

**IDS120j WITHOUT RESISTIVE MAGNETS**

**MODIFYING Hg MODULE (NEW SH#1 REGION + Hg POOL LENGTH)**

**Nicholas Souchlas, PBL (11/29/2012)**

**IDS120j GEOMETRY, NO RESISTIVE MAGNETS: WITH 20 cm GAPS BETWEEN CRYOSTATS**

\*\*\*\*\*

**# MODIFYING Hg MODULE TO SIMULATE VAN GRAVE'S DESIGN.**

**A NEW UNIFIED SHIELDING VOLUME ( SH#1 + SH#4 ) WITHIN CRYO#1 WAS DECIDED DURING THE LAST MEETING AND AN EXTENSION OF THE Hg POOL UPSTREAM UP TO ~ - 100 cm.**

**NEW SHIELDING CONFIGURATION ADDS ~ 8 cm THICK CYLIDRICAL VOLUME OF SHIELDING AT R ~ 50 cm.**

**# RESULTS FROM SIMULATIONS WITH MODIFIED Hg POOL AND SH#1 REGION.**

\*\*\*\*\*

**>SIMULATION CODE: MARS1512 ( USING MCNP CROSS-SECTION LIBRARIES )**

**>NEUTRON-ENERGY CUTOFF:  $10^{-11}$  MeV**

**>SHIELDING: 60% W + 40% He ( WITH STST VESSELS)**

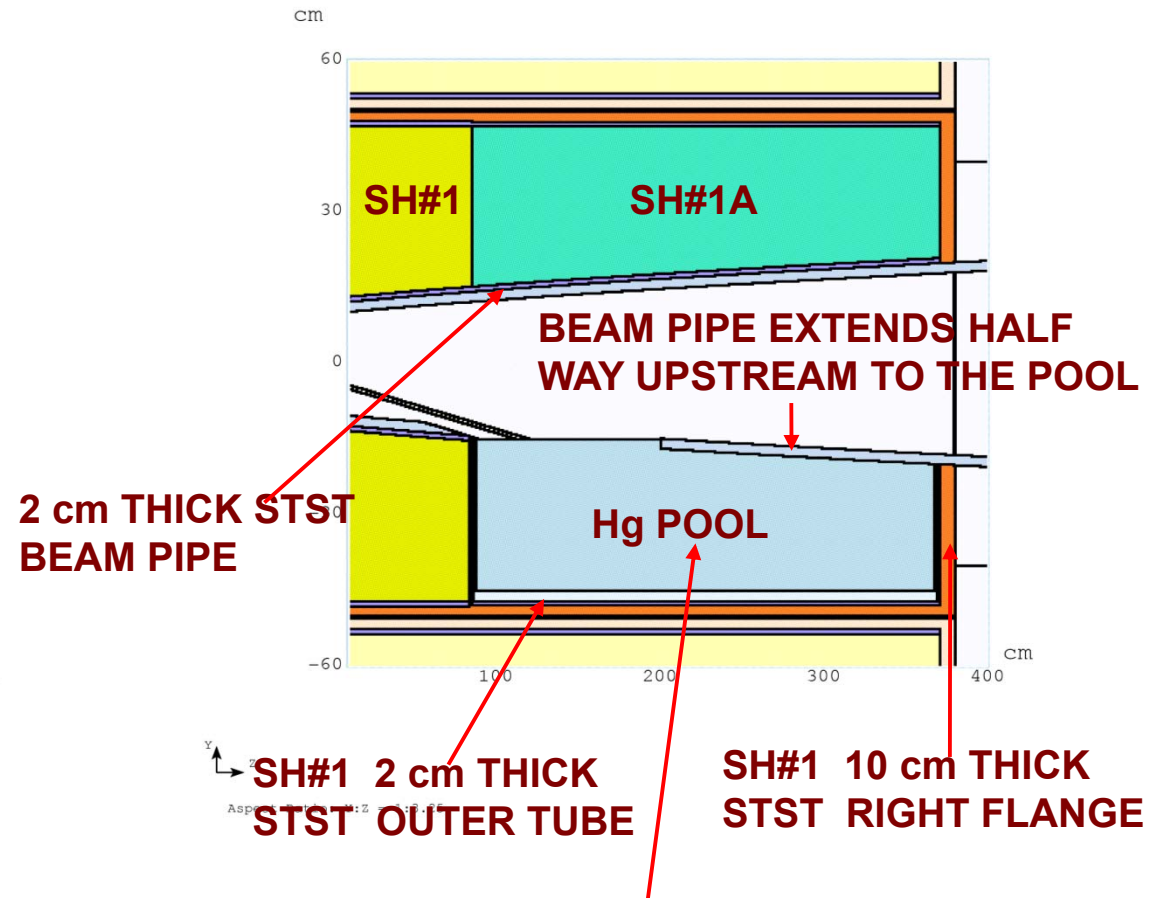
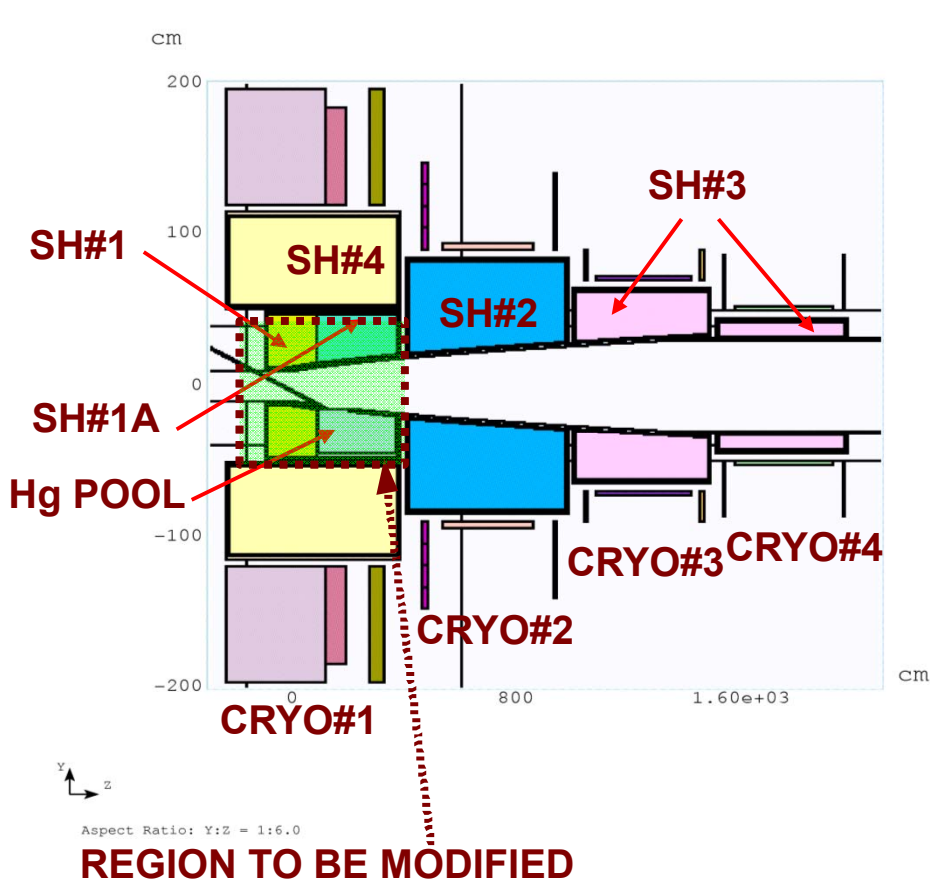
**>PROTON BEAM POWER: 4 MW**

