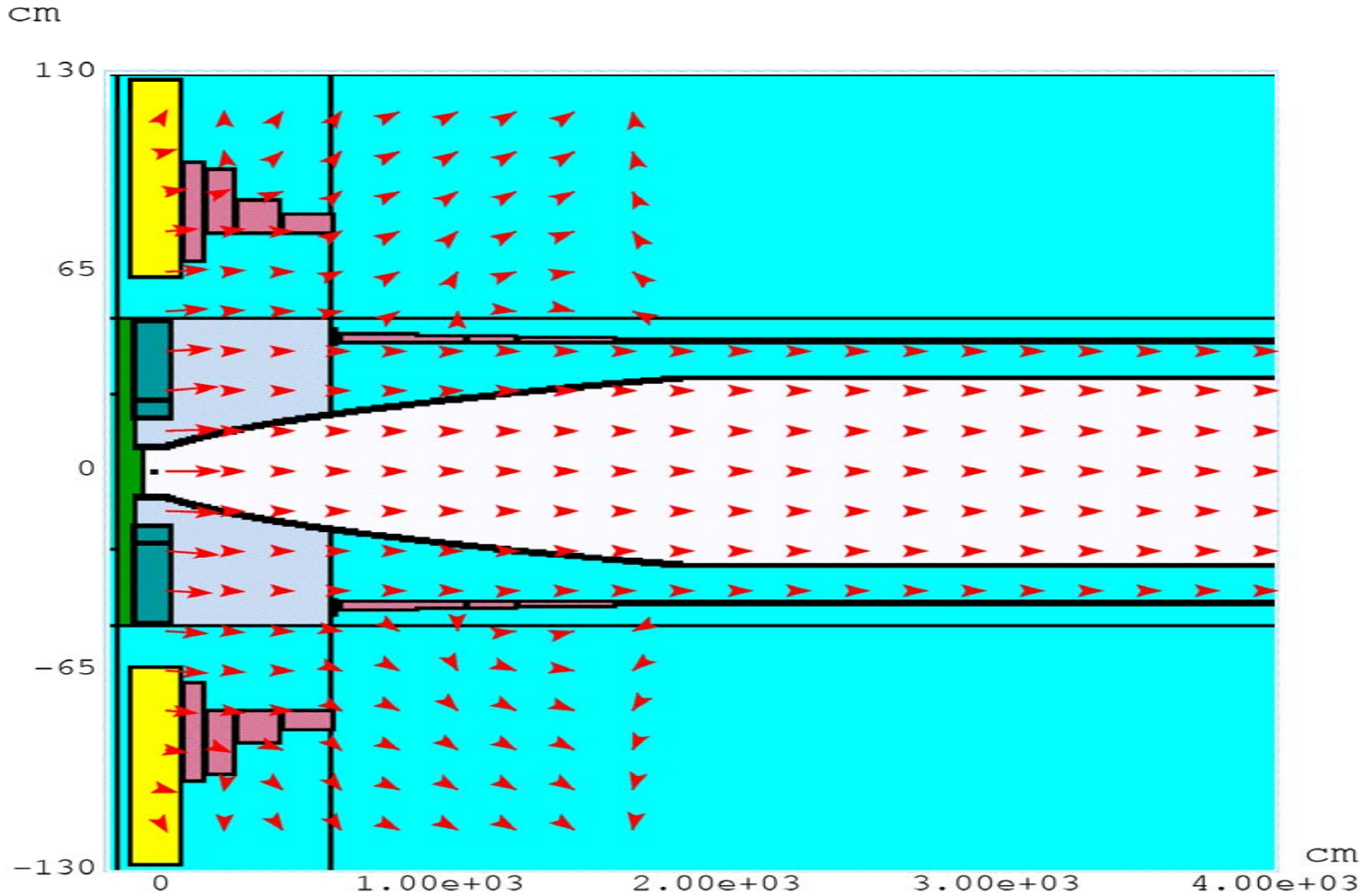


Aspect Ratio: X:Z = 1:16.9230

SC#1	-120 < z < 57.8 cm	$R_{in} = 63.3$ cm	$R_{out} = 127.8$ cm	
SC#2	67.8 < z < 140.7 cm	$R_{in} = 68.6$ cm	$R_{out} = 101.1$ cm	
SC#6-13	632.5 < z < 218.7 cm	$R_{in} = 42.2$ cm	$R_{out} = 45.1 \rightarrow 43.4$ cm	(TOTAL #

SC=13)

# STANDARD (OLD) SOLENOID GEOMETRY: MAGNETIC FIELD



Aspect Ratio: X:Z = 1:16.1538

# Energy deposition from MARS and MARS+MCNP codes, also by introducing a 20 MeV neutron energy cutoff.

(STANDARD GEOMETRY, 80%WC+20% H2O SHIELDING)

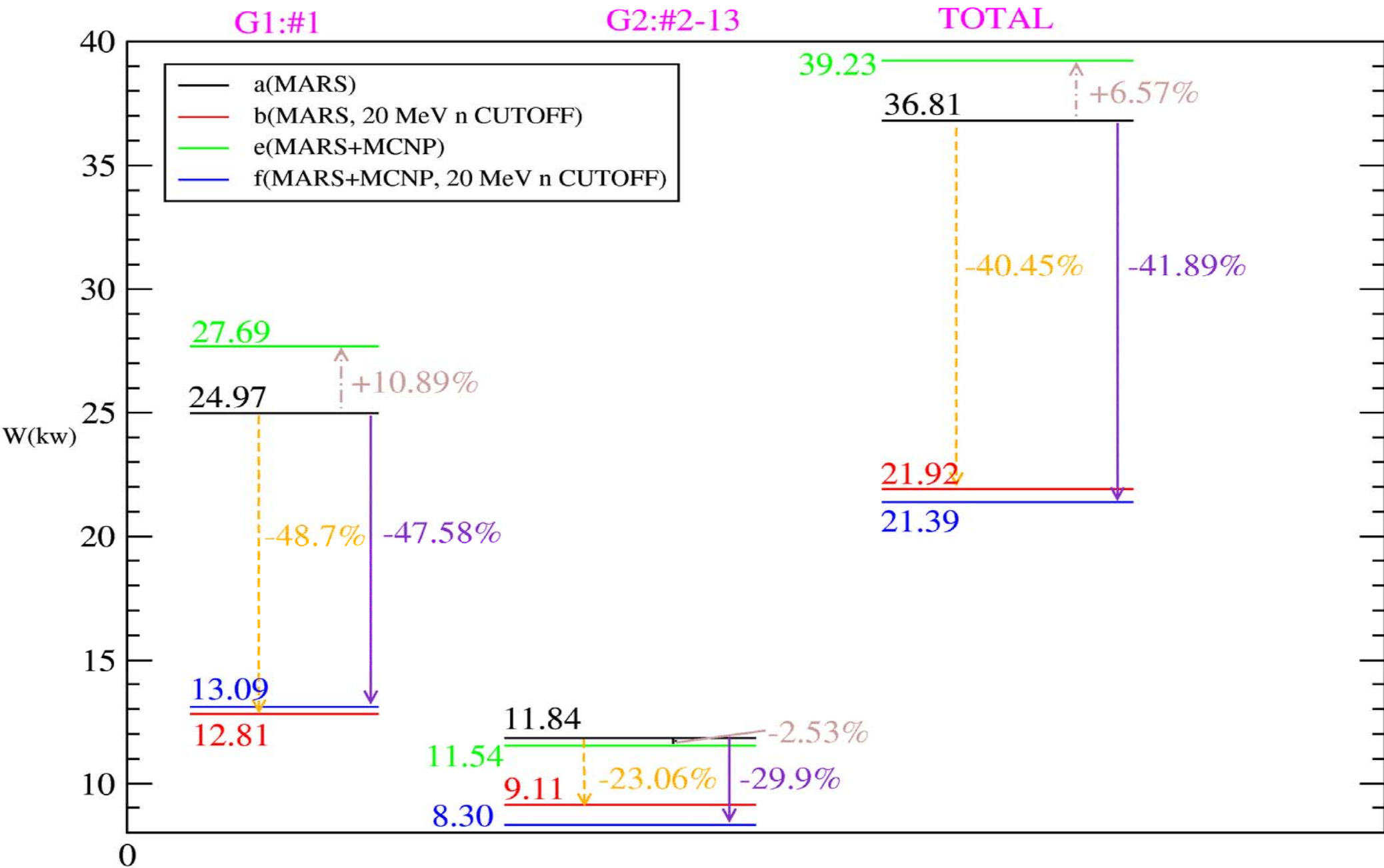
Table 0.1: (10/5/2010)

$N_p=100,000$ , STANDARD GEOMETRY,13 SC COILS, 2 SC groups:G1=1, G2=2-13
STANDARD SHIELDING WITH: 80% WC+20% $H_2O$
SOLENOID MATERIALS: SC#1-13=SCON (NiTi+Cu+..)
a=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian)
b=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 20$ MeV)
c=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 50$ MeV)
d=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 150$ MeV)
e=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian)
f=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 20$ MeV)
g=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 50$ MeV)
h=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 150$ MeV)
i=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian,Ding/def SCON )
j=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian,I define SCON )

Table 0.2: POWER OF DEPOSITED ENERGY IN KW, DW/W %= $((W_x-W_a)/W_a) \times 100$  where x=b,c,d. (10/5/2010)

