

Thermal Shock Measurements and Modelling for Solid High-Power Targets at High Temperatures

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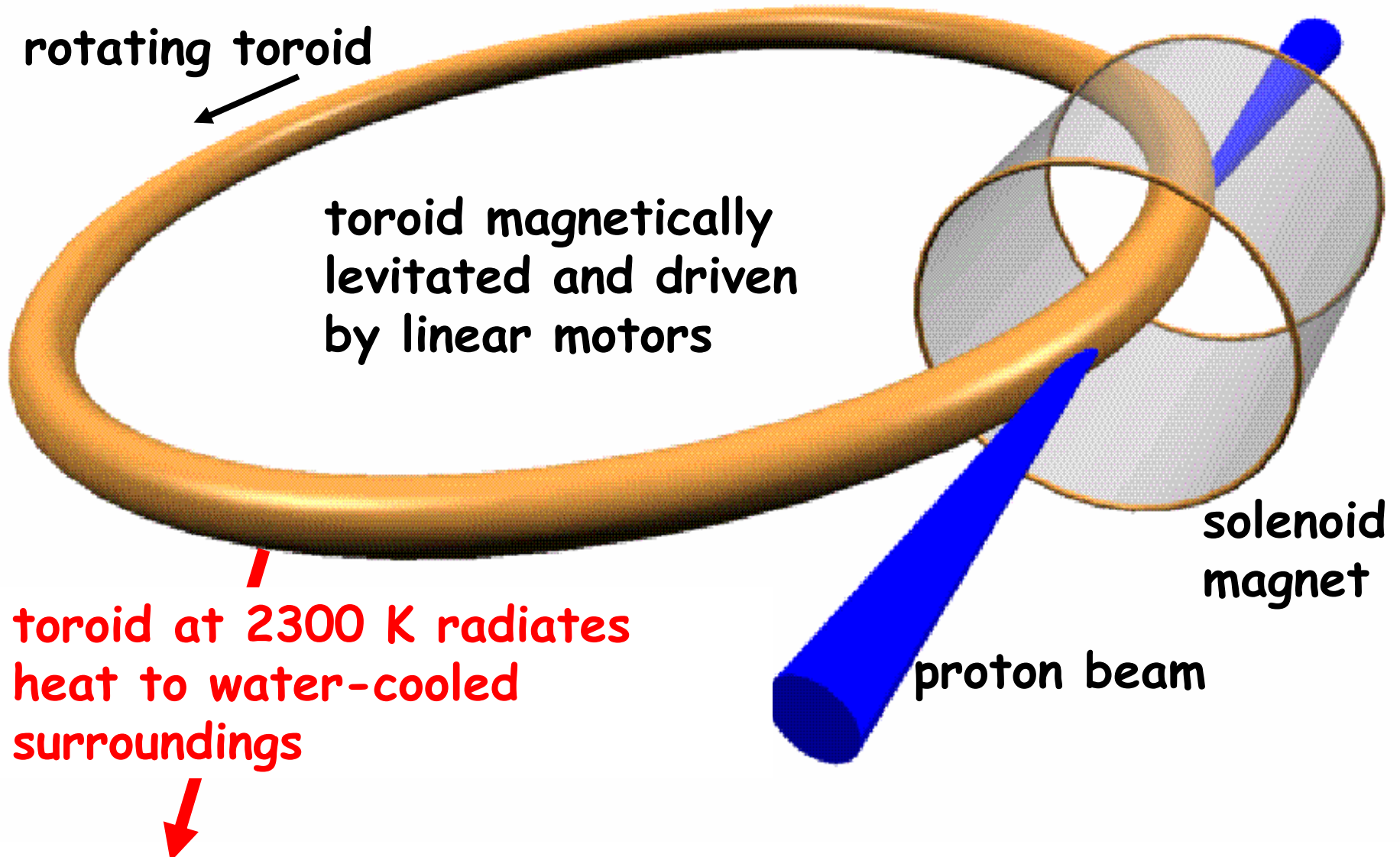
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OUTLINE

1. Introduction
2. Wire tests - an update from NuFact06
3. Fatigue and Creep
4. *Longitudinal versus Transverse Bar Feed*

The original RAL Target concept -
(after Bruce King)

Schematic diagram of the radiation cooled rotating toroidal target



The alternative concept -

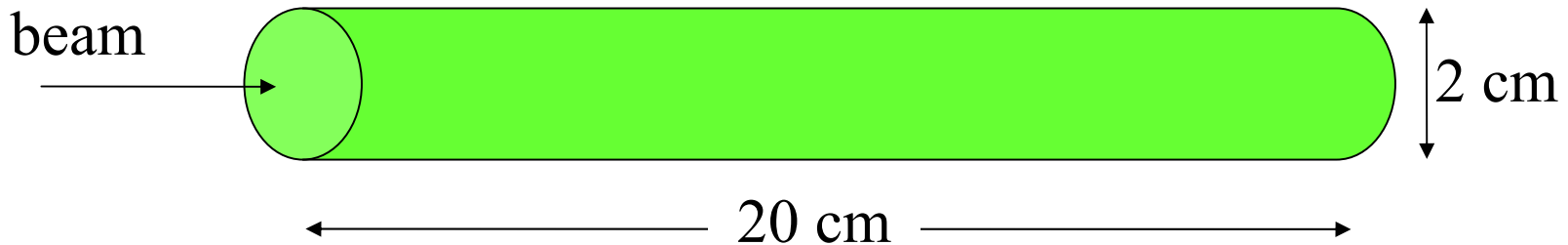
Individual Bar Targets

Target Parameters

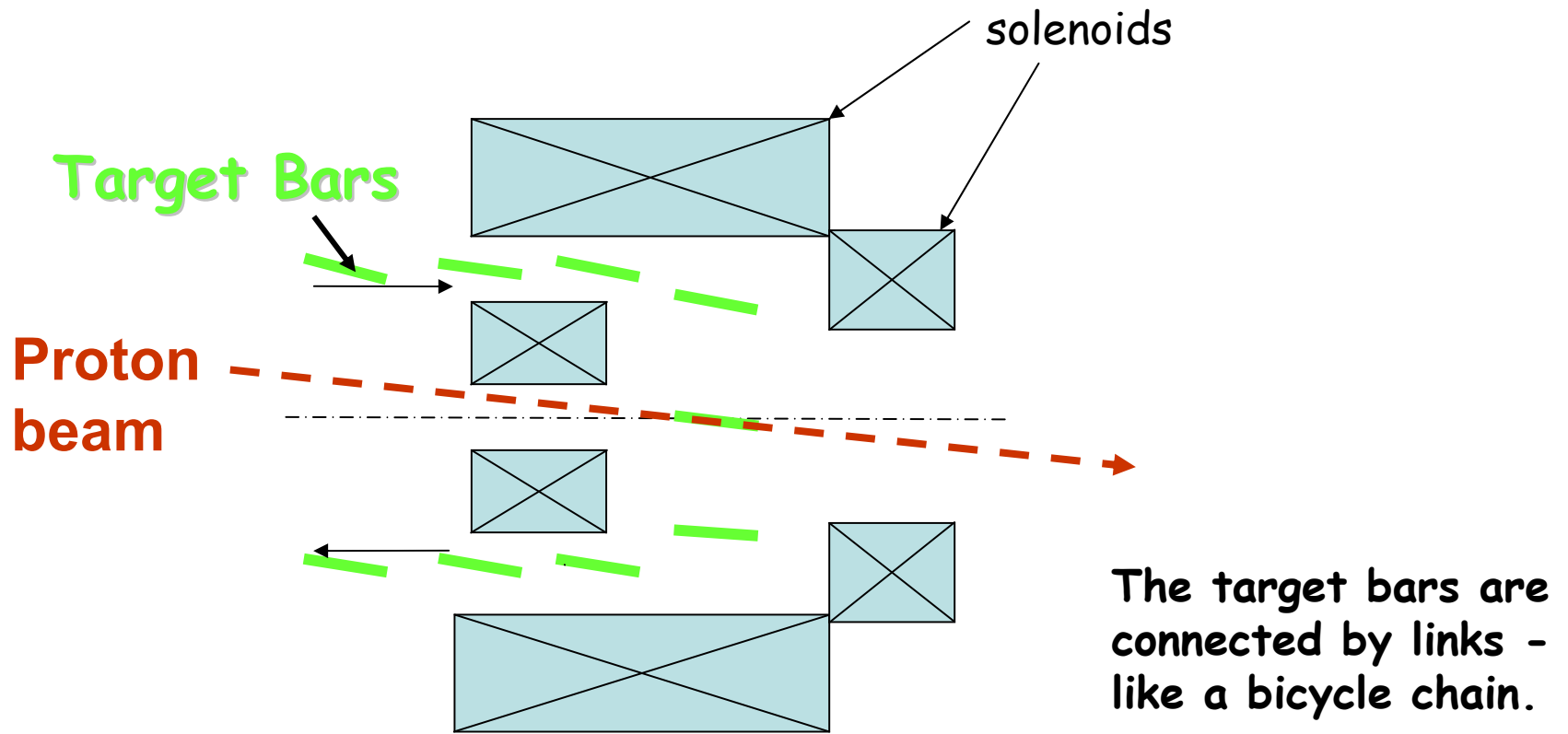
Proton Beam

pulsed	50 Hz
pulse length	$\sim 40 \mu\text{s}$
energy	$\sim 10 \text{ GeV}$
average power	$\sim 4 \text{ MW}$