**>PROTON ENERGY: E = 8 GeV**

**>PROTON BEAM PROFILE: GAUSSIAN,  $\sigma_x = \sigma_y = 0.12$  cm**

**>EVENTS IN SIMULATIONS :  $N_p = 500,000$  ( OR 4 x 500,000 FOR SC#1+2)**

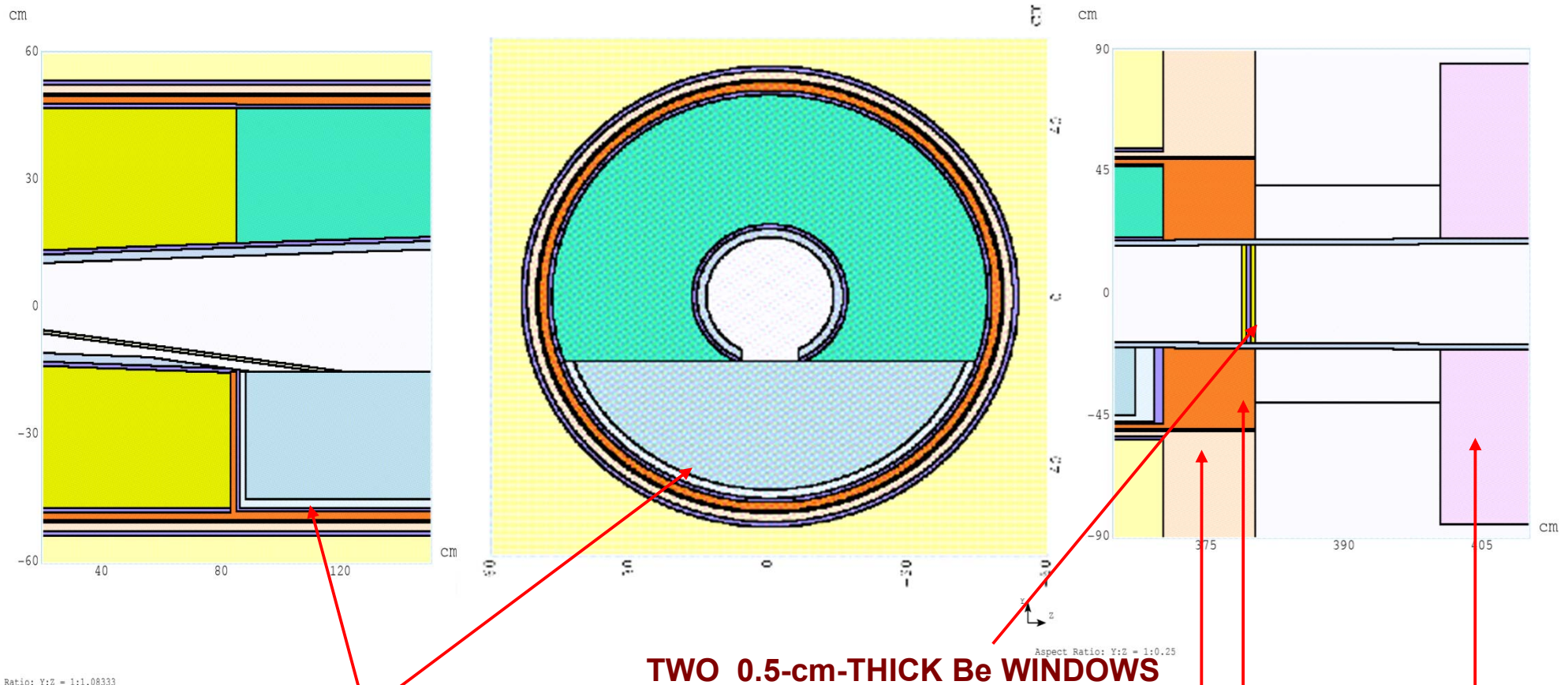
**IDS120j: GENERAL OVERVIEW (LEFT), POOL REGION DETAILS (RIGHT). [20 cm GAPS]**



**Hg POOL STARTS ~ 85 cm AND EXTENDS ALL THE WAY TO THE END OF THE FIRST CRYOSTAT ~ 370 cm.**

**THE NEW Hg POOL MODULE WILL DISPLACE A LARGE VOLUME OF SHIELDING MATERIAL IN SH#1 AND THE FIRST HALF OF SH#1A (TOP VOLUME REGION), AS WELL AS FROM THE BOTTOM VOLUME, BEFORE THE Hg POOL (UPSTREAM), WHERE IT IS MOSTLY NEEDED FOR THE PROTECTION OF SC#1 – SC#4 [INNER Hg MODULE, NOW EXTENDED UPSTREAM ALL THE WAY AT THE BEGINNING OF THE SC#1]. UPDATED CONFIGURATION UNIFIES SH#1 AND SH#4 VOLUMES AND EXTENDS Hg POOL UPSTREAM UP TO ~ -100 cm.**

**IDS120j: WITHOUT RESISTIVE MAGNETS. DETAILS OF THE DOUBLE STST Hg POOL VESSEL (LEFT, MIDDLE) AND THE DOUBLE Be WINDOW (RIGHT). [20-cm GAPS]**