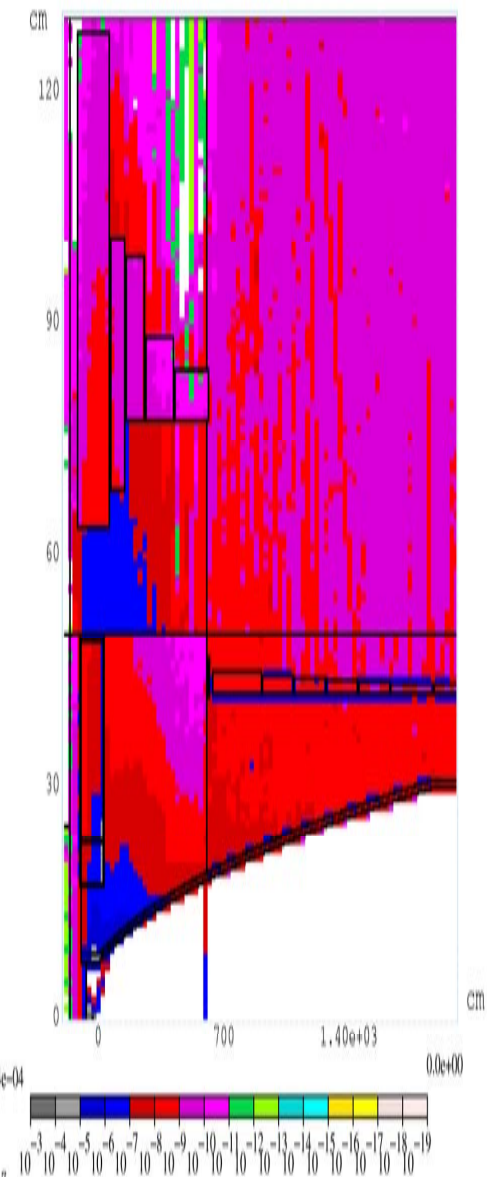
	G1	%	G2	%	Total	%
a	24.97	-	11.84	-	36.81	-
b	12.81	-48.70	9.11	-23.06	21.92	-40.45
c	8.31	-66.72	7.73	-34.71	16.03	-56.45
d	2.22	-91.11	6.70	-43.41	8.92	-75.77
e	27.69	+10.89	11.54	-2.53	39.23	+6.57
f	13.09	-47.58	8.30	-29.90	21.39	-41.89
g	7.78	-68.84	7.39	-37.58	15.17	-58.79
h	2.43	-90.27	6.01	-49.24	8.44	-77.07
i	24.91	-	11.23	-	36.13	-
j	24.73	-	12.09	-	36.81	-

$N_p=100,000, E_p=8\text{GeV}, 4\text{ MW}, \text{ standard geom.}, 13\text{ SC}, 80\%WC+20\% H_2O, \text{ SC:1-13(SCON)}, \text{ DEPOSITED ENERGY POWER}$

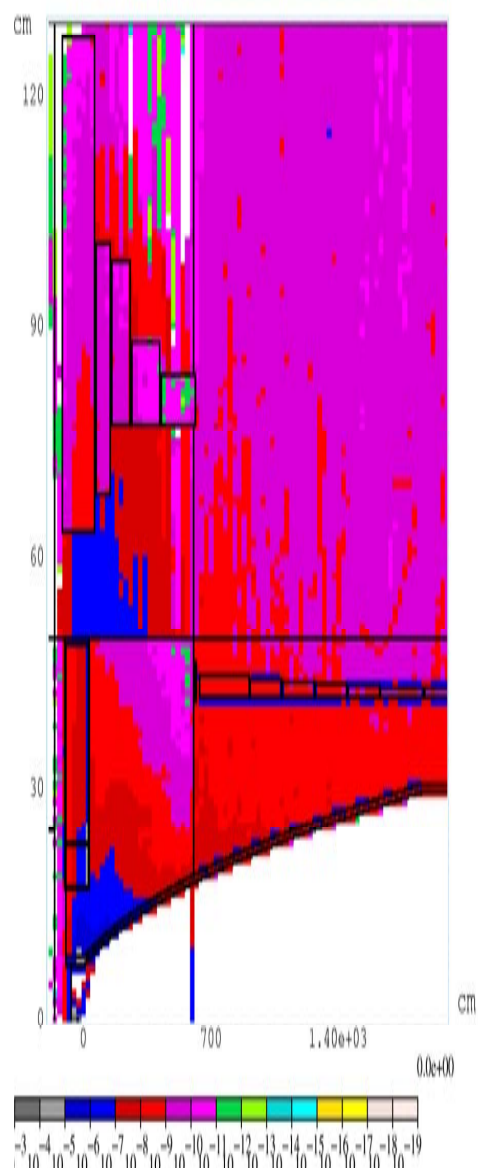




STANDARD GEOMETRY-ENERGY DEPOSITION



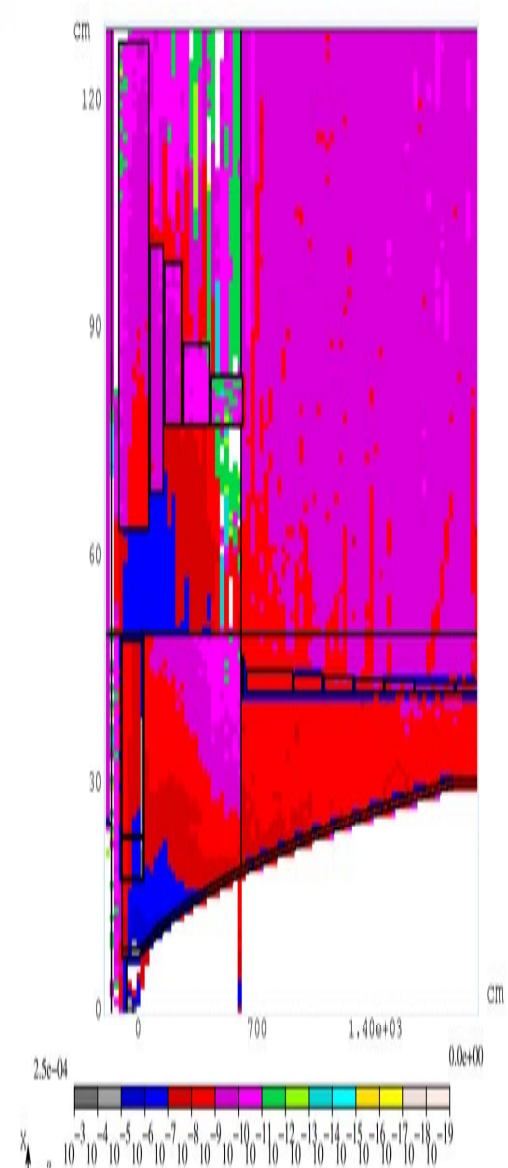
3D GEOMETRY ENERGY DEPOSITION, 20 MeV NEUTRON ENERGY C



MARS+MACNP ENERGY DEPOSITION



MARS+MCNP ENERGY DEPOSITION 20 MeV NEUTRON ENERGY CUTOFF



Power peaks at 5 mW/gr

**Energy deposition from MARS+MCNP code.  
Introducing different neutron energy cutoffs.  
(STANDARD GEOMETRY, 80% WC+20% H2O SHIELDING)**

Table 0.3(10/5/2010)

	$E_n \geq E_t$ (MeV)	SC#1	%	SC#2-13	%	Total	%
1	$1 \cdot 10^{-11}$	37.94	-	12.25	-	50.19	-
2	$1 \cdot 10^{-6}$	31.64	-16.60	11.60	-5.31	43.24	-13.85
3	$1 \cdot 10^{-5}$	30.59	-19.37	11.28	-7.92	41.87	-16.58
4	$1 \cdot 10^{-4}$	29.50	-22.25	11.57	-5.51	41.06	-18.19
5	$1 \cdot 10^{-3}$	29.00	-23.56	11.03	-9.96	40.03	-20.24
6	$1 \cdot 10^{-2}$	28.47	-24.96	11.17	-8.81	39.63	-21.04
7*	$1 \cdot 10^{-1}$	27.69	-27.02	11.54	-5.80	39.23	-21.84
8	$1 \cdot 10^0$	26.73	-29.55	11.42	-6.78	38.15	-23.99
9	$1 \cdot 10^{+1}$	20.51	-45.94	9.97	-18.61	30.48	-39.27
10*	$2 \cdot 10^{+1}$	13.09	-65.50	8.30	-32.24	21.39	-57.38
11	$5 \cdot 10^{+1}$	7.78	-79.49	7.39	-39.67	15.17	-69.77
12	$15 \cdot 10^{+1}$	2.43	-90.27	6.01	-49.24	8.44	-83.18

CASE 7: MARS DEFAULT NEUTRON ENERGY CUTOFF.

CASE 10: MCNP HANDLES ALL NEUTRONS FOR ALL ISOTOPES UP TO 20 MeV, BEYOND THAT, UP TO 150 MeV ONLY CERTAIN CASES.



Deposited energy Power for SC#1, SC#2-13 and total, standard geom., different neutron energy cutoffs ( $10^{-6}$  to 150 MeV)  
(MARS+MCNP) 80% WC+20% H<sub>2</sub>O shielding, 8 GeV protons, 4 MW, Gaussian Distribution  $\sigma_x=\sigma_y=0.12$  cm