Target (not a stopping target)



mean power dissipation	1 MW
energy dissipated/pulse	20 kJ (50 Hz)
energy density	300 J cm^{-3} (50 Hz)



Schematic diagram of the target and collector solenoid arrangement

The value of the peak stress is:

$$\sigma_{\max} = \pm E \alpha T$$

With typical values for tungsten:

$$E = 300 \text{ GPa}$$

$$\alpha = 0.9 \times 10^{-5} \text{ K}^{-1}$$

$$T = 100 \text{ K}$$

0.2% Yield Strength = ~20 MPa at 2000 K

UTS = ~100 MPa

$$s_{\max} = 270 \text{ MPa}$$

**Stress exceeds UTS
FAILURE EXPECTED!!**

Real Life is not this simple.

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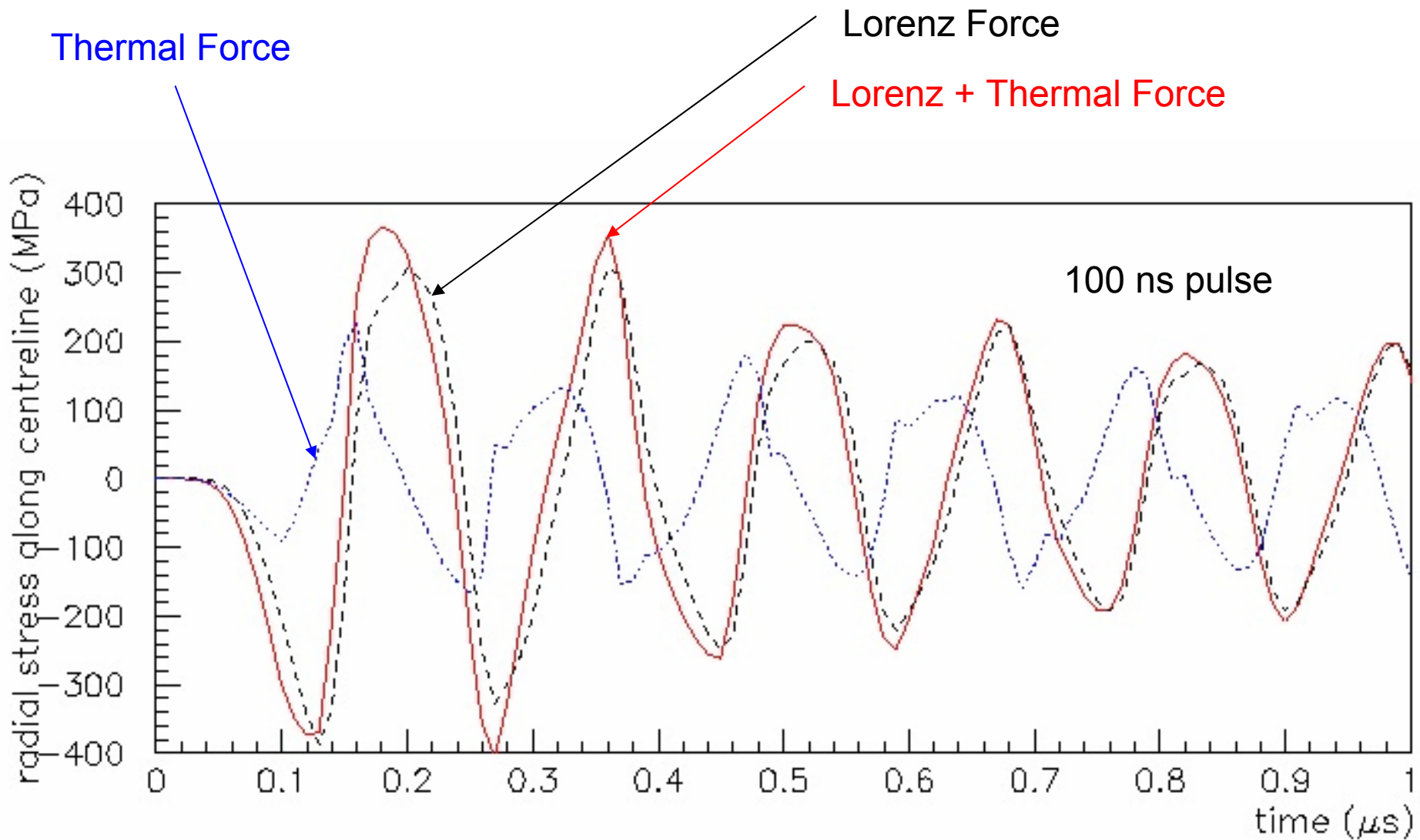
The Pbar target at FNAL withstands 40,000 J
cm⁻³!

-

The NF target has only 300 J cm⁻³

□ It is not possible to test the full size targets in a proton beam and do a life test.

□ Produce shock by passing high current pulses through thin wires.



Typical radial stress in the wire from thermal and Lorentz forces

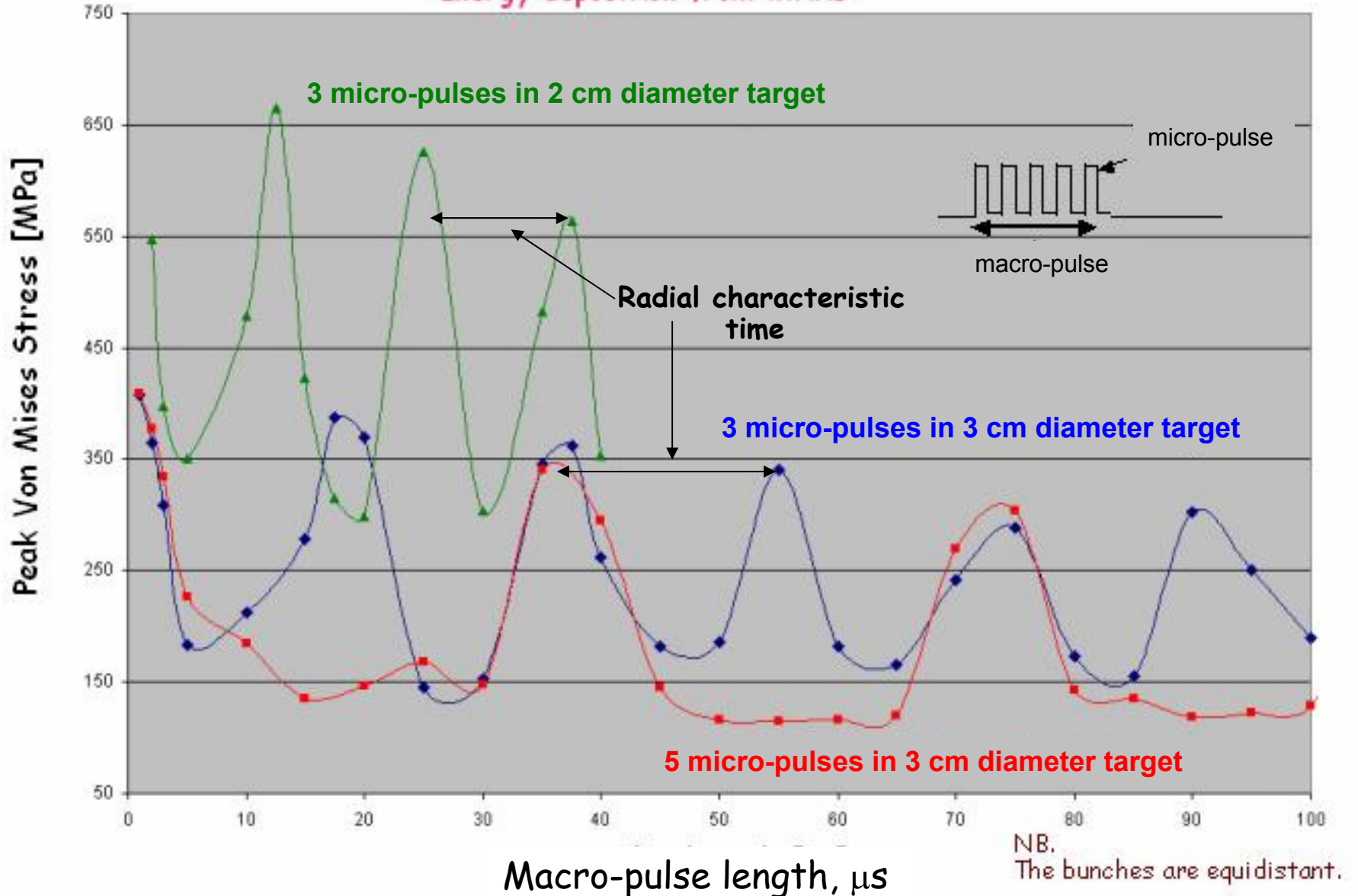
Results

LS-DYNA

Power = 4 MW, repetition rate = 50 Hz,
Beam energy = 6 GeV (parabolic distribution)
2 ns long bunches