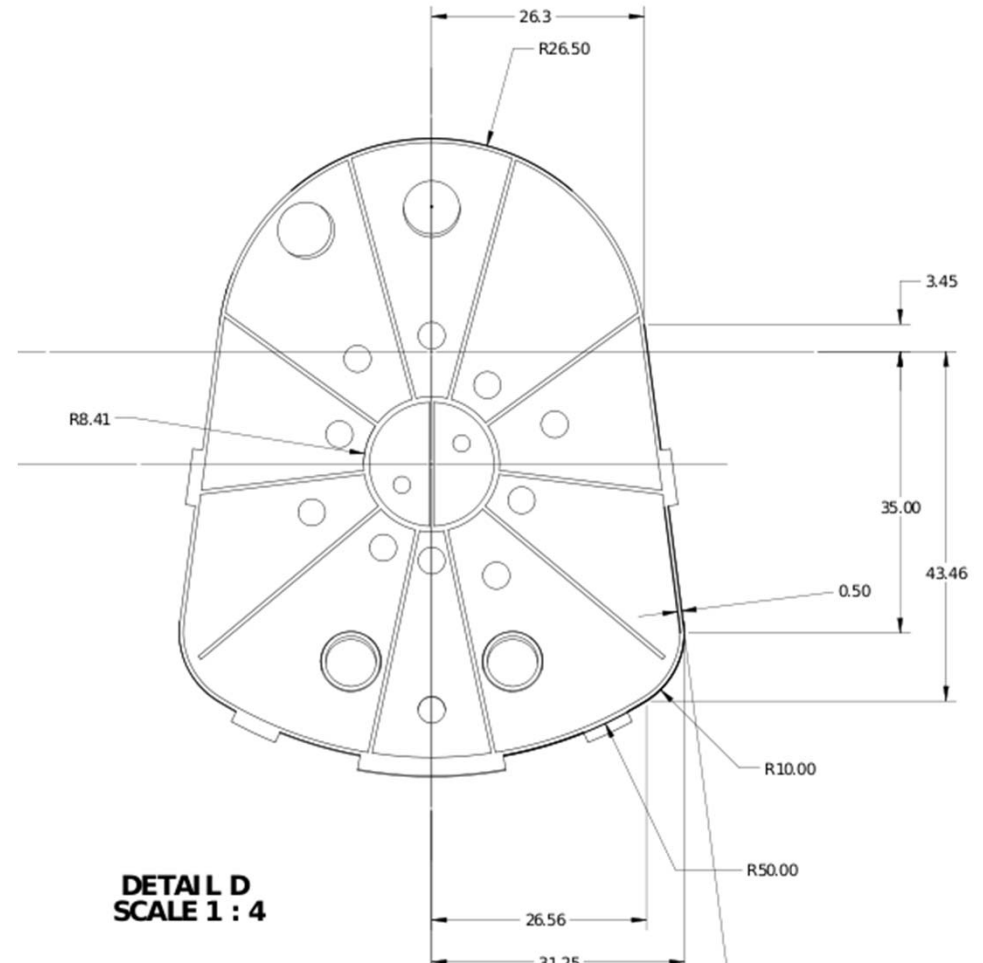
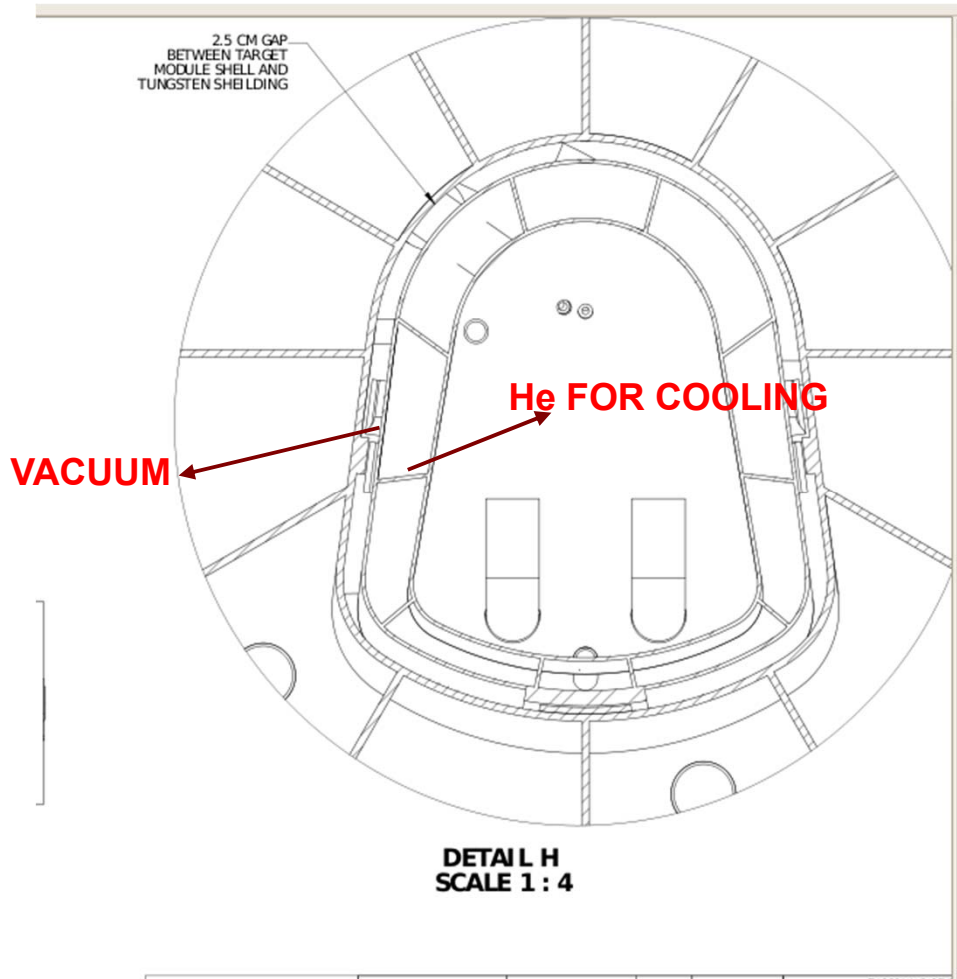


**2 cm THICK STST INNER Hg POOL VESSEL WITH 1-cm He GAP FOR COOLING.**

**TWO 0.5-cm-THICK Be WINDOWS AT THE END OF CRYO#1 WITH 0.5-cm He GAP BETWEEN THEM FOR COOLING.**

**10-cm-THICK STST RIGHT / LEFT FLANGE OF SHVS#4, SHVS#1 / SHVS#2 WITH 20-cm GAP BETWEEN THEM.**

**IDS120j: y-z CROSS SECTIONS WITH DETAILS OF Hg POOL MODULE, FROM VAN GRAVE'S PRESENTATION ( 8 / 9 / 2012 ).**

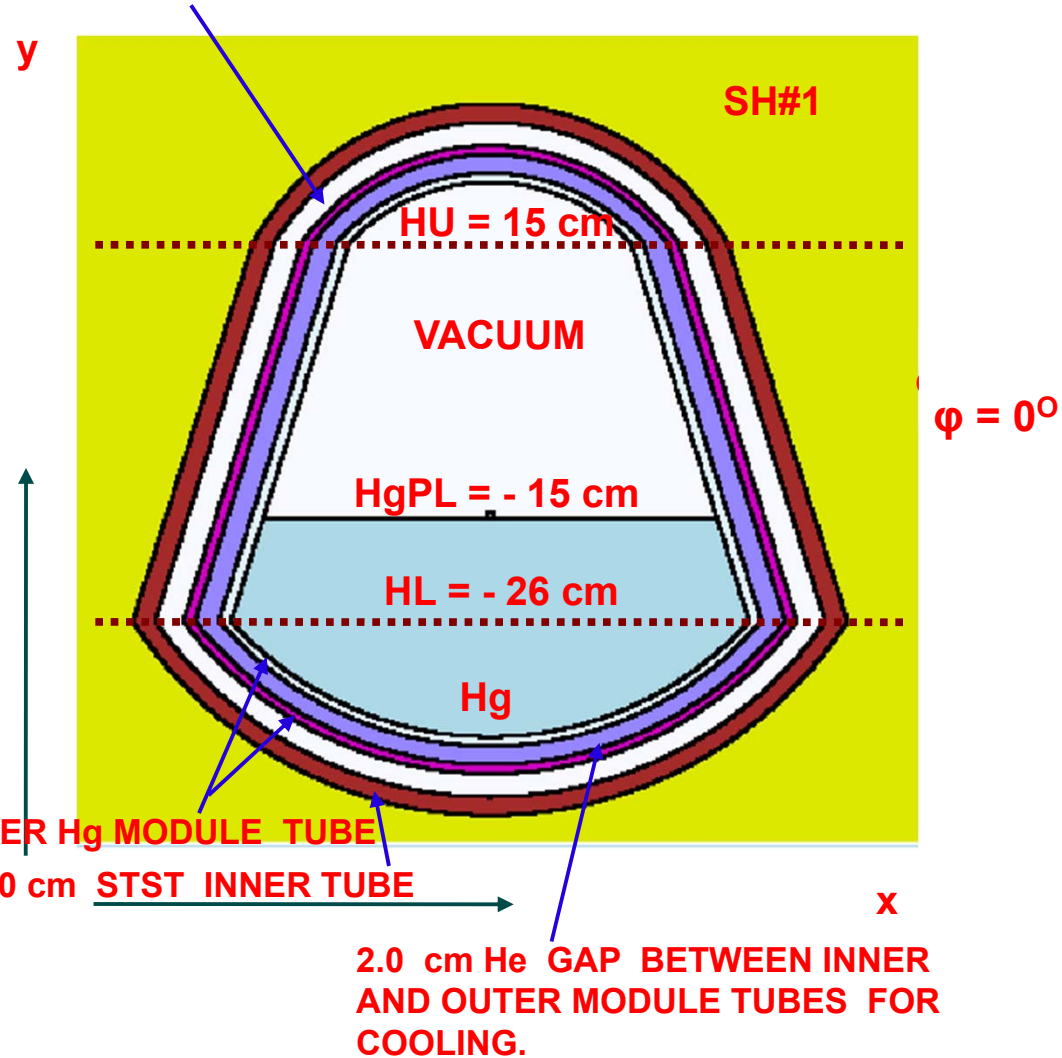
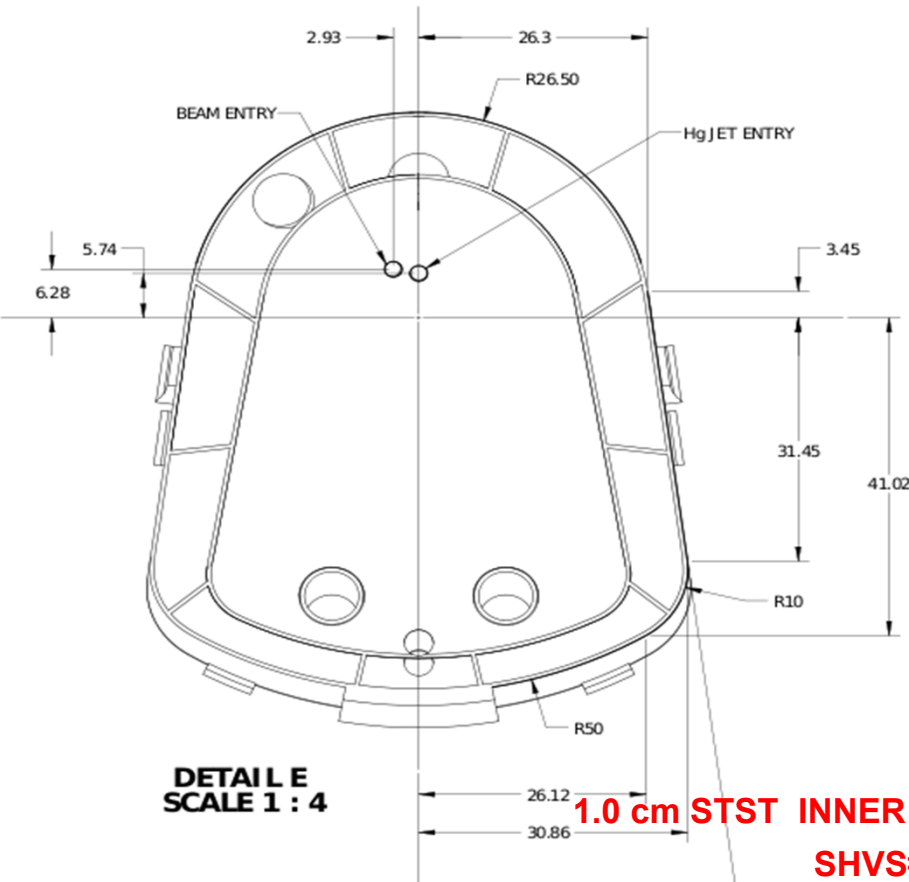