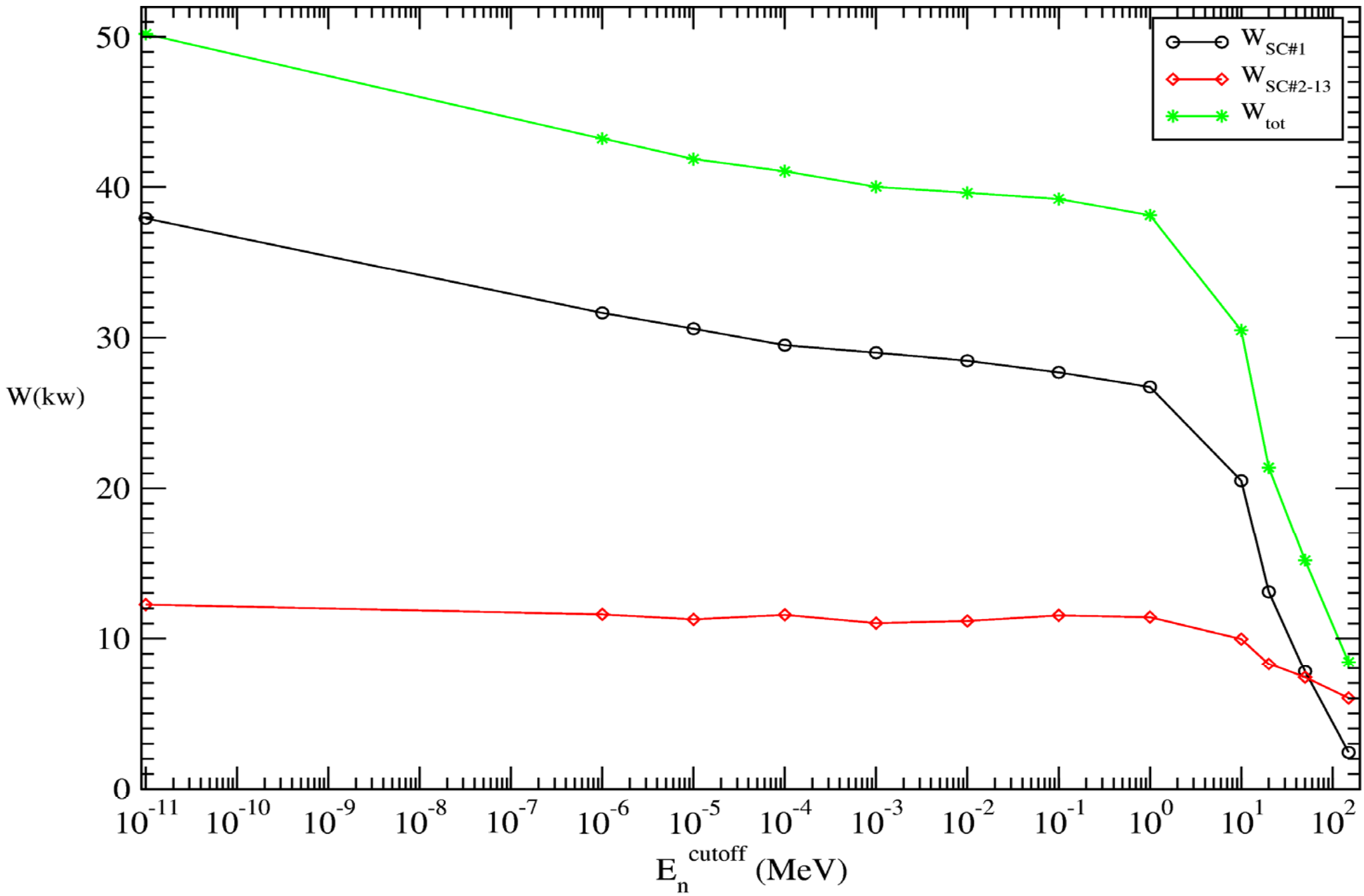


Table 0.4: MARS+MCNP, STANDARD GEOMETRY, 8 GeV, 4 MW, GAUSSIAN ( $\sigma_x = \sigma_y = 0.12$  cm), 80% WC+20%  $H_2O$  SHIELDING, POWER OF DEPOSITED ENERGY IN KW, INITIALIZING MARS WITH DIFFERENT SEEDS(NOTICE: last case s is the seed used throughout in the rest of our studies) . (10/8/2010)

	SEED(8 DIG.)	SC#1	SC#2-13	Total
1	23765224	27.56	11.28	38.83
2	35765224	27.49	11.31	38.80
3	77225426	27.76	11.06	38.82
4	66666666	27.34	11.19	38.53
5	12345671	27.91	11.20	39.11
6	52255524	27.27	11.43	38.70
7	23445625	27.58	11.38	38.96
8	36264424	27.11	10.87	37.97
9	73275327	27.11	11.52	38.63
10	66265556	28.00	10.93	38.93
-	MIN	27.11	10.87	37.97
-	MAX	28.00	11.52	39.11
-	AVERAGE	27.51	11.22	38.73
-	$\sigma$ (Deviat.)	0.296	0.201	0.298
s	55265522	27.64	11.54	39.23

**Energy deposition from MARS and MARS+MCNP codes .**

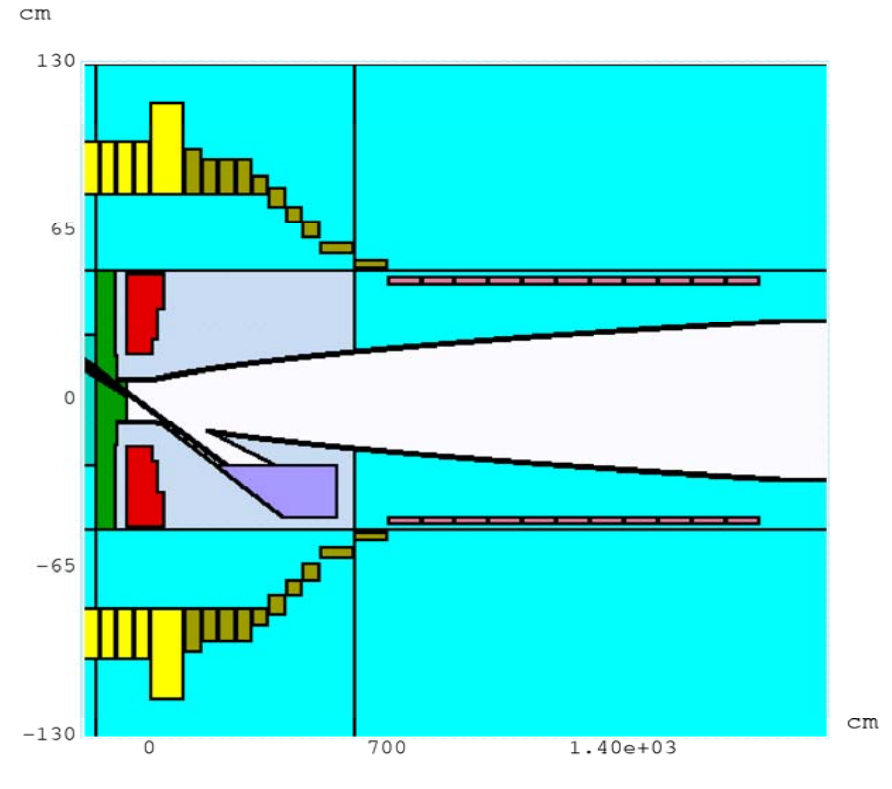
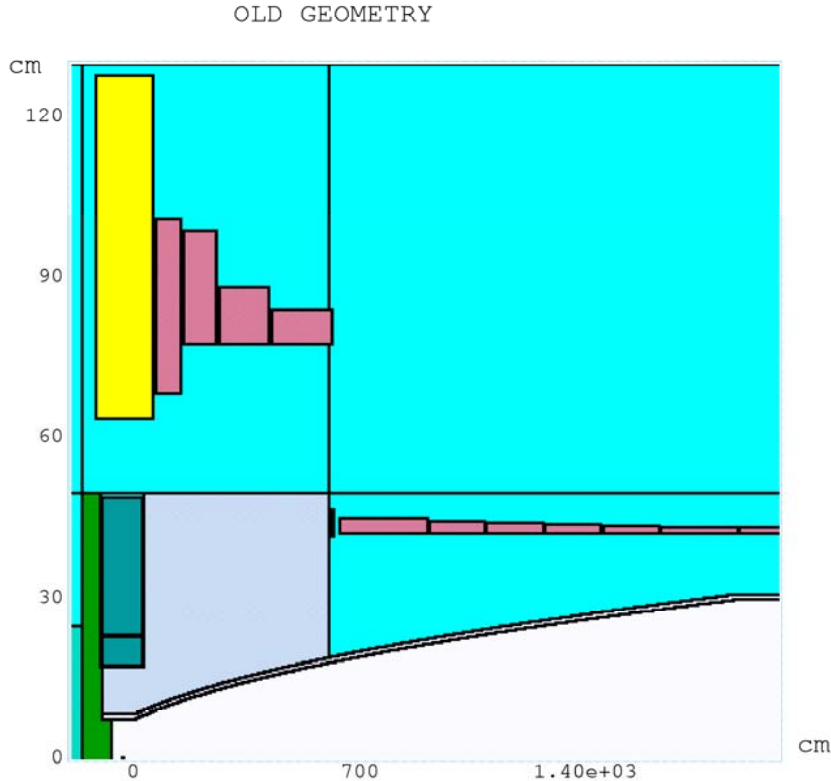
**IDS80 GEOMETRY, STANDARD SHIELDING(60%WC+40% H2O)**

**GAUSSIAN PROFILE:  $\sigma_x = \sigma_y = 0.12$  cm**

**E=8 GeV, 4MW proton beam**

**also introducing a 20 MeV neutron energy cutoff**

# STANDARD (OLD) VS. IDS80 (NEW) SOLENOID GEOMETRY (IDS80 WITH STANDARD SHIELDING BUT 60%WC+40% H2O)



Aspect Ratio: Y:Z = 1:8.46153

**OLD:** SC#1 -120<z<57.8 cm  $R_{in}=63.3$  cm  $R_{out}=127.8$  cm  
 SC#2 67.8<z<140.7 cm  $R_{in}=68.6$  cm  $R_{out}=101.1$  cm  
 SC#6-13 632.5<z<218.7 cm  $R_{in}=42.2$  cm  $R_{out}=45.1 \rightarrow 43.4$  cm (TOTAL # SC=13)

**NEW:** SC#1-10 -200<z<345 cm  $R_{in}=80.0$  cm  $R_{out}=100$  (1-4)/115 (5)/97 (6)/93(7-9)/87(10)cm  
 SC#11-15 350<z<695 cm  $R_{in}=75.0 \rightarrow 51$  cm  $R_{out}=82.0 \rightarrow 54$  cm  
 SC#16-26 700<z<1795 cm  $R_{in}=45$  cm  $R_{out}=48$  cm (TOTAL # SC=26)

# Energy deposition from MARS and MARS+MCNP codes, also by introducing a 20 MeV neutron energy cutoff.

(IDS80 WITH STANDARD SHIELDING+GAUSSIAN PROFILE BEAM)

Table 0.4: (10/4/2010)

$N_p=100,000$ , 4 SC groups:G1=1-5, G2=6-10, G3=11-15, G4=16-26
STANDARD SHIELDING WITH: 60% WC+40% $H_2O$
SOLENOID MATERIALS: SC#1-10=NBSN (Ni+..) and SC#11-26=SCON (NiTi+Cu+..)
a=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian)
b=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 20$ MeV)
c=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian)
d=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 20$ MeV)