TUNGSTEN target
operating at 2000 K
Beam radius = Rod radius

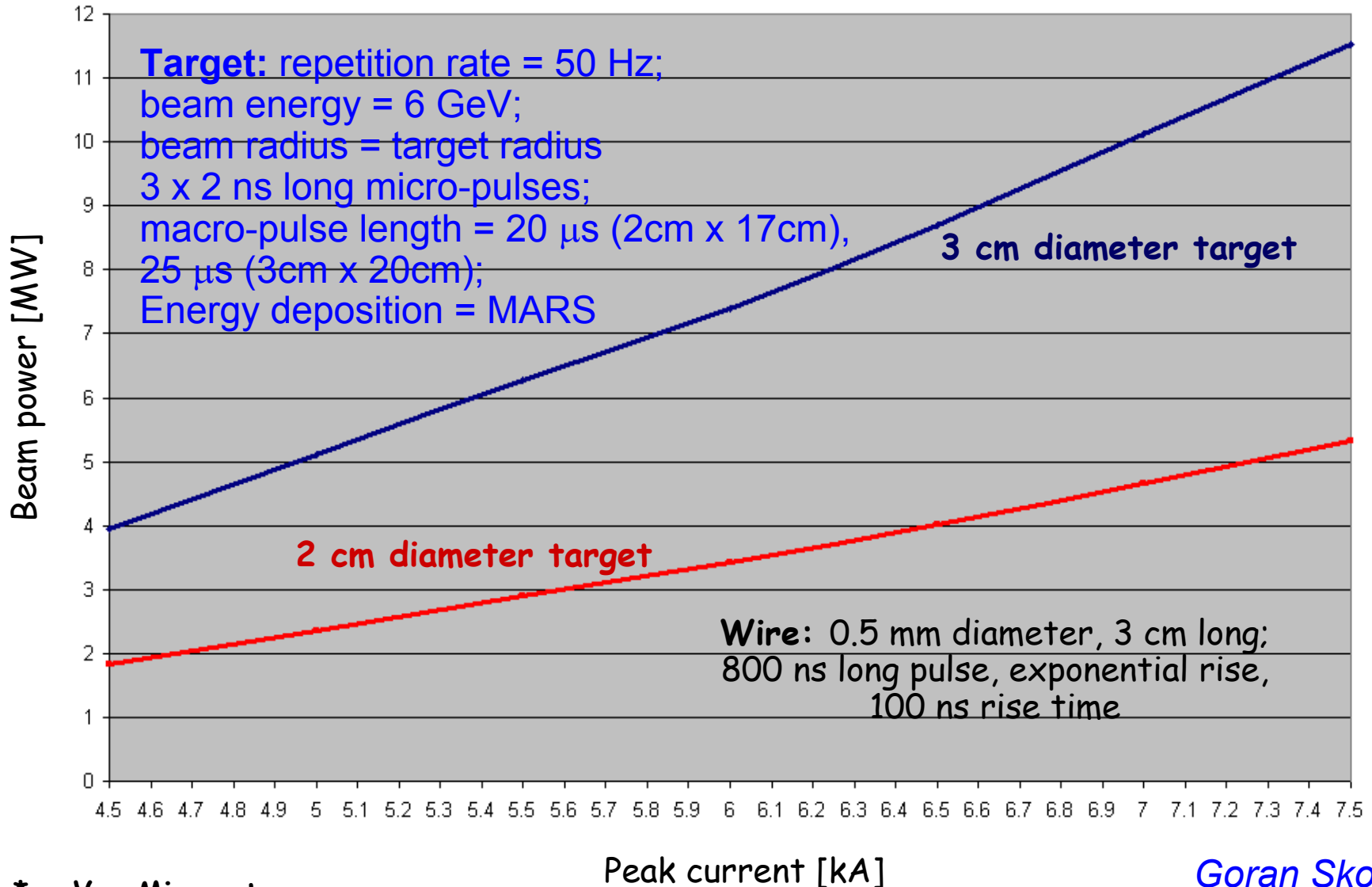
Energy deposition from MARS



Isostress* lines for tungsten target and wire (operating at 2000 K)

Results

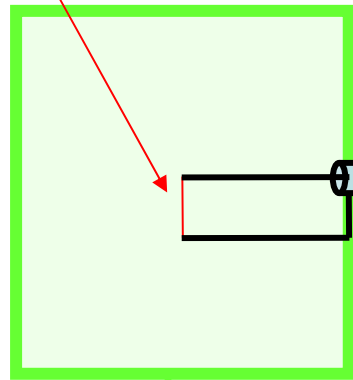
LS-DYNA



* - Von Mises stress

Goran Skoro

Test wire,
0.5 mm Φ



Coaxial wires



Pulsed Power Supply.