**THE DESIGN REQUIRES A 2.5-cm ! GAP BETWEEN SH#1 INNER VESSEL AND Hg POOL MODULE OUTER VESSEL. AN EVEN LARGER GAP APPEARS BETWEEN INNER AND OUTER VESSEL OF THE Hg POOL MODULE FOR THE FLOW OF He GAS FOR COOLING THE POOL. THE RADIUS OF THE UPPER HALF SEMICIRCULAR SECTION OF INNER Hg POOL VESSEL WILL BE 26.5 cm, MUCH LARGER THAN THE BEAM-PIPE APERTURE AT THE END OF CRYO#1 (~ 17.7 cm).**



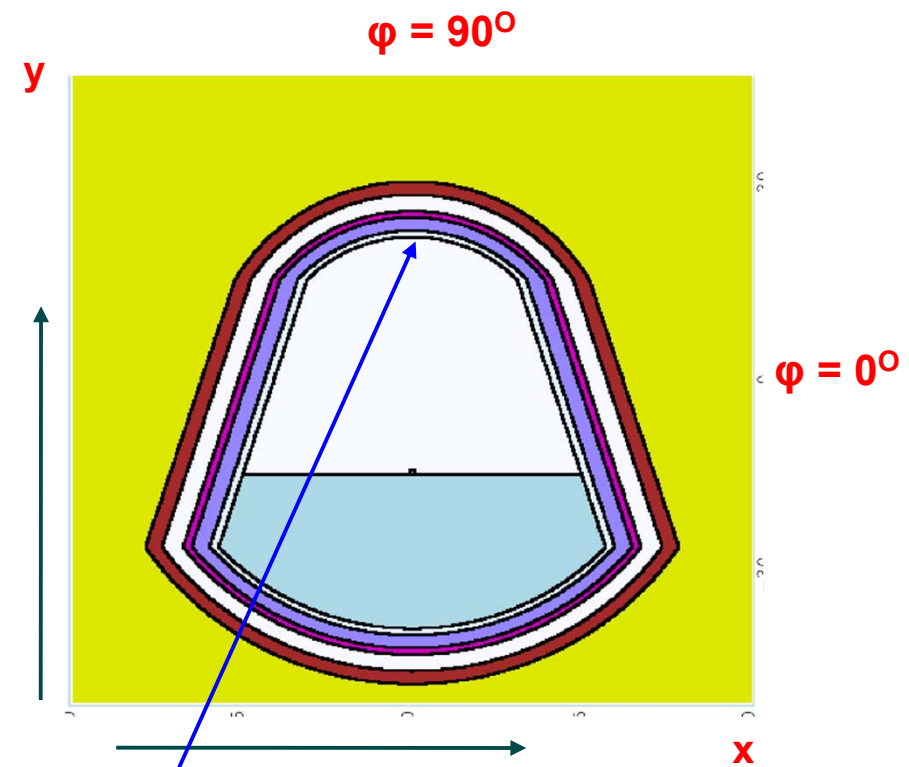
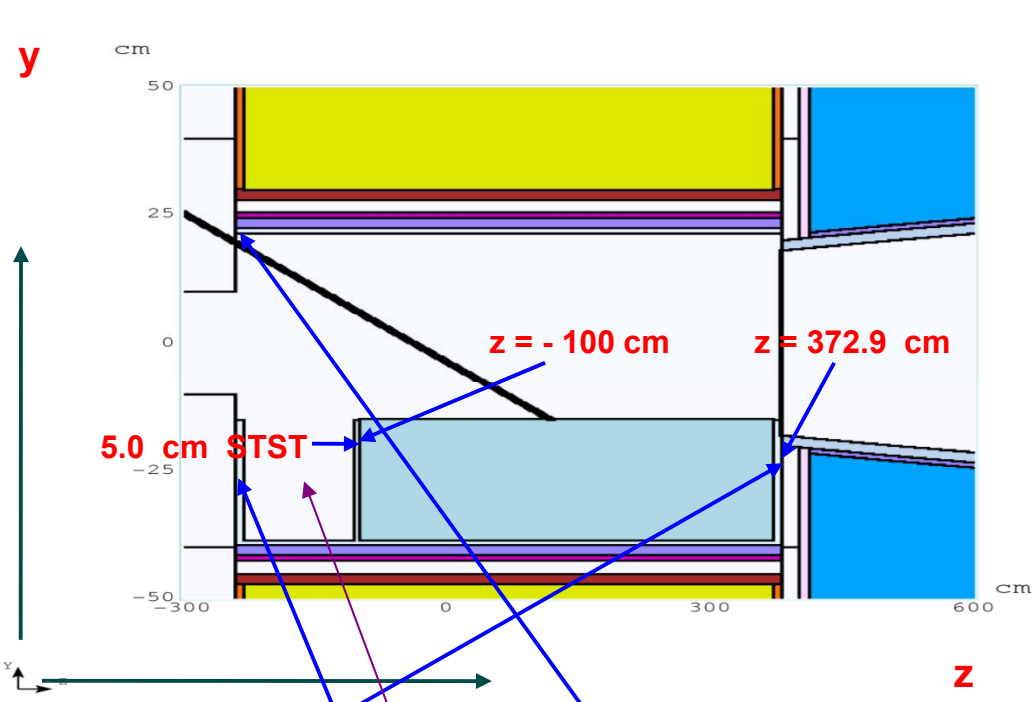
**IDS120j: yx CROSS SECTION WITH DETAILS OF Hg POOL MODULE FROM VAN'S PLOTS ( LEFT ) AND ADAPTED DESIGN FOR MARS SIMULATIONS ( RIGHT ) [ AT z = 100 m ].**