Table 0.5: POWER OF DEPOSITED ENERGY IN KW, DW/W %= $((W_x-W_a)/W_a) \times 100$  where x=b,c,d. (10/4/2010)

	G1	%	G2	%	G3	%	G4	%	Total	%
a	11.56	-	2.606	-	0.807	-	9.870	-	24.843	-
b	6.185	-46.50	1.500	-42.43	0.823	+1.98	8.665	-12.21	17.730	-30.87
c	12.925	+11.81	2.707	+3.90	0.702	-13.01	9.465	-4.10	25.800	+3.86
d	6.240	-46.02	1.437	-44.86	0.654	+18.95	8.880	-10.03	17.211	-30.72

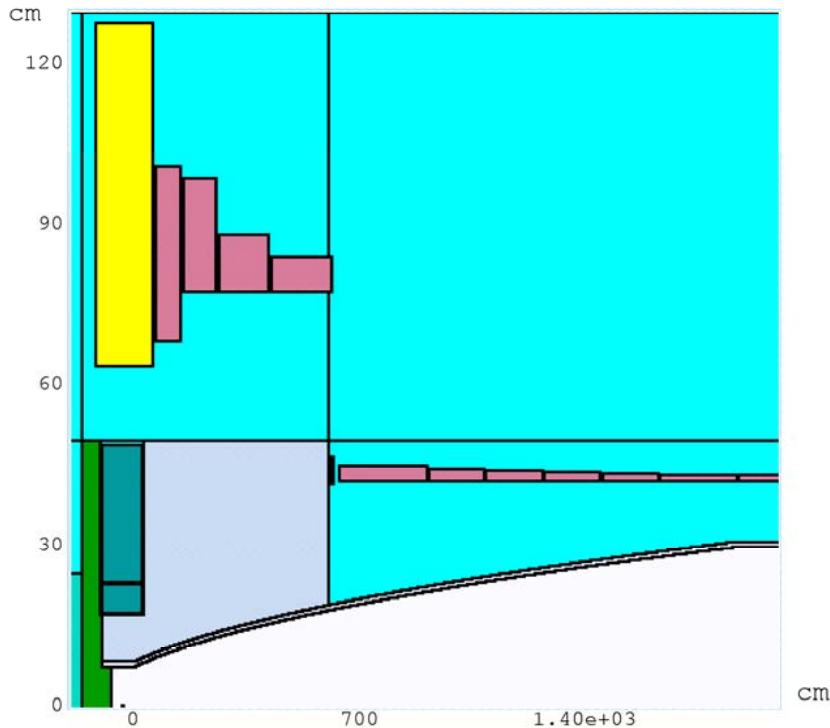
## Energy deposition for different initial beam profiles and energies. MARS, MARS+MCNP results (IDS80 SUPER-ENHANCED SHIELDING)

- Uniform density in square region  
 $[-\sigma_x, \sigma_x] \times [-\sigma_y, \sigma_y]$ 
  - a)  $\sigma_x = \sigma_y = 0.12$  cm
  - b)  $\sigma_x = \sigma_y = 0.30$  cmfor  $E=8.0$  GeV, 4MW proton beam
- Gaussian profile  $\sigma_x = \sigma_y = 0.12$  cm
  - a)  $E=7.5$  GeV
  - b)  $E=8.5$  GeV
- MARS+MCNP results for gaussian profile
- Use a 20 MeV neutron energy cutoff (MARS, MARS+MCNP)-->?

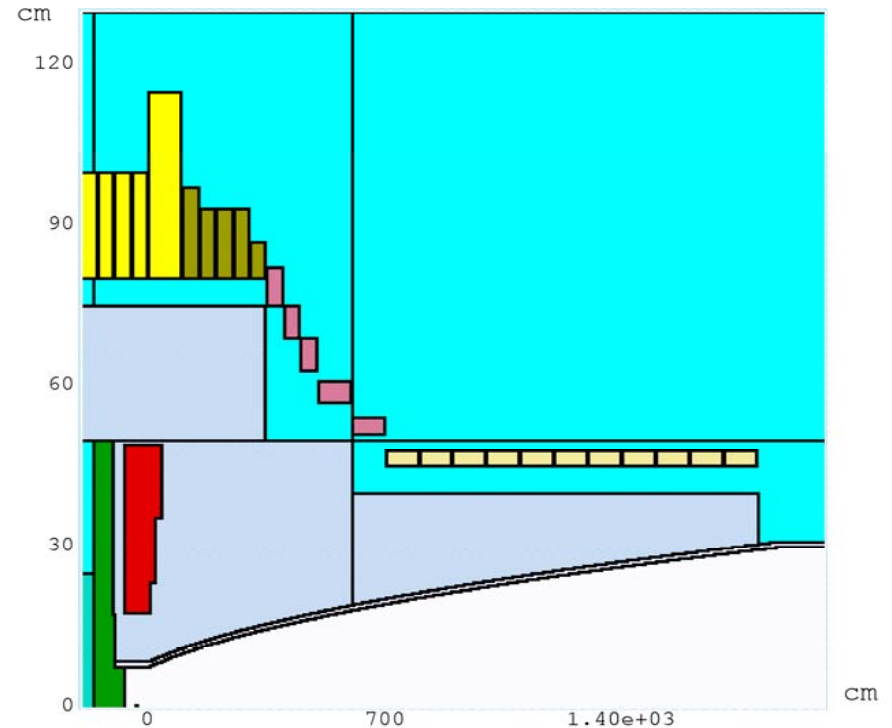


# OLD VS. NEW SOLENOID GEOMETRY (IDS80 SUPER-ENHANCED SHIELDING)

OLD GEOMETRY



SUPER-ENHANCED GEOMETRY SC#1-10 (NBSN) SC#11-26 (SCON)



Aspect Ratio: X:Z = 1:16.9230

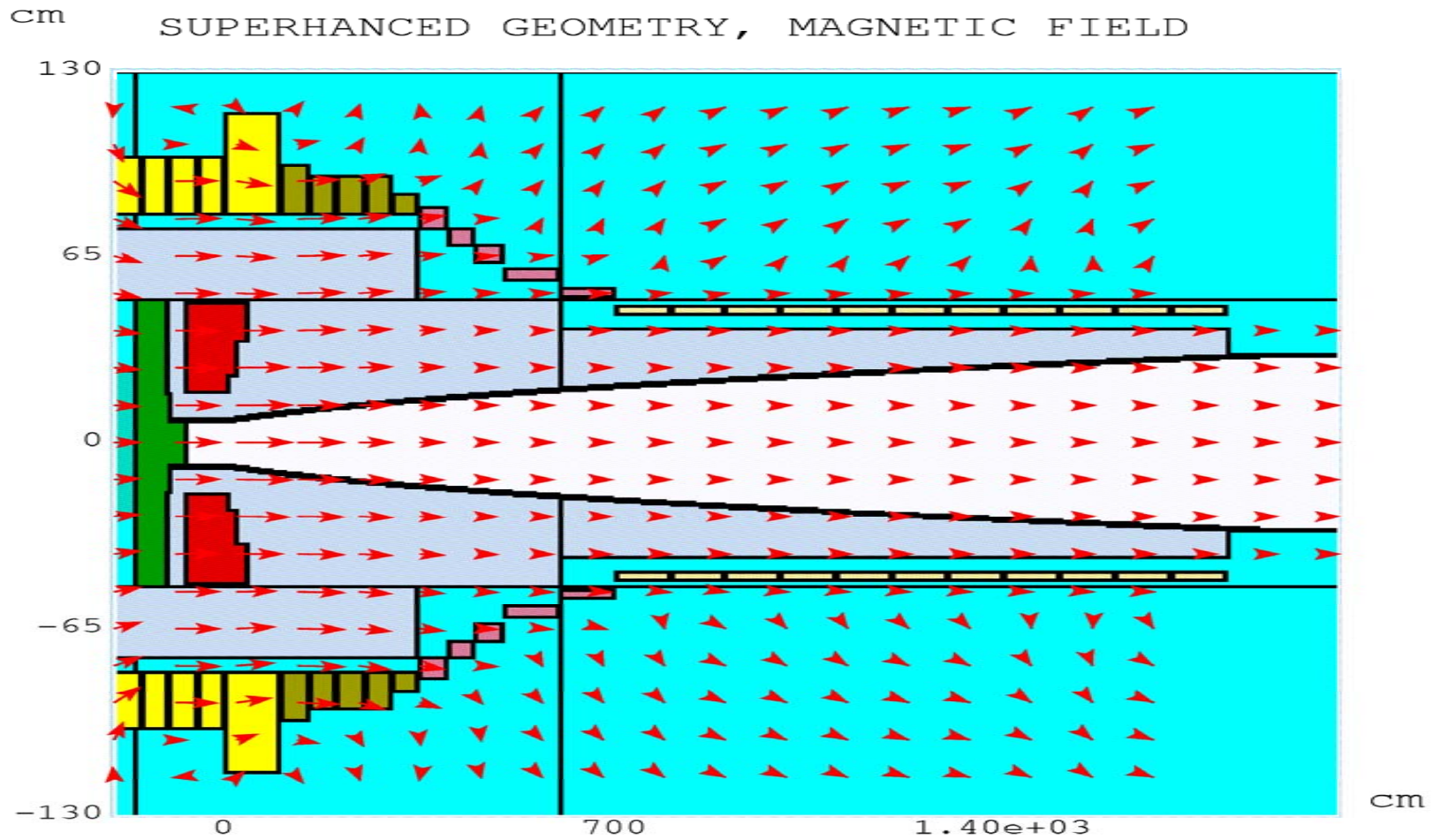


Aspect Ratio: X:Z = 1:16.9230

**OLD:** SC#1     $-120 < z < 57.8$  cm     $R_{in} = 63.3$  cm     $R_{out} = 127.8$  cm  
 SC#2     $67.8 < z < 140.7$  cm     $R_{in} = 68.6$  cm     $R_{out} = 101.1$  cm  
 SC#6-13     $632.5 < z < 218.7$  cm     $R_{in} = 42.2$  cm     $R_{out} = 45.1 \rightarrow 43.4$  cm    (TOTAL # SC=13)