0-60 kV; 0-10000 A

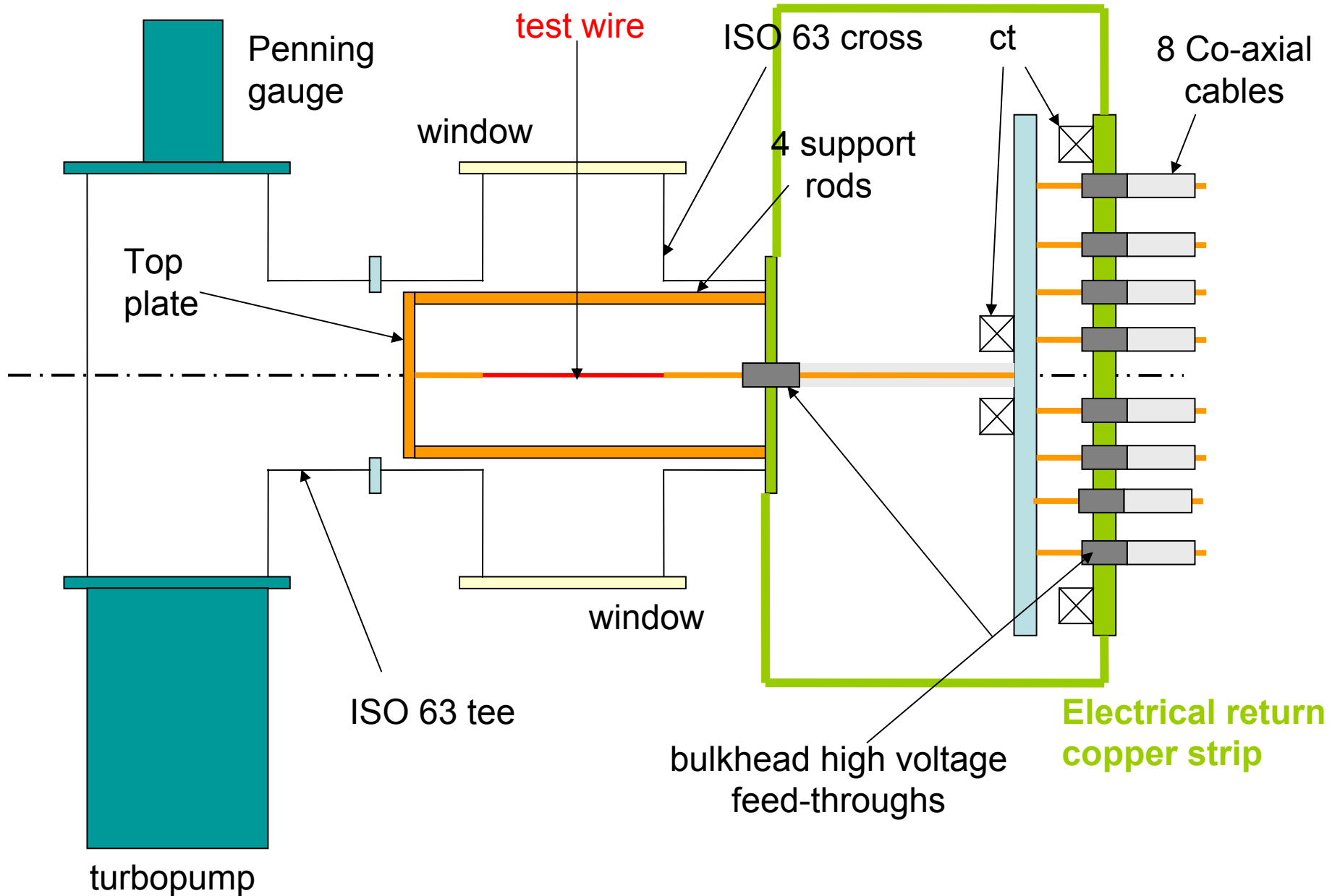
100 ns rise and fall time

800 ns flat top

Repetition rate 50 Hz or
sub-multiples of 2

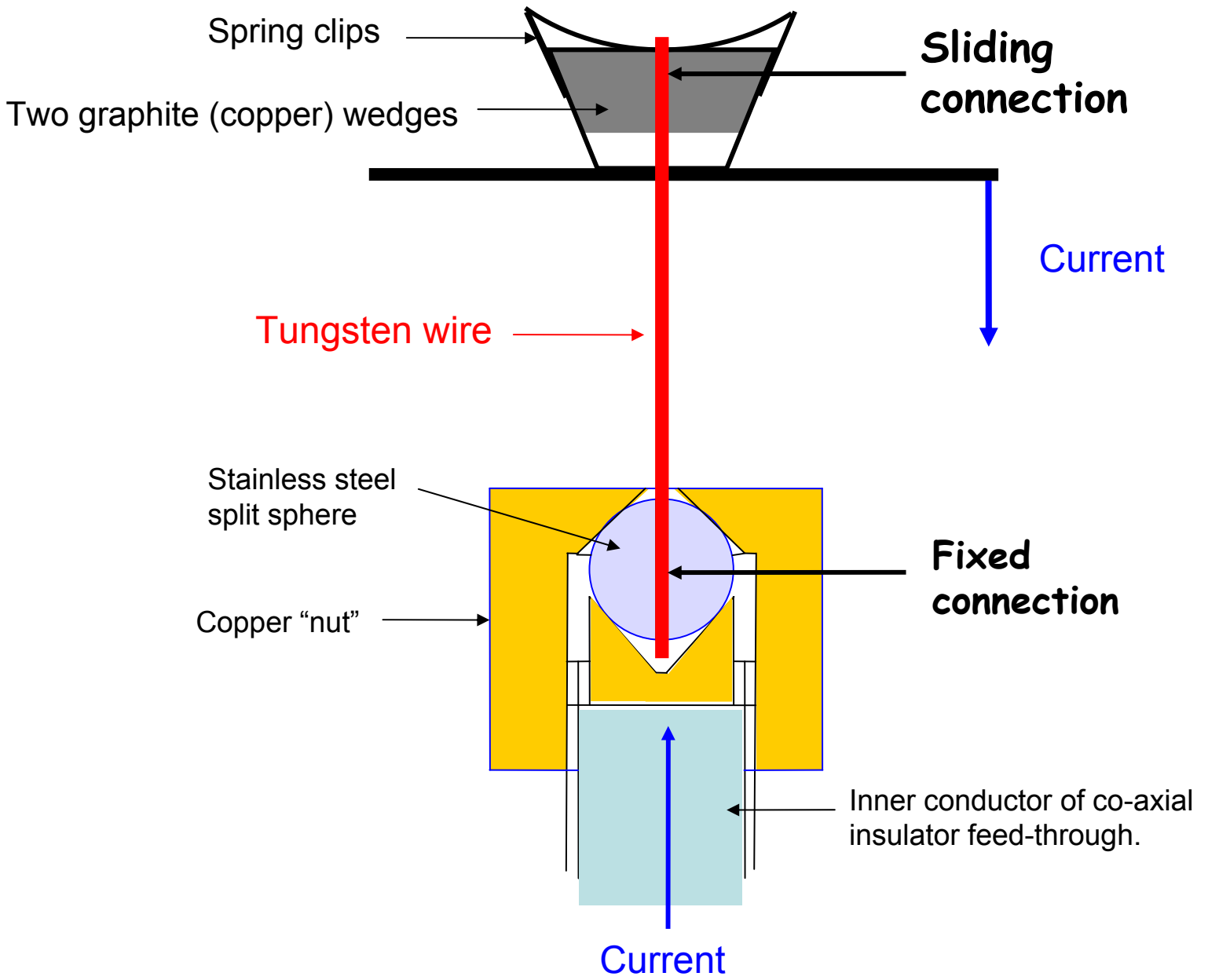
Vacuum chamber,
 2×10^{-7} - 1×10^{-6} mbar

Schematic circuit diagram of the wire test equipment



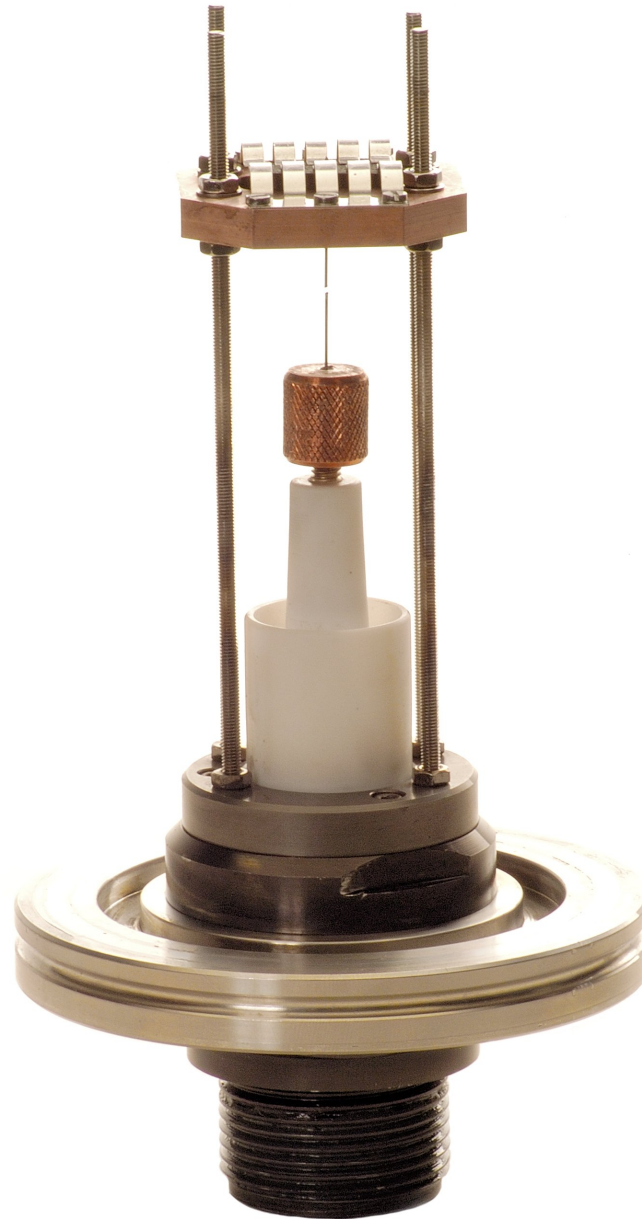
Schematic section of the wire test assembly