**ADAPTED DESIGN FOR 2% VACUUM GAP BETWEEN SHVS#1 INNER AND Hg MODULE OUTER TUBE**  $\phi = 90^\circ$



**EVERYTHING HAS BEEN PARAMETRIZED FOR FUTURE CONVENIENCE. THE HEIGHTS OF THE END POINTS OF THE STRAIGHT SECTIONS ARE HL = - 26 cm AND HU = 15 cm. THE FREE Hg POOL SURFACE IS AT y = - 15 cm. THE RADIUS OF THE LOWER HALF OF THE INNER VESSEL OF THE Hg MODULE IS NOW SMALLER THAN BEFORE : FROM ~ 45 cm ----> ~ 39 cm. THE REST OF THE SPACE BETWEEN SHVS#1 INNER AND OUTER TUBE ( AT R ~ 115 cm ) IS FILLED WITH SHIELDING.**

**IDS120j: y-z ( LEFT ) AND y-x AT z = 10 cm ( RIGHT ) CROSS SECTION WITH DETAILS OF THE NEW Hg MODULE AND THE LOWER HALF OF THE UPSTREAM REGION.**



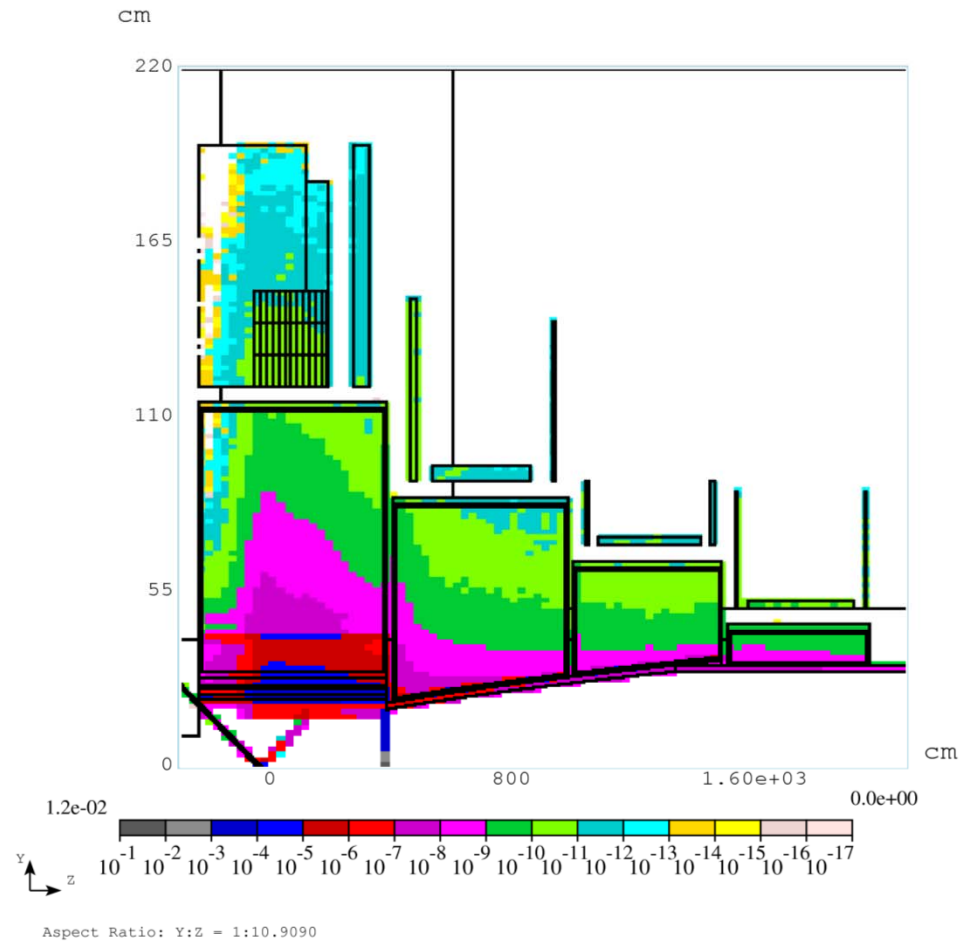
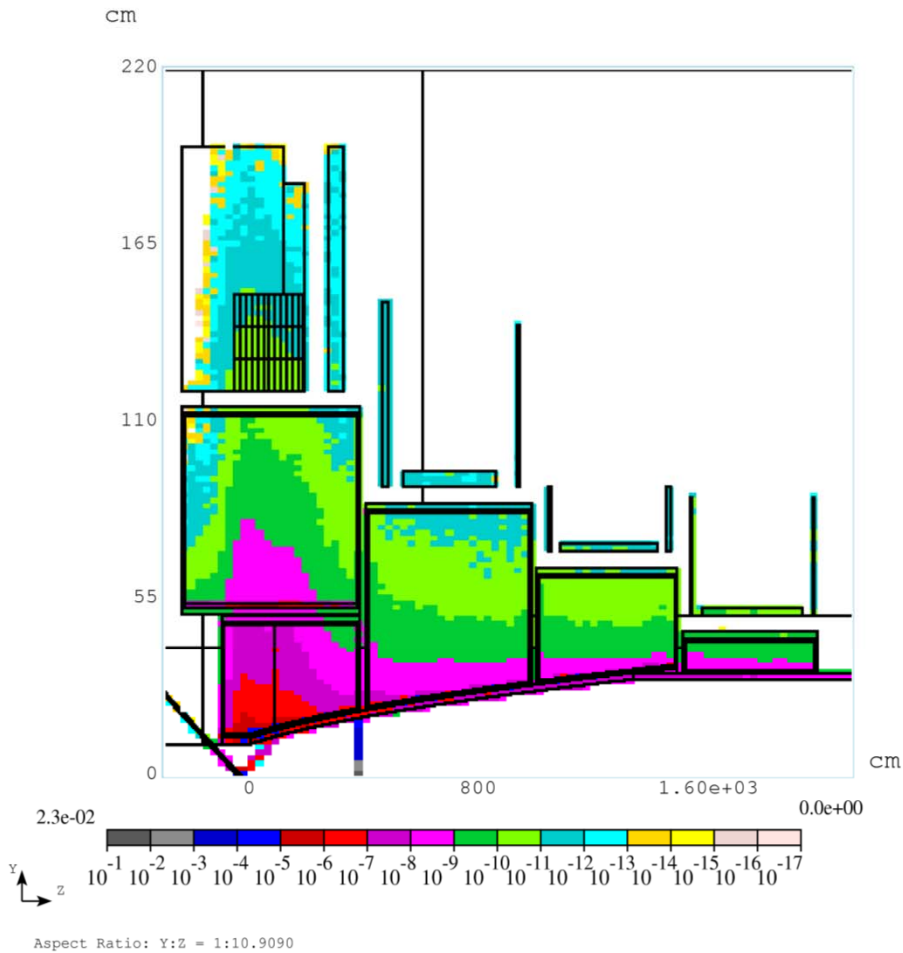
**10-cm-THICK STST FOR THE UPSTREAM AND DOWNSTREAM FLANGE OF Hg MODULE**

**THE RADIUS OF THE TOP SEMICIRCULAR SECTION OF THE Hg INNER TUBE IS SUCH THAT WILL NOT INTERFERE WITH THE Hg JET AND THE BEAM PROTONS AT THE BEGINNING OF CRYO#1 ( z ~ - 240 cm )**

# ACCORDING TO VAN'S DESIGN, THE VOLUME FROM THE BEGINNING OF CRYO#1 ( z ~ - 240 cm ) TO THE BEGINNING OF THE Hg POOL ( z ~ - 100 cm ) AND FROM y ~ -15 cm TO THE BOTTOM OF THE Hg MODULE INNER VESSEL ( R ~ 39 cm ) WILL BE EMPTY, TO ACCOMODATE THE PIPES AND OTHER COMPONENTS OF THE Hg POOL MODULE.