**NEW:** SC#1-10     $-200 < z < 345$  cm     $R_{in} = 80.0$  cm     $R_{out} = 100$  (1-4)/115 (5)/97 (6)/93(7-9)/87(10)cm  
 SC#11-15     $350 < z < 695$  cm     $R_{in} = 75.0 \rightarrow 51$  cm     $R_{out} = 82.0 \rightarrow 54$  cm  
 SC#16-26     $700 < z < 1795$  cm     $R_{in} = 45$  cm     $R_{out} = 48$  cm    (TOTAL # SC=26)

# Magnetic field for IDS80 with super-enhanced shielding.



Aspect Ratio: X:Z = 1:8.46153

Table 0.6: (9/30/2010)

$N_p=100,000$ , 4 SC groups:G1=1-5, G2=6-10, G3=11-15, G4=16-26
SUPERENHANCED SHIELDING WITH: 60% WC+40% $H_2O$
SOLENOID MATERIALS: SC#1-10=NBSN (Ni+..) and SC#11-26=SCON (NiTi+Cu+..)
a=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian)
b=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Uniform/square)
c=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.3$ cm Uniform/square)
d=( $E_p=7.5$ GeV, 4 MW BEAM (NORM.), $\sigma_x=\sigma_y=0.12$ cm Gaussian)
e=( $E_p=8.5$ GeV, 4 MW BEAM (NORM.), $\sigma_x=\sigma_y=0.12$ cm Gaussian)
f=( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 20$ MeV)
g=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian)
h=MARS+MCNP ( $E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian, $E_n \geq 20$ MeV)

Table 0.7: POWER OF DEPOSITED ENERGY IN KW, DW/W %= $((W_x-W_a)/W_a) \times 100$  where x=b,c,d,e,f,g,h. (9/30/2010)

	G1	%	G2	%	G3	%	G4	%	Total	%
a	1.830	-	0.386	-	0.132	-	0.264	-	2.612	-
b	1.853	+1.26	0.329	-14.77	0.110	-16.67	0.294	+11.36	2.586	-0.99
c	1.725	-5.74	0.395	+2.33	0.119	-9.85	0.252	-4.55	2.491	-4.86
d	1.749	-4.43	0.346	-10.36	0.115	-12.88	0.241	-8.71	2.451	-6.16
e	1.757	-3.99	0.341	-11.66	0.143	+8.33	0.249	-5.68	2.489	-4.71
f	1.025	-43.99	0.266	-31.09	0.089	-32.58	0.146	-44.70	1.526	-41.58
g	1.980	+8.20	0.413	+6.99	0.146	+10.61	0.245	-7.20	2.784	+6.58
h	1.165	-36.34	0.232	-39.90	0.075	-43.18	0.200	-24.24	1.672	-35.99

Table 0.8: POWER OF DEPOSITED ENERGY IN KW, a=MARS, b=MARS+MCNP (default  $E_n \geq 0.1$  MeV), c=MARS+MCNP (Choose  $E_n \geq 20$  MeV), 3 SC coil groups, SC#1-15=NBSN material (Ni alloy) SC#16-26 SCON material (NiTi and Cu alloy) (correct materials SC#1-10=NBSN and SC#11-26=SCON), SUPERENHANCED GEOMETRY 60% WC+40%  $H_2O$ , DW/W %= $((W_x - W_a)/W_a) \times 100$  where x=b,c. (9/30/2010)

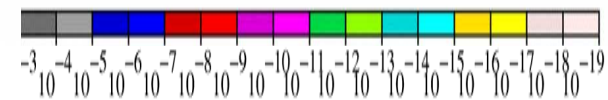
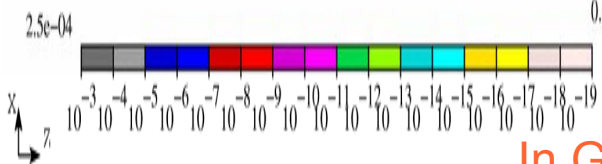
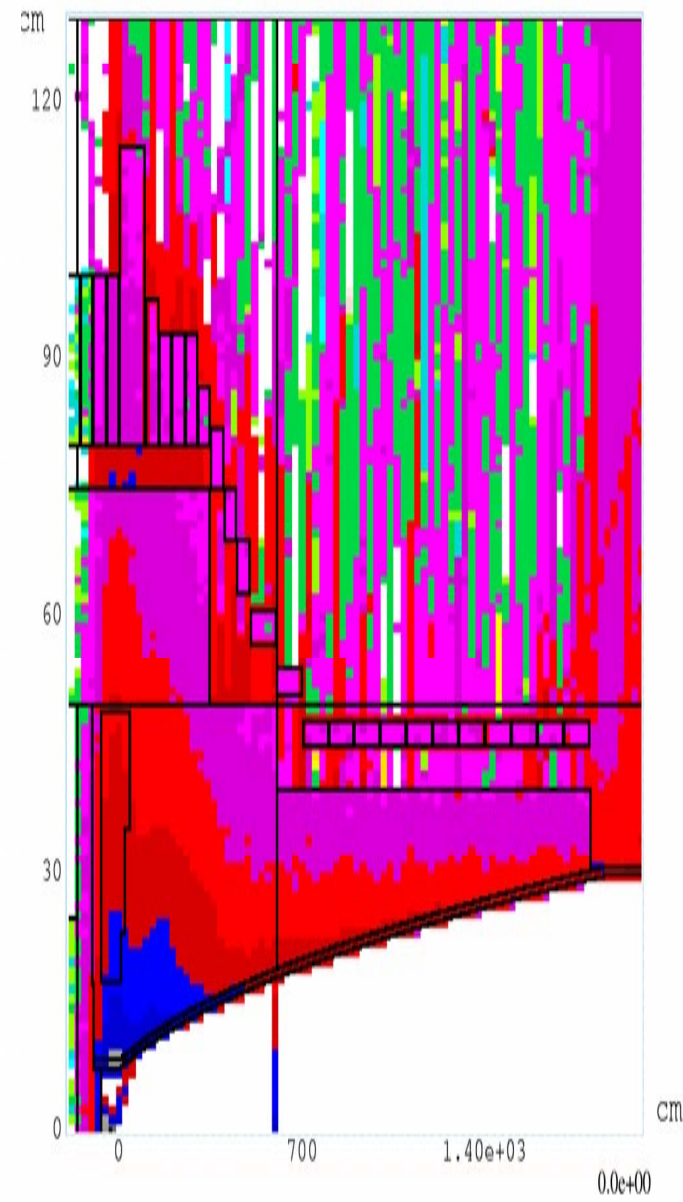
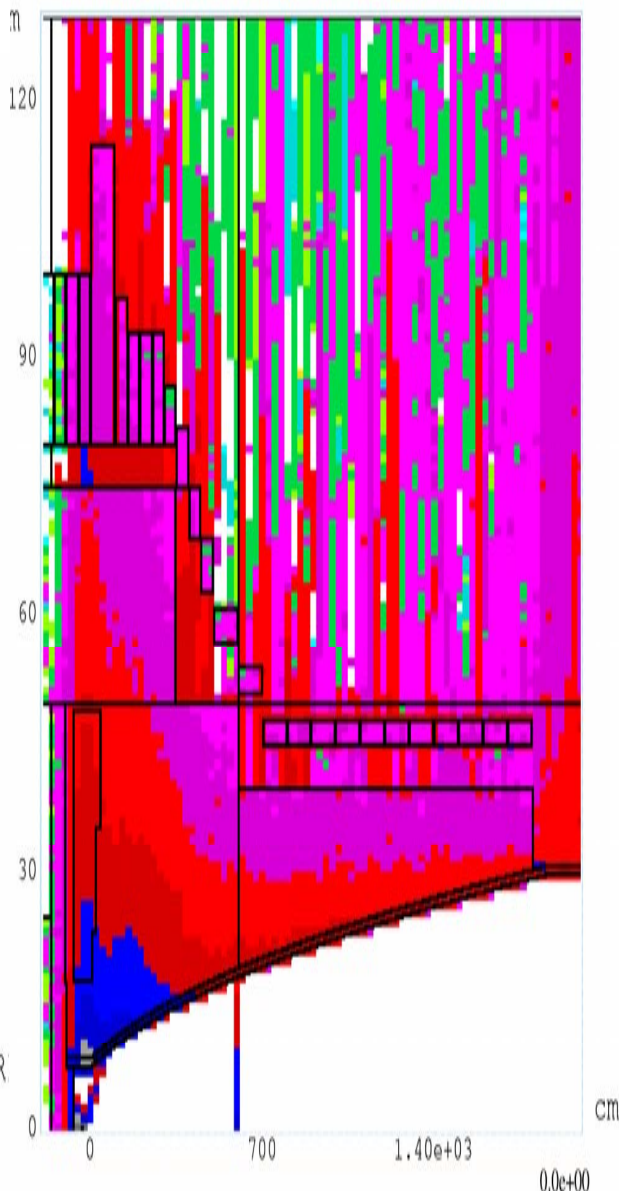
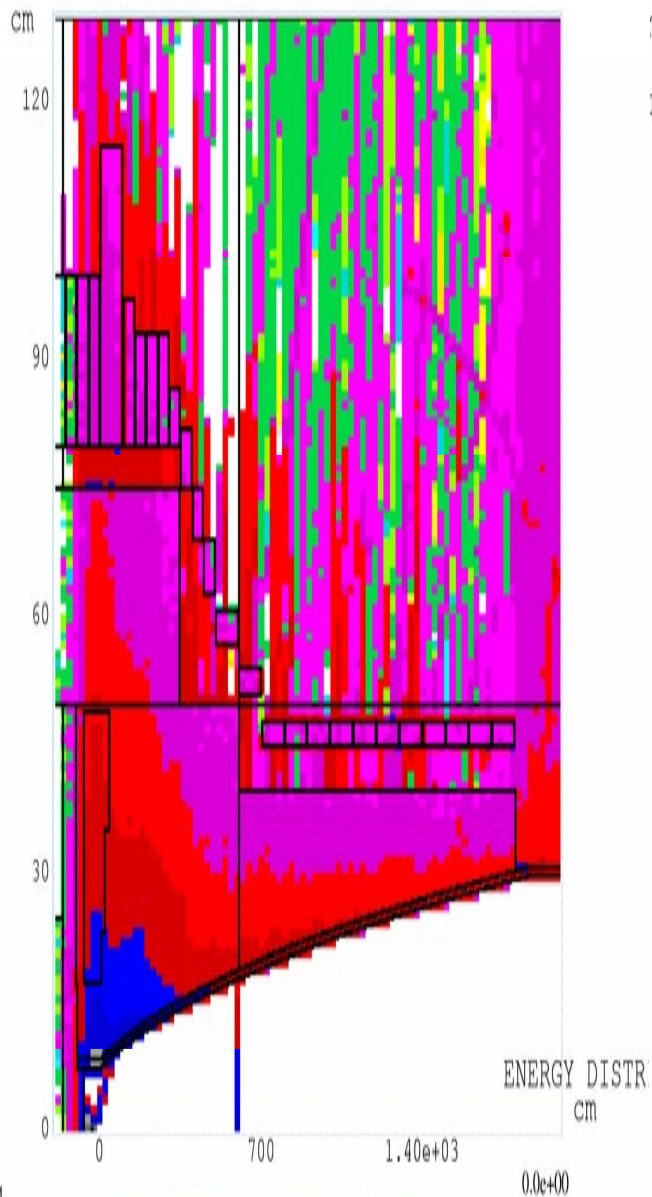
$N_p=100,000, E_p=8$ GeV, 4 MW, $\sigma_x=\sigma_y=0.12$ cm Gaussian, 3 SC groups								
mode/ SC	#1-5	%	#6-15	%	#16-26	%	Total	%
a	1.769	-	0.5435	-	0.2709	-	2.5843	-
b	1.9255	+8.8	0.585	+7.63	0.25395	-6.25	2.764	+6.971
c	1.048	-40.7	0.313	-42.41	0.183	-32.44	1.544	-40.25