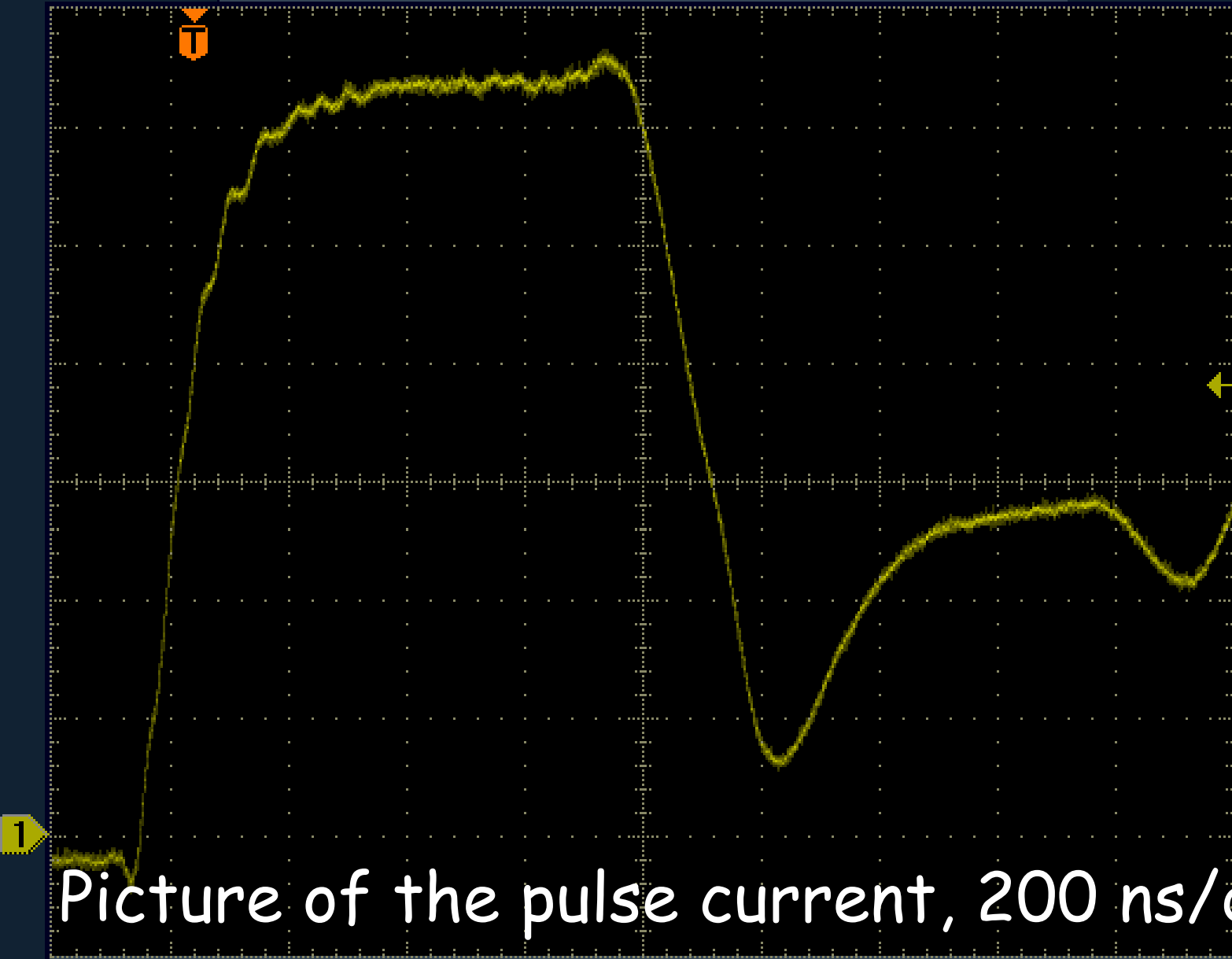
Vertical Section through the Wire Test Apparatus