# SOME IMPROVEMENT IN SHIELDING IS ACHIEVED BY UNIFYING H#1 AND SH#4. THERE WILL BE SIGNIFICANT INCREASE IN THE SHIELDING MASS ( > 200 tons ), TO BE CONTAINED IN THE NEW VESSEL, => GREATER ASYMMETRY IN THE WEIGHT DISTRIBUTION. He COOLING OF SUCH A LARGE OLUME ( > 22 m<sup>3</sup> ) OF SHIELDING CAN BE CHALENGING.

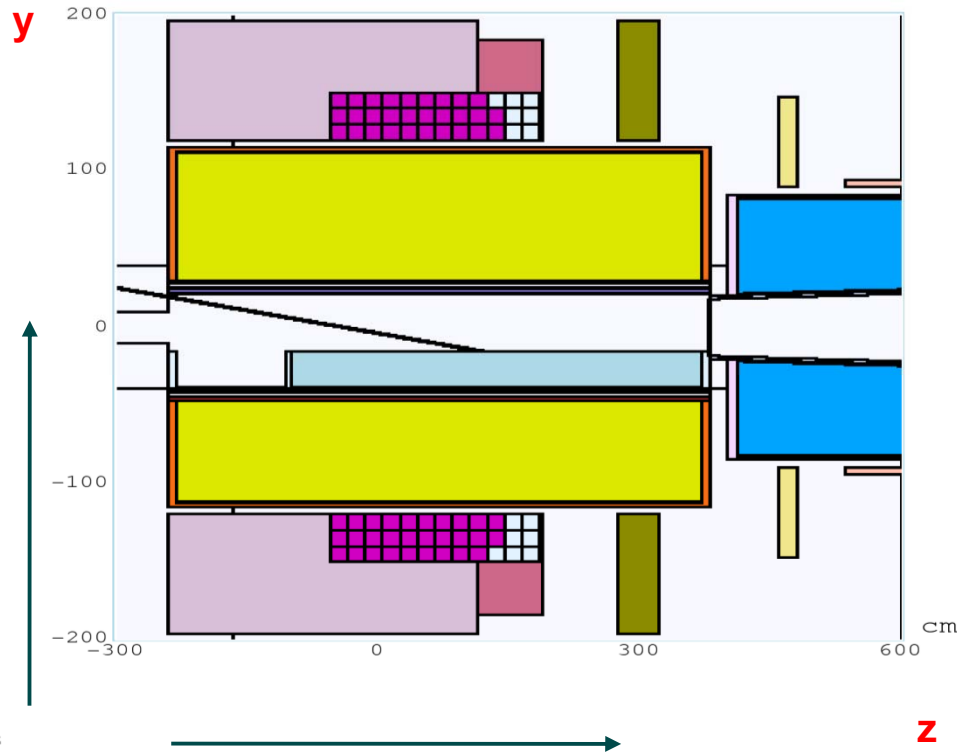
# IDS120j: y-z CROSS SECTION FOR THE AZIMUTHALLY AVERAGED TDPD WITH THE OLD Hg POOL VESSEL ( LEFT ) AND THE NEW ONE ( RIGHT ) [ P12 POINT ].



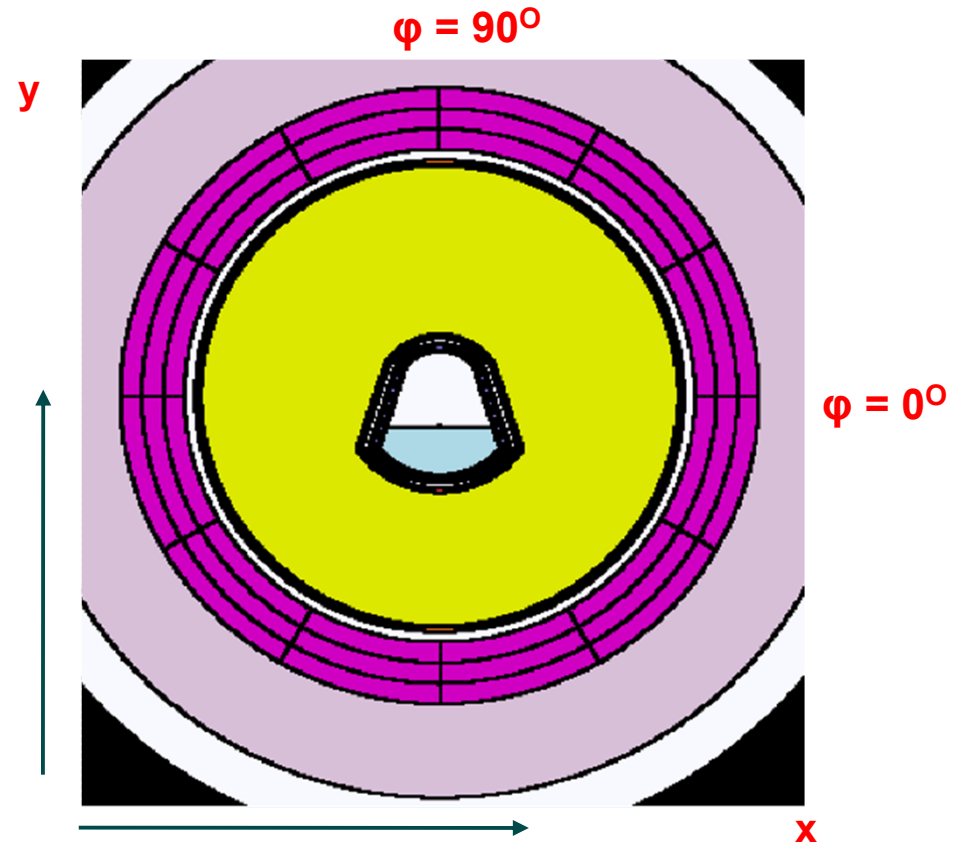
# COMPARISON OF THE AZIMUTHALLY AVERAGED TDPD (Total Deposited Power Density) BETWEEN OLD AND UPDATED Hg MODULE REVEALS A SIGNIFICANT INCREASE IN THE RADIAL SPREAD OF THE TDPD AROUND THE TARGET REGION, AS WELL AS SPREADING FURTHER DOWNSTREAM ( CRYO#2 SHIELDING REGION ).  
COLOR SCALE IS SAME FOR BOTH PLOTS.