ENERGY DISTRIBUTION GAUSSIAN PROFILE 0.12,0.12 E=8 GeV

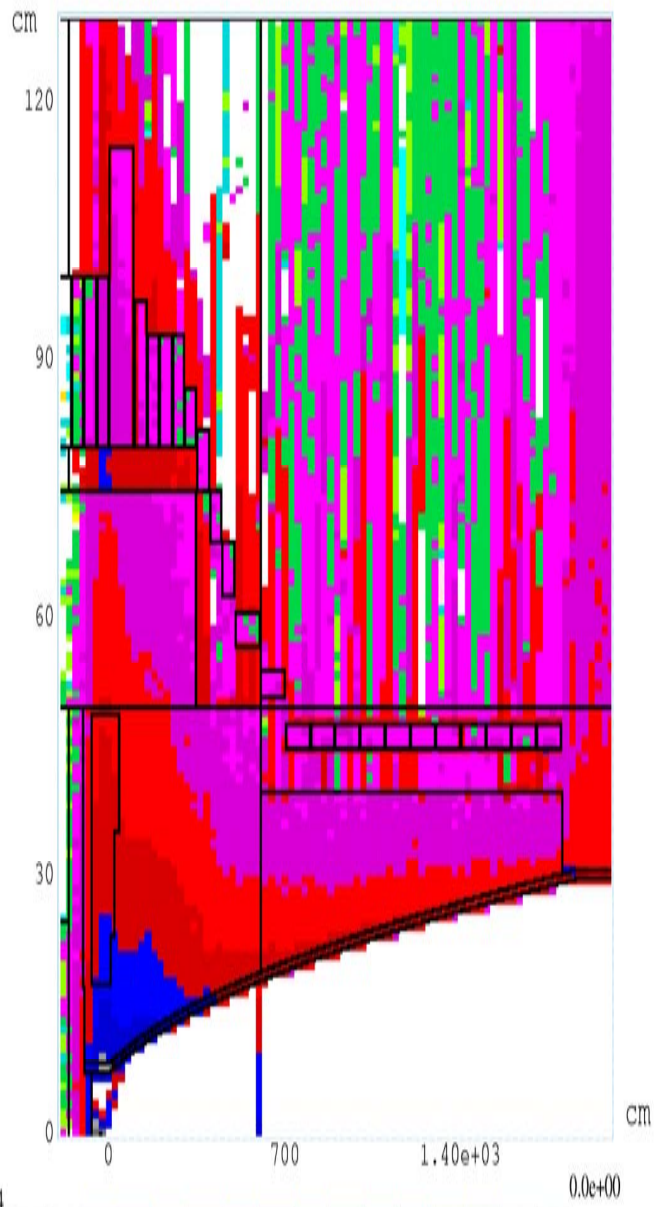
DISTRIBUTION UNIFORM PROFILE 0.24x0.24 SQUARE

DISTRIBUTION UNIFORM PROFILE 0.6x0.6 SQUARE

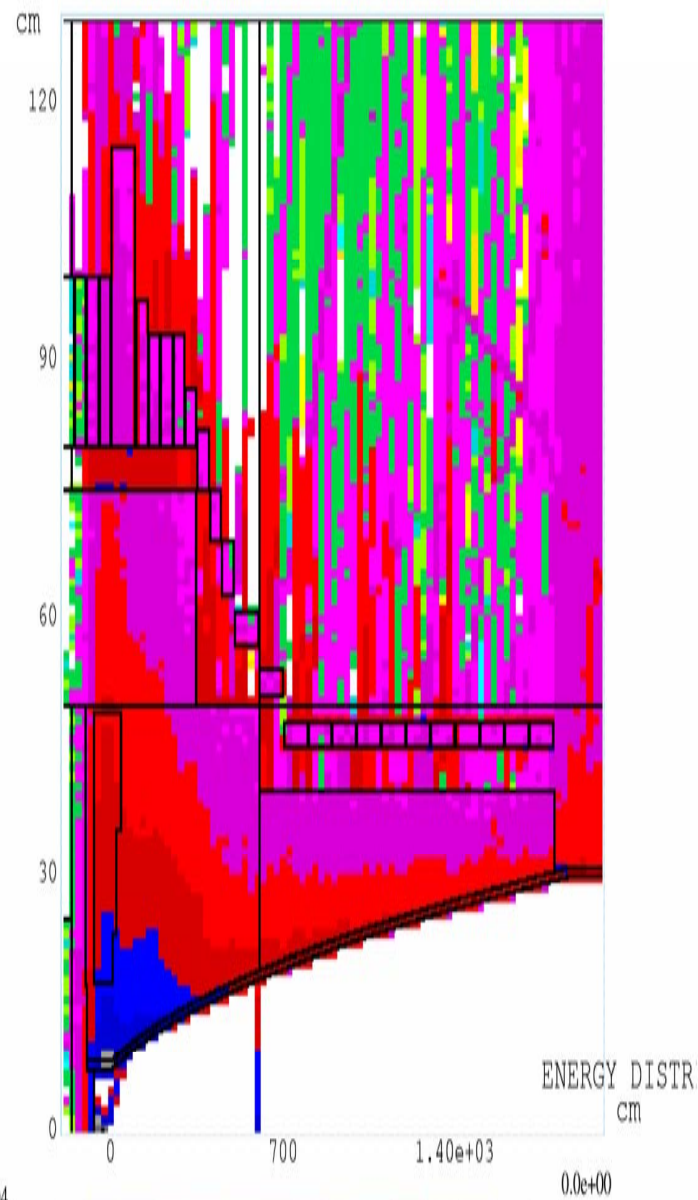


In GeV/gr/proton, peak 0.5 mW/gr

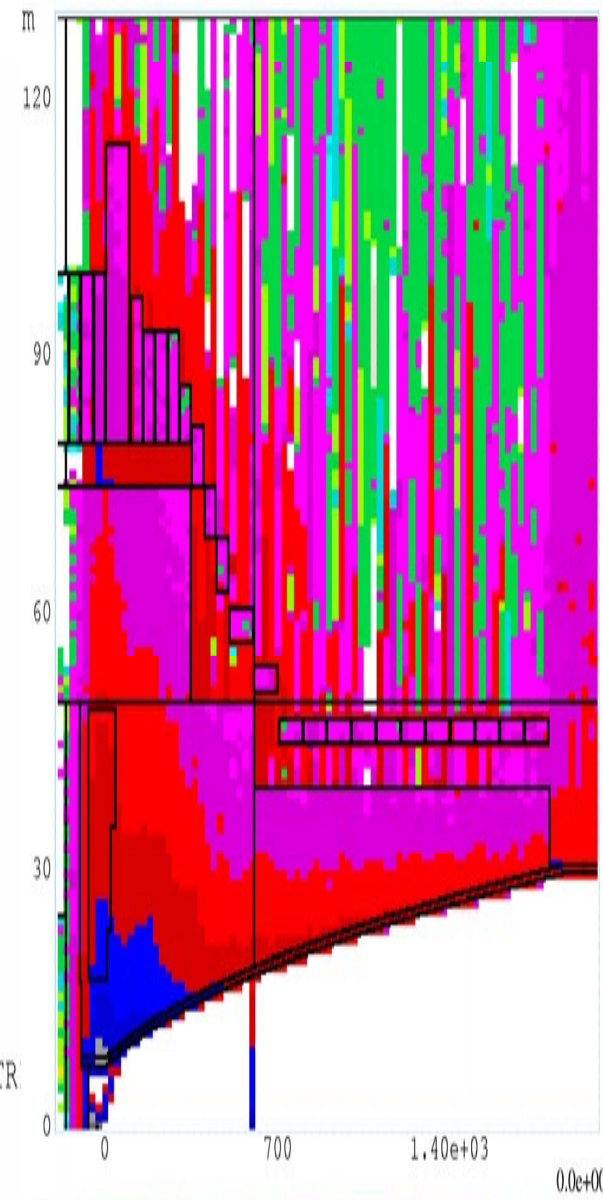
ENERGY DISTRIBUTION GAUSSIAN PROFILE E=7.5 GeV