W26

Tungsten
Wire
Assembly

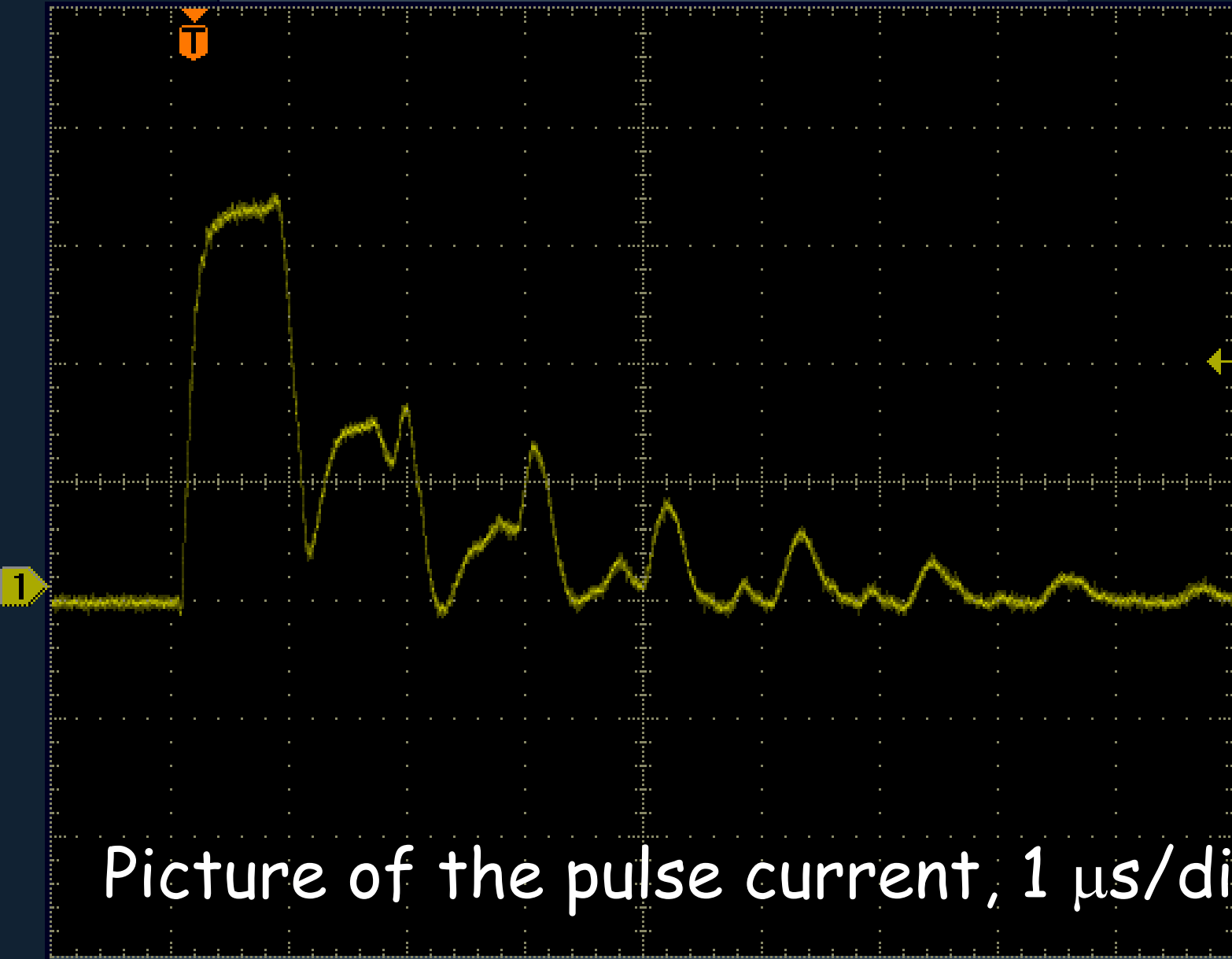




Picture of the pulse current, 200 ns/division

Ch1 1.00 V BW M 200ns A Ch1 3.80 V

12.00 %

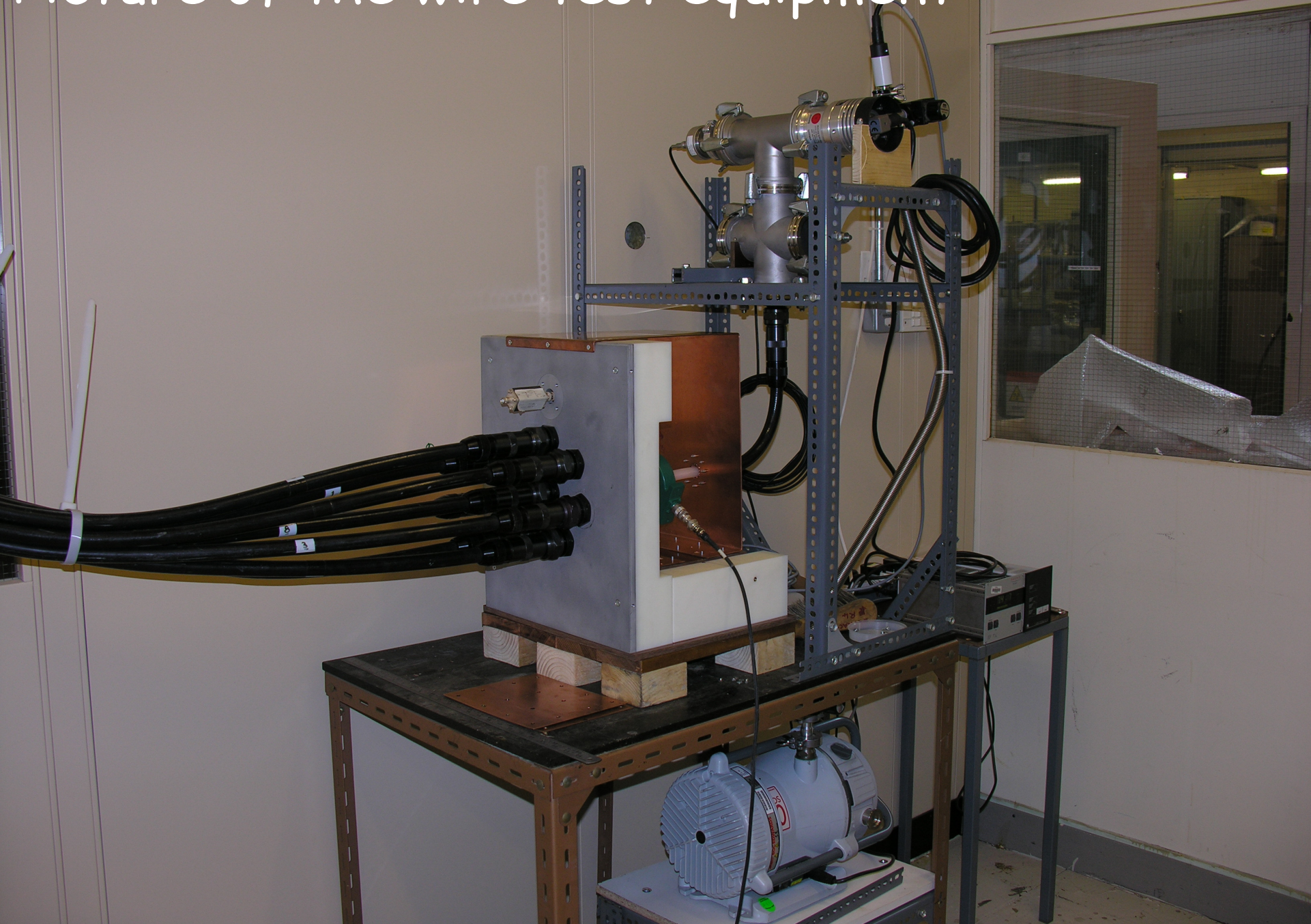


Picture of the pulse current, 1 μ s/division

Ch1 2.00 V B_W M 1.00 μ s A Ch1 3.80 V

12.00 %

Picture of the wire test equipment



135.00

(DEG.C)