**IDS120j: y-z ( LEFT ) AND y-x CROSS SECTION WITH DETAILS OF THE SC#1+2 SEGMENTATION**



Aspect Ratio: Y:Z = 1:2.25

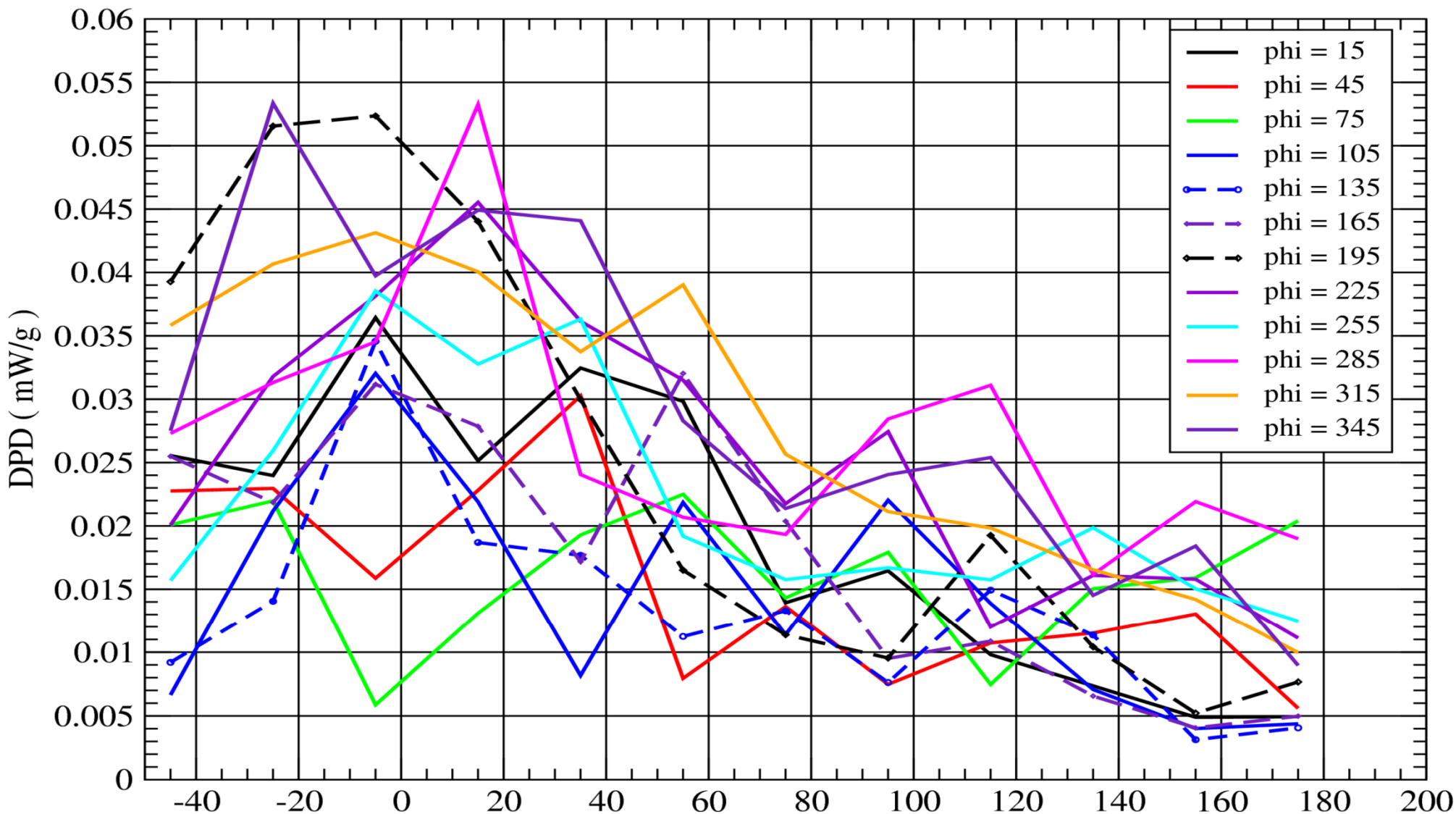


$120.0 < r < 150.0$  cm       $dr = 10.0$  cm       $N_r = 3$  bins  
 $- 55.0 < z < 185.0$  cm       $dz = 20.0$  cm       $N_z = 12$  bins  
 $0.0 < \phi < 360.0$  deg.       $d\phi = 30$  deg.       $N_\phi = 12$  bins  
 $N_{tot} = 432$  "pieces"

**ONLY THE AREA WITH HIGHEST AVERAGE AZIMUTHAL DPD ( DETERMINED FROM MARS PLOTS ) WAS STUDIED.**

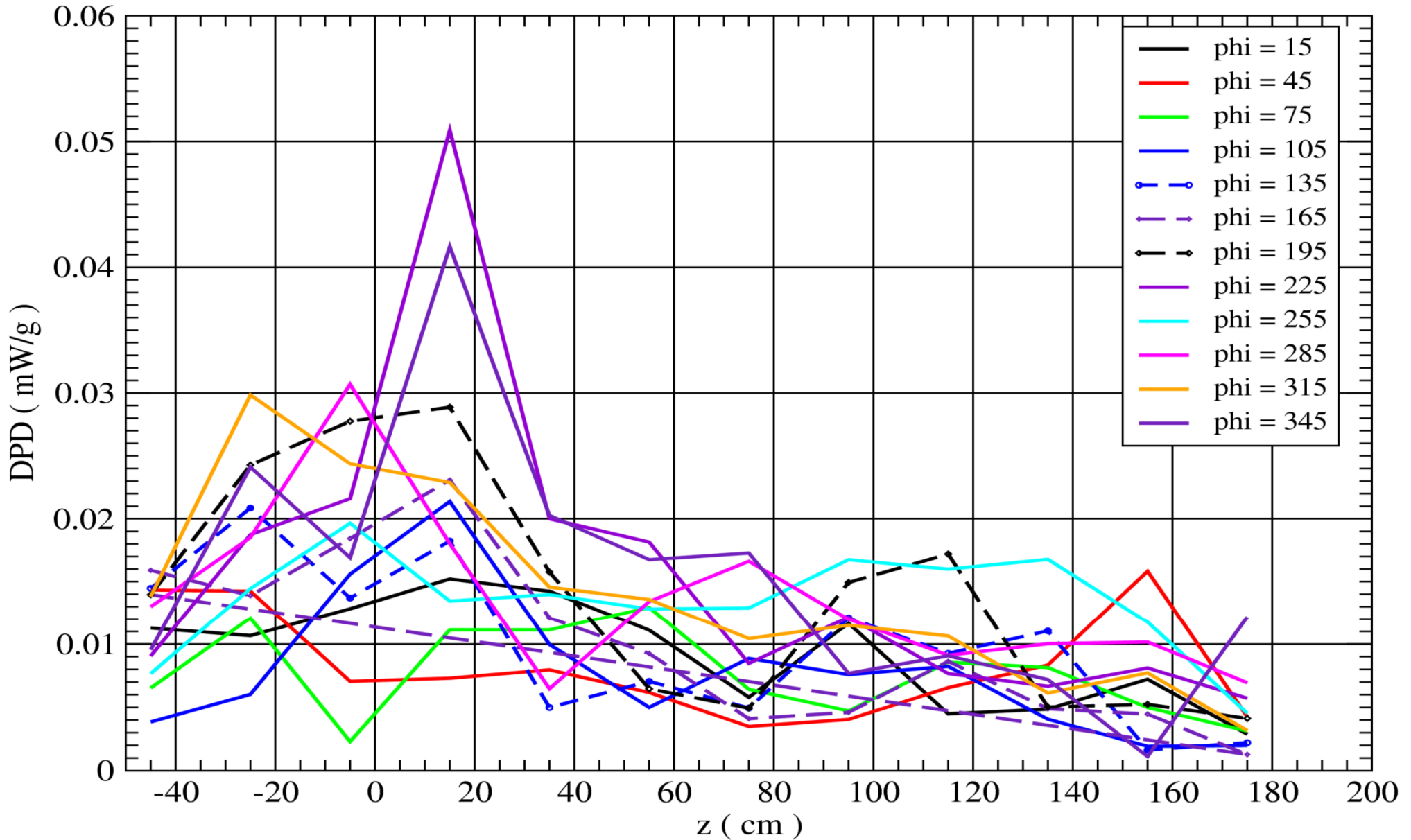
SC1 + SC2 DPD vs. z FOR 12 ANGLES AND r = 125 cm, "HOT REGION" [ -55 < z < 185 cm, 120 < r < 150 cm ]

(dr, dz, dphi) = ( 10 cm, 20 cm, 30 deg)--> ( 3, 12, 12 ) #BINS



PEAK TDPD < 0.06 mW / g. MOST OF THE DP IS BETWEEN ~ - 40 < z < 40 cm AND IN THE LOWER HALF OF SC#1+2, TOWARDS THE + x DIRECTION. THIS IS THE RESULT OF REPLACING SHIELDING MATERIAL AT THE BOTTOM PART OF THE Hg MODULE WITH LIQUID Hg. THE NEGATIVE IMPACT OF THE NEW Hg MODULE IN SH#1 IS GREATLY MITIGATED BY THE INTRODUCTION OF ~ 8 cm THICK CYLIDRICAL SHIELDING VOLUME AT R ~ 50 cm WHEN SH#1 AND SH#4 ARE UNIFIED INTO ONE VOLUME.