ENERGY DISTRIBUTION GAUSSIAN PROFILE 0.12,0.12 E=8 GeV



Y DISTRIBUTION GAUSSIAN PROFILE E=8.5 GeV



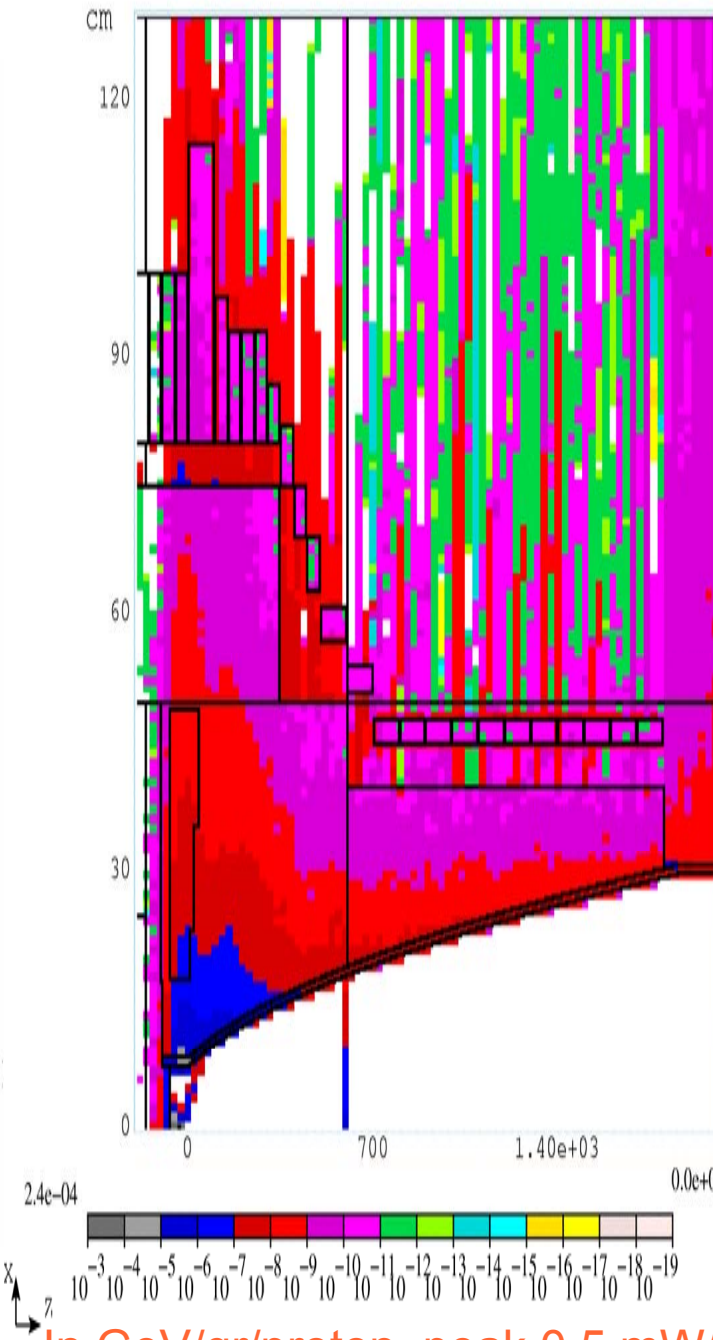
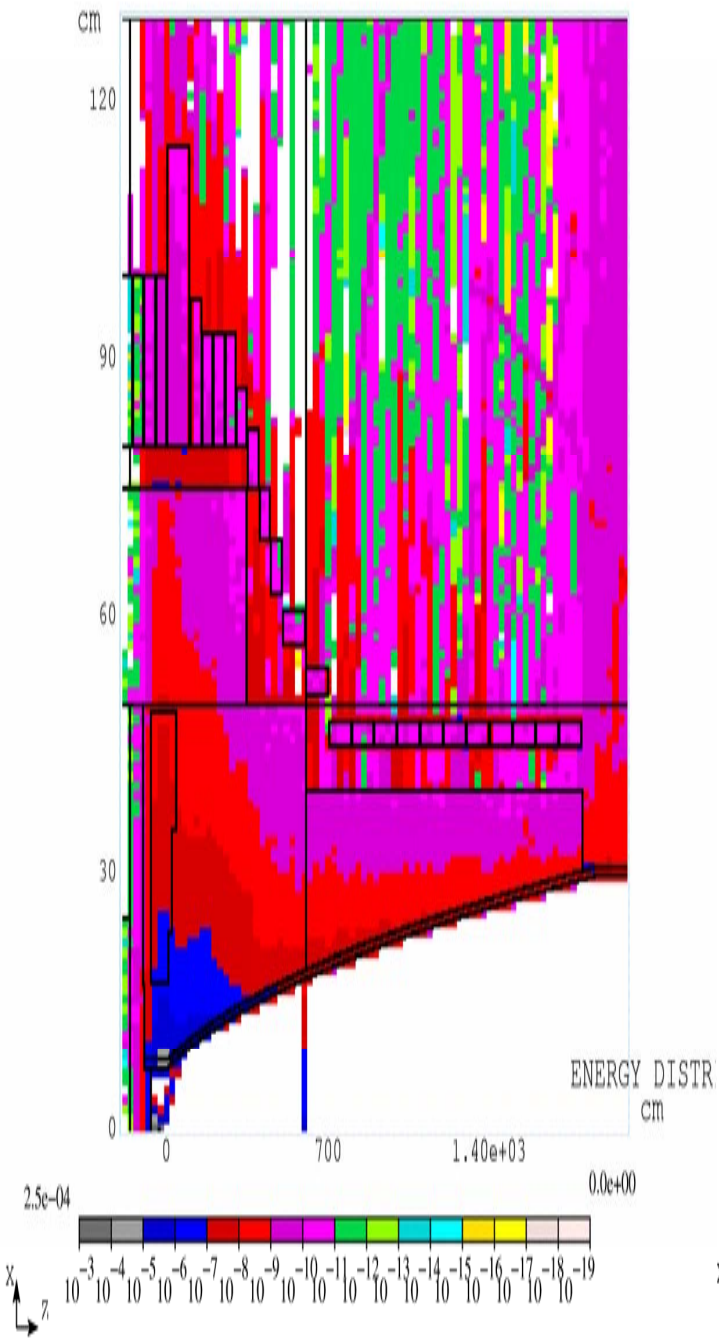
In GeV/gr/proton, peak 0.5 mW/gr



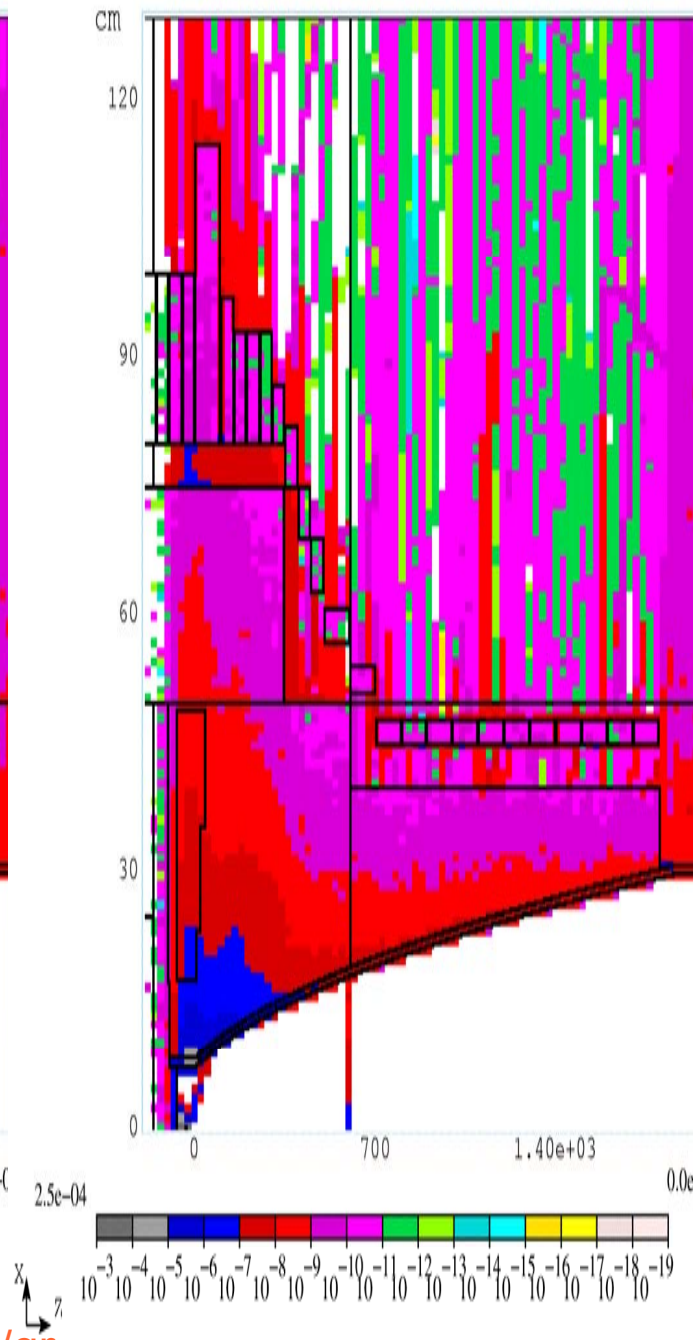
ENERGY DISTRIBUTION GAUSSIAN PROFILE 0.12,0.12 E=8 GeV