1700

1650

1600

1550

1500

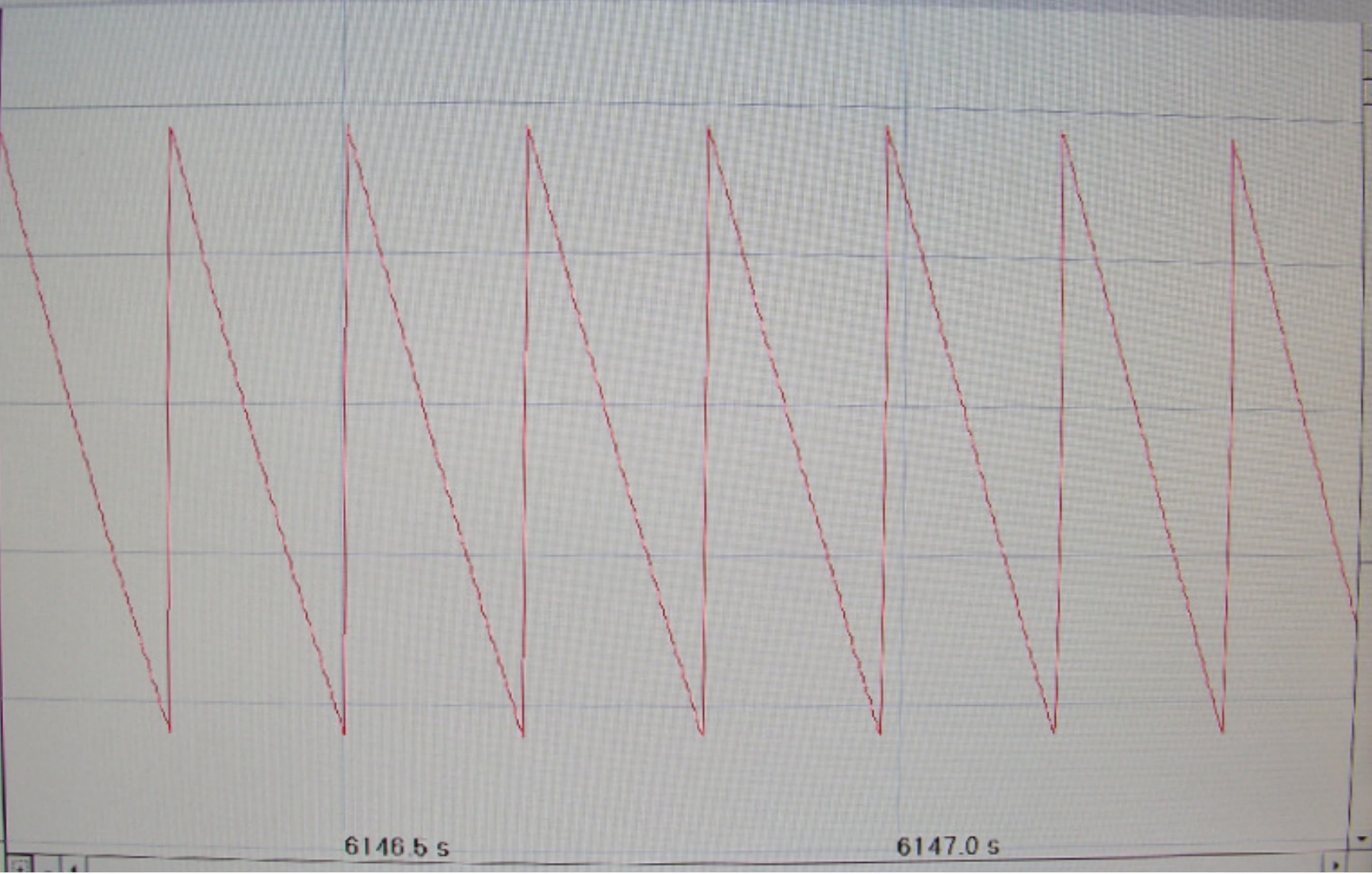
1450

6146.5 s

6147.0 s

Measurement of the Pulse Temperature

1 kHz measurement rate

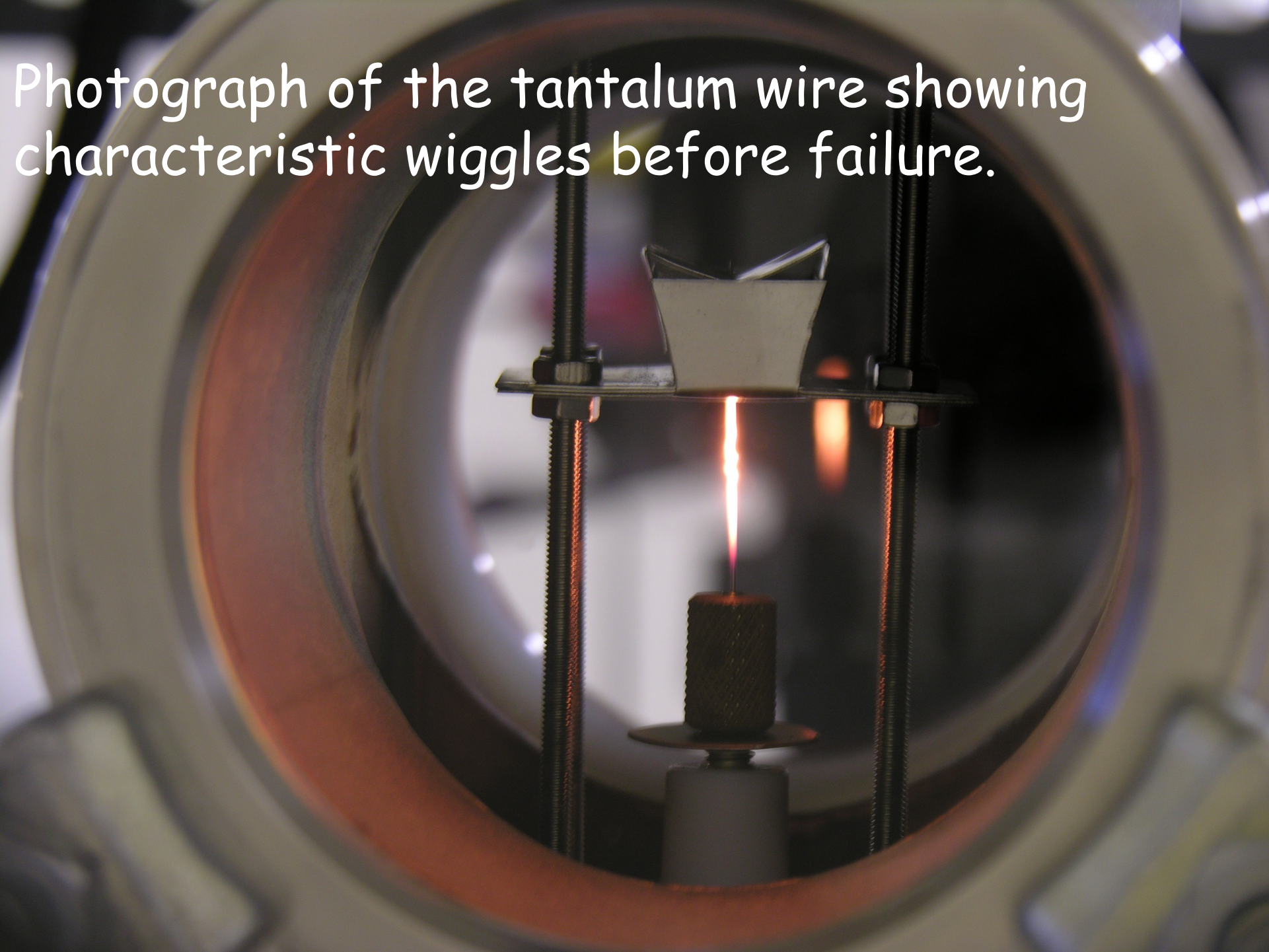


Tests on Tantalum Wire

The wire lasted for a few hundred thousand pulses before breaking or bending.

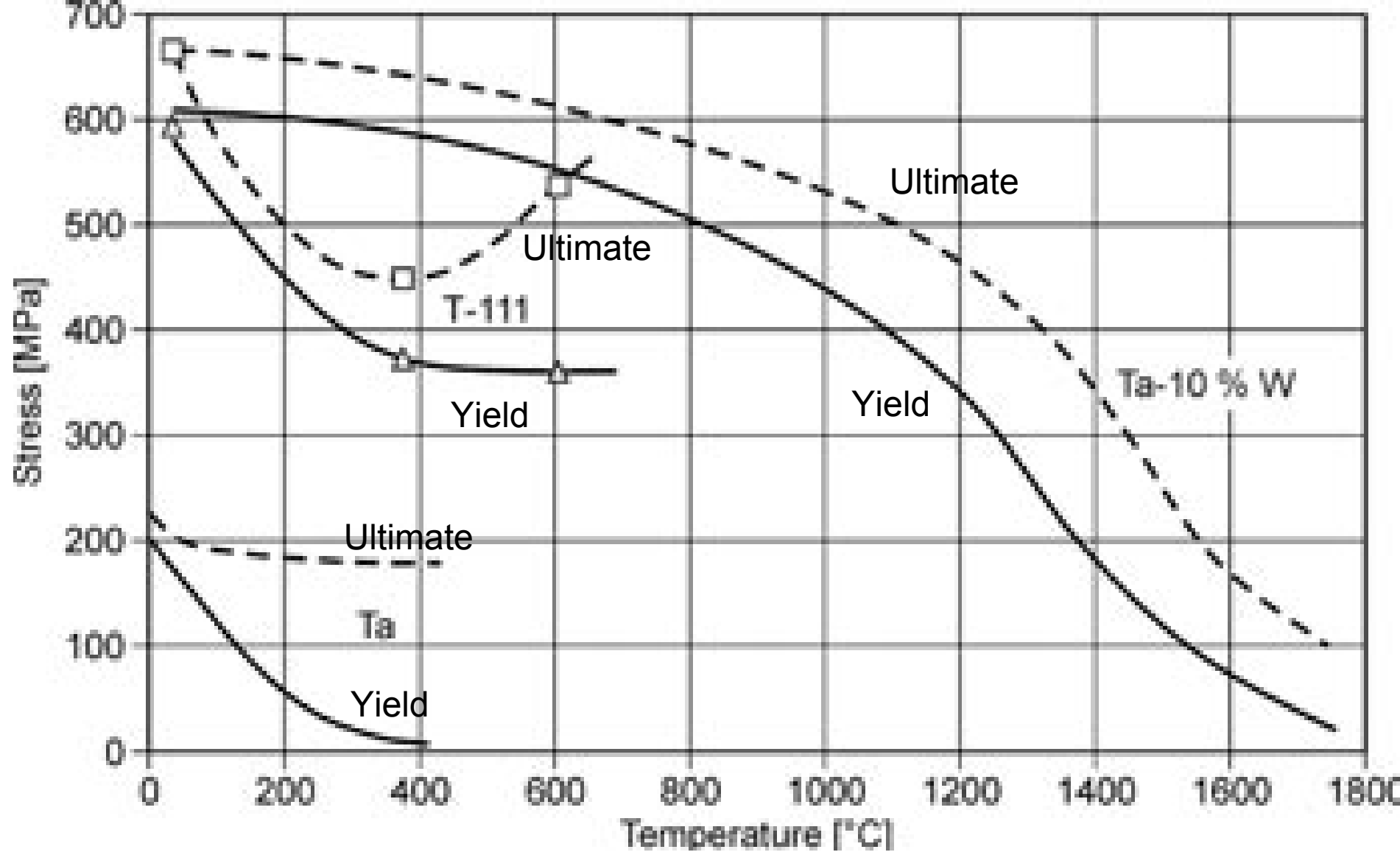
Tantalum is not a suitable material since it too weak at high temperatures (1600-2000 K).

Photograph of the tantalum wire showing characteristic wiggles before failure.

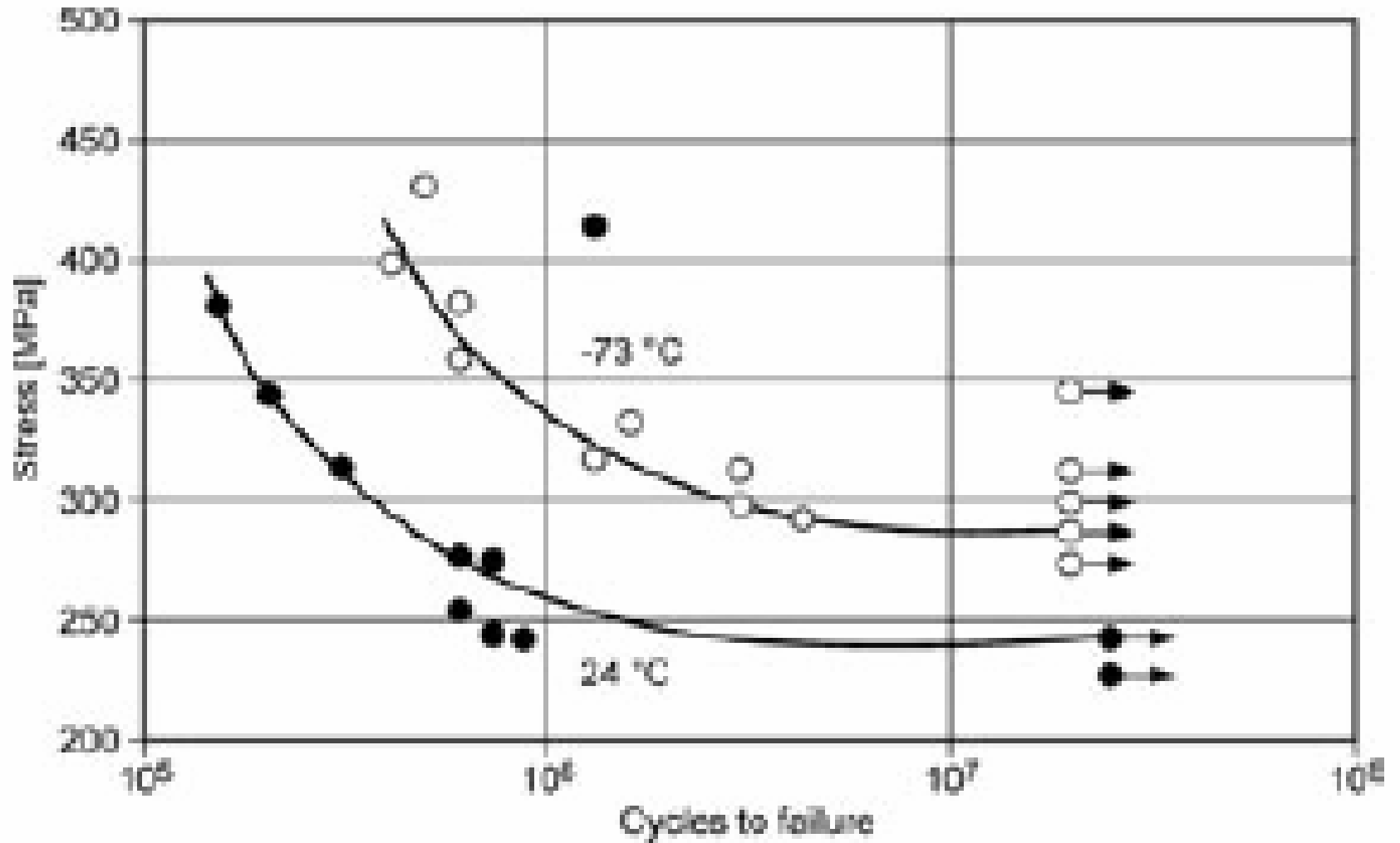


A close-up photograph of a mechanical testing apparatus. A thin, dark wire is suspended vertically from a metal plate at the top. The wire is broken in the middle, with a jagged, wavy fracture surface. The lower end of the wire is attached to a cylindrical component with a diamond-patterned mesh texture. This component is resting on a flat, circular metal base. The entire setup is supported by a frame of vertical threaded rods and horizontal plates. The background is a plain, light-colored surface.