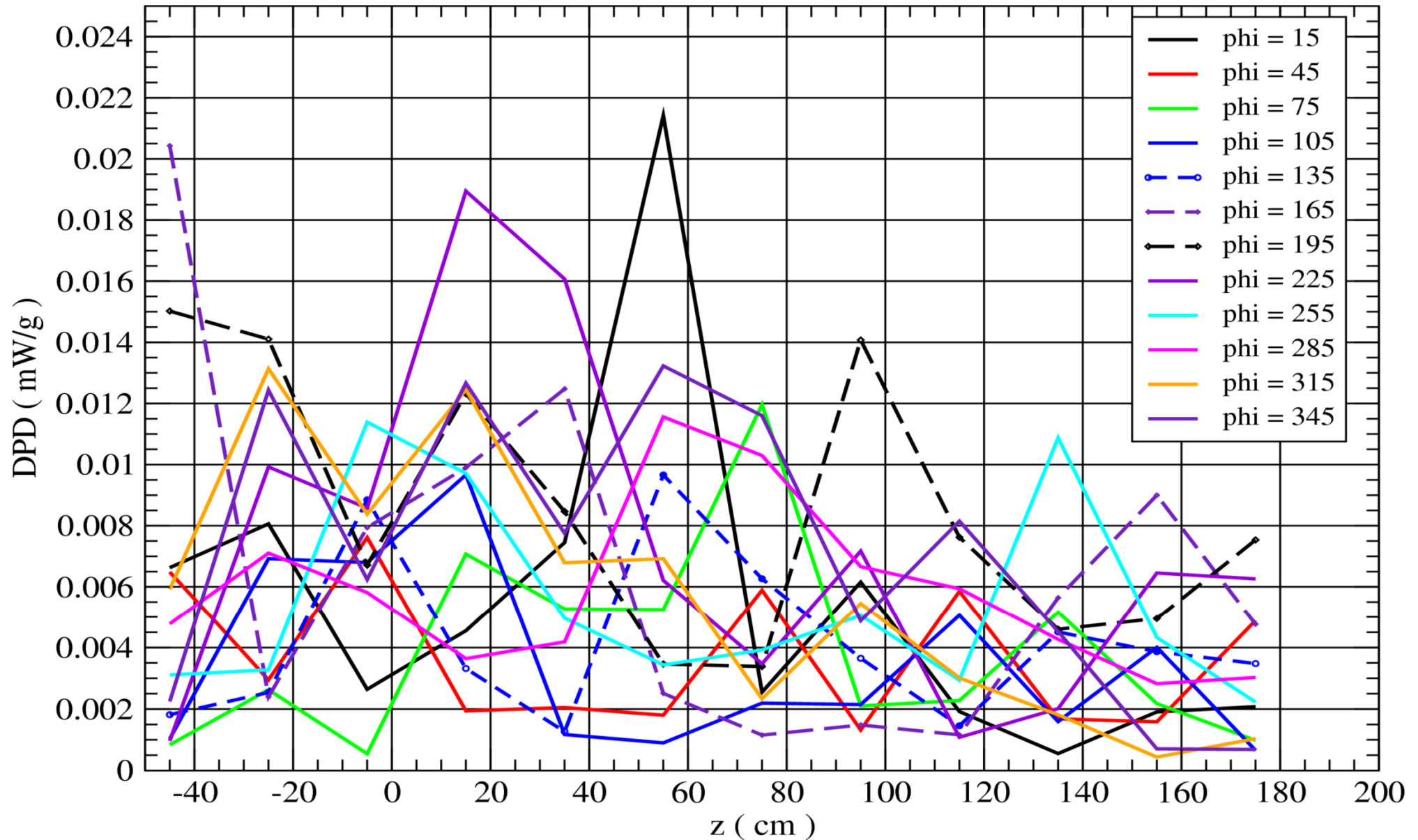
(dr, dz, dphi) = ( 10 cm, 20 cm, 30 deg)--> ( 3, 12, 12 ) #BINS



PEAK TDPD < 0.05 mW / g. STILL QUITE HIGH FOR THESE  $r = 135$  cm RADIUS PIECES. AS BEFORE, MOST OF THE DP IS BETWEEN  $\sim -40 < z < 40$  cm AND IN THE LOWER HALF OF SC#1+2, TOWARDS THE + x DIRECTION.

SC1 + SC2 DPD vs. z FOR 12 ANGLES AND  $r = 145$  cm, "HOT REGION" [  $-55 < z < 185$  cm,  $120 < r < 150$  cm ]

$(dr, dz, dphi) = (10$  cm, 20 cm, 30 deg) $--> (3, 12, 12)$  #BINS



PEAK TDPD  $< 0.02$  mW / g FOR THE  $r = 145$  cm RADIUS PIECES. MORE UNIFORMITY IN AZIMUTHAL TDPD DISTRIBUTION NOW. ONE CAN COMPARE THESE PLOTS WITH THE ONES IN 9 / 20 / 2012 PRESENTATION WITH THE RESULTS FROM THE OLD Hg MODULE.

....

- A) THE PEAK DPD IN SC#1+2 IS  $\sim 0.05$  mW / g AT  $(r, z, \phi) = (125 \text{ cm}, -25 \text{ cm}, 345 \text{ deg})$  IN SC#1 LOWER HALF OF THE COIL ( $y < 0, x > 0$ ) CLOSE TO THE -y AXIS.
- B) 0.725 kW OF DEPOSITED POWER IN THE SC#1+2 JUST IN THE SEGMENTED VOLUME.  
ABOUT 0.882 kW IN BOTH COILS SC#1+2 [ GOOD NEWS ].  
DEPOSITED POWER IN ALL 12 SCs  $\sim 1.31$  kW [ BAD NEWS ].  
DEPOSITED POWER IN SC#4  $\sim 0.15$  kW IS QUITE HIGH ---> SEGMENTATION STUDIES TO CHECK DPD.
- C) INNER TUBE OF Hg MODULE RECEIVES  $\sim 276$  kW WHILE OUTER TUBE  $\sim 166$  kW [ BOTH 1 cm THICK STST BELL-LIKE SHAPE ]. INNER TUBE OF SHVS#1 [ 2 cm THICK STST BELL-LIKE SHAPE ] WILL GET  $\sim 165$  kW.
- D) DEPOSITED POWER IN SH#1 :  $\sim 579$  kW  
DEPOSITED POWER IN SH#2 :  $\sim 94$  kW  
DEPOSITED POWER IN SH#3 :  $\sim 10$  kW  
DEPOSITED POWER IN SH#4 :  $\sim 5$  kW
- E) DEPOSITED POWER IN SHVS#1 :  $\sim 3$  kW  
DEPOSITED POWER IN SHVS#2 :  $\sim 41$  kW  
DEPOSITED POWER IN SHVS#3 :  $\sim 4$  kW  
DEPOSITED POWER IN SHVS#5 :  $\sim 0.5$  kW
- F) DEPOSITED POWER IN Hg JET :  $\sim 418$  kW  
DEPOSITED POWER IN Hg POOL :  $\sim 1212$  kW
- G) DEPOSITED POWER IN Be WINDOW :  $\sim 10$  kW  
DEPOSITED POWER IN BP#2 :  $\sim 108$  kW  
DEPOSITED POWER IN BP#3 :  $\sim 19$  kW