MARS WITH 20 MeV NEUTRON ENERGY CUTOFF, GAUSSIAN

MARS+MCNP WITH 20 MeV NEUTRON ENERGY CUTOFF, GAUSSIAN



In GeV/gr/proton, peak 0.5 mW/gr



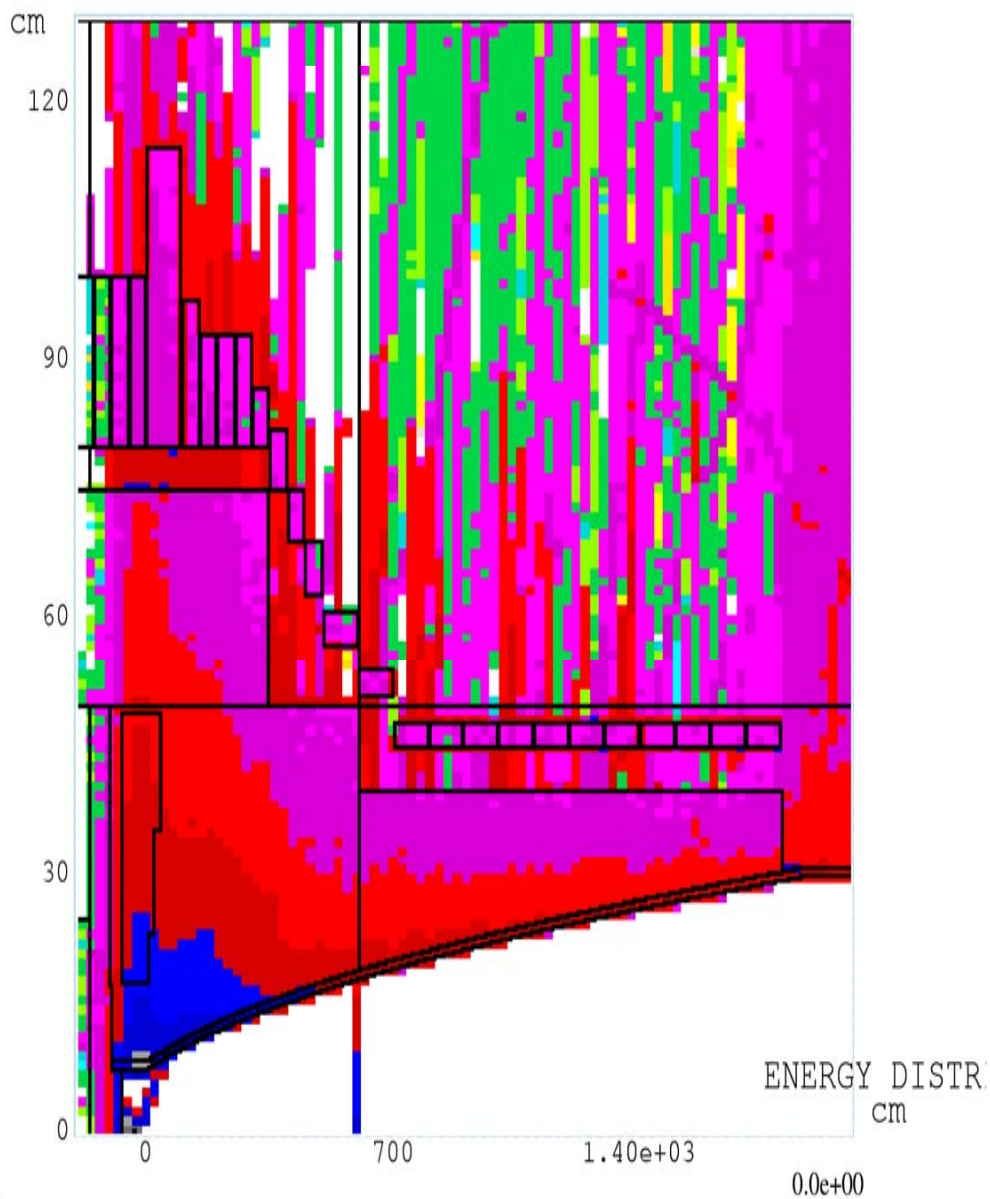
Aspect Ratio: X:Z = 1:16.9230

Aspect Ratio: X:Z = 1:16.9230

Aspect Ratio: X:Z = 1:16.9230

ENERGY DISTRIBUTION GAUSSIAN PROFILE 0.12,0.12 E=8 GeV

MARS+MCNP GAUSSIAN 0.16, 0.16 E=8 GeV



In GeV/gr/proton, peak 0.5 mW/gr

# SUM-UP, COMMENTS AND CONCLUSIONS(standard)

**b-->** about 46 % decrease in deposited energy in G1, 42% in G2, about same in G3, 12% decrease in G4, 31% in the total energy: MORE THAN 40% OF THE DEPOSITED ENERGY IN G1, G2 IS DUE TO LOW ENERGY NEUTRONS, MUCH LESS IN G4.  
LOW ENERGY NEUTRONS ACCOUNT FOR ABOUT 30% OF THE TOTAL ENERGY DEPOSITED IN THE SC SOLENOIDS.

**c-->(MARS+MCNP):** about 12 % increase in deposited energy in G1, 4% in G2, 13% decrease in G3 and 4% decrease in G4, 4% increase in total energy: MARS HANDLES PRETTY GOOD THE LOW ENERGY NEUTRONS FOR THIS CONFIGURATION.

**d-->(MARS+MCNP):** low energy neutrons add about 46 % in energy in G1, 45% in G2, a 19% increase G3 (?), a 10% decrease in G4, 31% decrease in total energy:  
AGAIN WE SEE LOW ENERGY NEUTRONS CONTRIBUTE MOST OF THE DEPOSITED ENERGY IN G1 AND G2 AND MUCH LESS IN G4.  
G3 INCREASE IS A RESULT OF MORE ACCURATE HANDLING OF LOW ENERGY NEUTRONS BY MCNP??



# SUM-UP, COMMENTS AND CONCLUSIONS(super-enhanced)

**b-->** about 15 % decrease in deposited energy in G2, G3, 11% increase in G4: SHOWS CONTRIBUTION FROM TAIL PROTONS IN G2+G3, BUT WHY THE INCREASE IN G4. BETTER STATISTICS?

TOTAL ENERGY ABOUT THE SAME SO WE HAVE DEPOSITED ENERGY REDISTRIBUTION.

SO: INDICATIONS OF IMPORTANCE OF TAIL PROTONS AND/OR THEIR STATISTICAL UNCERTAINTIES?

**c-->** about 5% decrease in G1, G4, about the same for G2, 10 % decrease in G3: INDICATIONS OF EFFECTS OF A BETTER STATISTICS FOR TAIL PROTONS? ABOUT 5% DECREASE IN TOTAL ENERGY. IS THIS THE OVERESTIMATION DUE TO TAIL PROTON UNCERTAINTIES?

NOTICE: WE HAVE CHANGES IN THE TOTAL DEPOSITED ENERGY AND THE DISTRIBUTION.

**d-->** from 4-13 % decrease in the deposited energy in G1, G2, G3, G4. 6% decrease in the total energy: A 6.25 % DECREASE IN PROTONS ENERGY WILL CAUSE A 6 % DECREASE IN THE TOTAL DEPOSITED ENERGY AND IS MOST BENEFICIAL FOR G2 AND G3 SOLENOIDS.

MORE ENERGY IS NOW LOST IN THE SHIELDING?

# SUM-UP, COMMENTS AND CONCLUSIONS(super-enhanced)

cont.

e--> small decrease in G1, G4, about 12% decrease in G2 and a 8% increase in G3. A 6.25 % increase in protons energy will cause a 5 % decrease in the total energy deposited!

REASON(S) ? MORE ENERGY IS NOW CHANNELED SOMEWHERE DOWN THE BEAM LINE?

OR CASCADE PARTICLES GO THROUGH WITH LESS ENERGY DEPOSITED?  
UNLIKE MORE ENERGY TO BE LOST IN THE SHIELDING.

f--> 44% decrease in energy for G2, G3 and about 32 % for G1, G4, 42 % in total:  
LOW ENERGY NEUTRONS (<20 MeV) ACCOUNT FOR ABOUT 40 % OF THE DEPOSITED ENERGY IN THE SOLENOIDS (COMPARED TO ABOUT 30% IN THE STANDARD SHIELDING).

LOW ENERGY NEUTRONS--> ENERGY MOSTLY GOES TO G1, G4 (IN G1, G2 IN THE STANDARD SHIELDING).

g-->(MARS+MCNP): 7-10 % increase in G1,G2, G3 deposited energy, 7% decrease in G4 about 7% increase in total. MARS WORKS VERY GOOD FOR LOW ENERGY NEUTRONS....BUT.... NEUTRONS CAN LOOSE MORE ENERGY IN THE SHIELDING, MORE NEUTRONS MAYBE PROCESSED THROUGH MCNP NOW WITH THE SUPER-ENHANCED SHIELDING...BUT... MORE NEUTRONS COULD ALSO BE STOPED IN THE SHIELDING.

SO OVERALL MAYBE A SMALLER NUMBER OF LOW ENERGY p IS PROCESSED IN MCNP THAN IN THE STANDARD SHIELDING, THEREFORE NOT ENOUGH TO MAKE SUCH A BIG DIFFERENCE? FROM CASE c IN TABLE 0.2 IT DOES NOT SEEM SO.

# SUM-UP, COMMENTS AND CONCLUSIONS(super-enhanced)

## cont.

h-->(MARS+MCNP): with 20 MeV neutron energy cutoff, they account for about 36% in G1, 40 % of the energy in G2, G3, and 24% in G4 (vs. 46% for G1, 45% for G2 and 10 % in G4 in standard shielding).

Overall 36% of the energy is due to low energy neutrons (vs. 31% in standard shielding).

MCNP is not activated.

COMPARING h AND f: RESULTS CLOSE BUT NOT THE SAME.

WITH THE 3G GROUPING (WITH WRONG MATERIAL FOR SC#6-10) THOUGH IS CLOSER.

W-H-Y????

-->OVERAL PEAKS OF DEPOSITED ENERGY NEVER EXCEED 0.5 mW/gr , BUT THE DISTRIBUTION MAY CHANGE FOR DIFFERENT CASES. IN STANDARD SHIELDING THE PEAK VALUES ARE OF 5 mW/gr.

In MCNP output file:

warning. unconverged density effect correction set to zero.

What the ...????