A broken tantalum wire

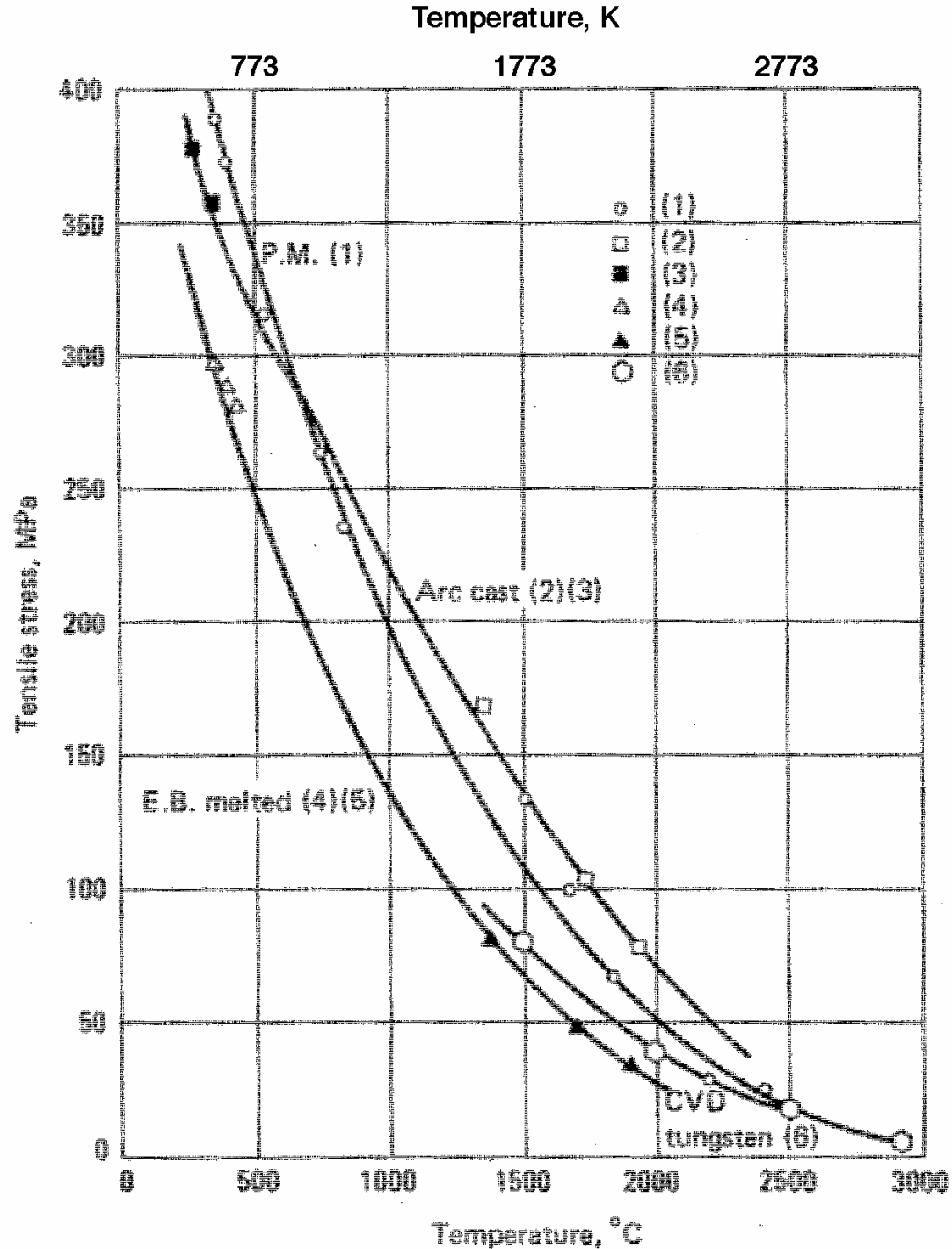


Yield and Ultimate Strength of Tantalum and alloys versus Temperature.

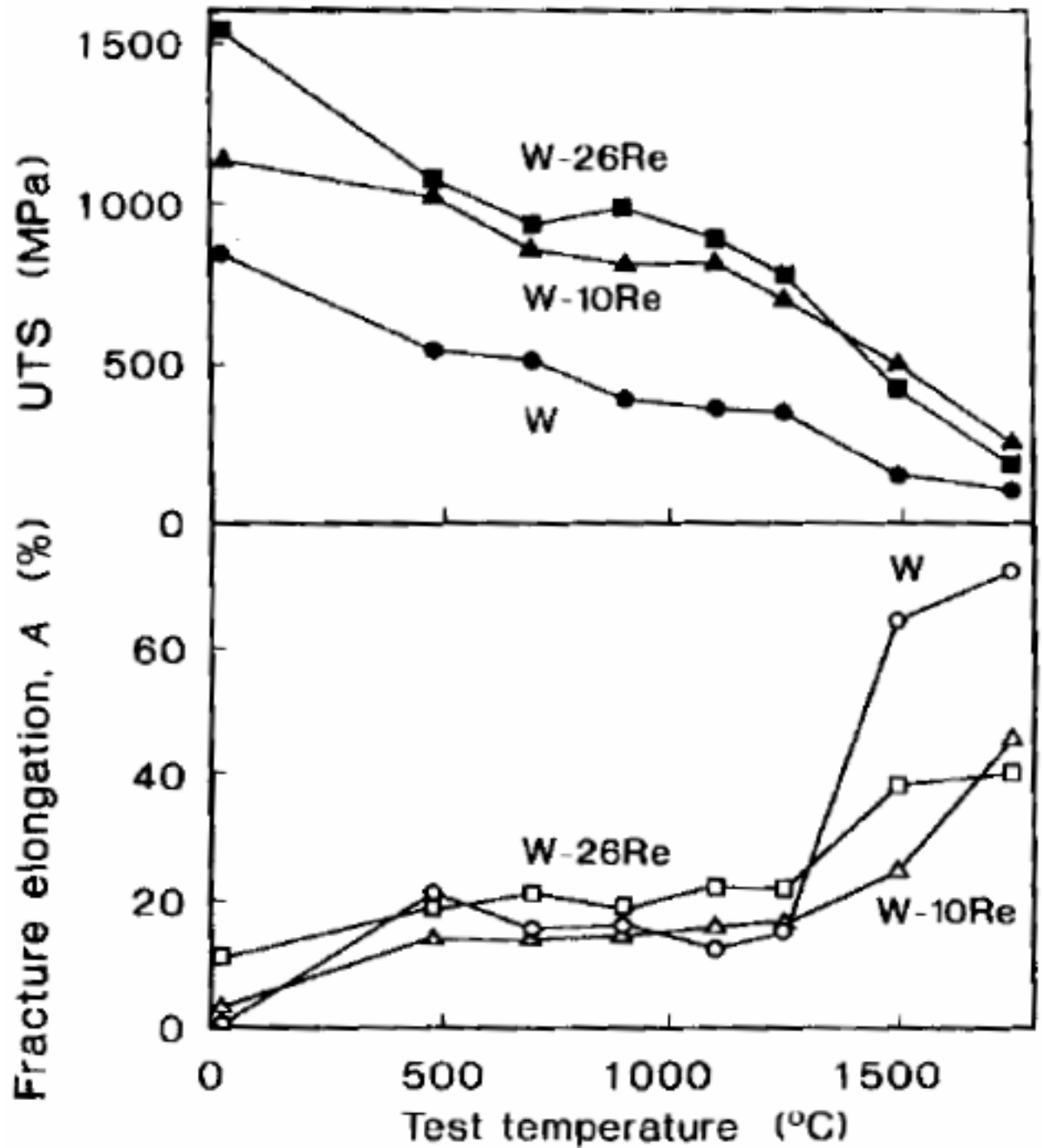


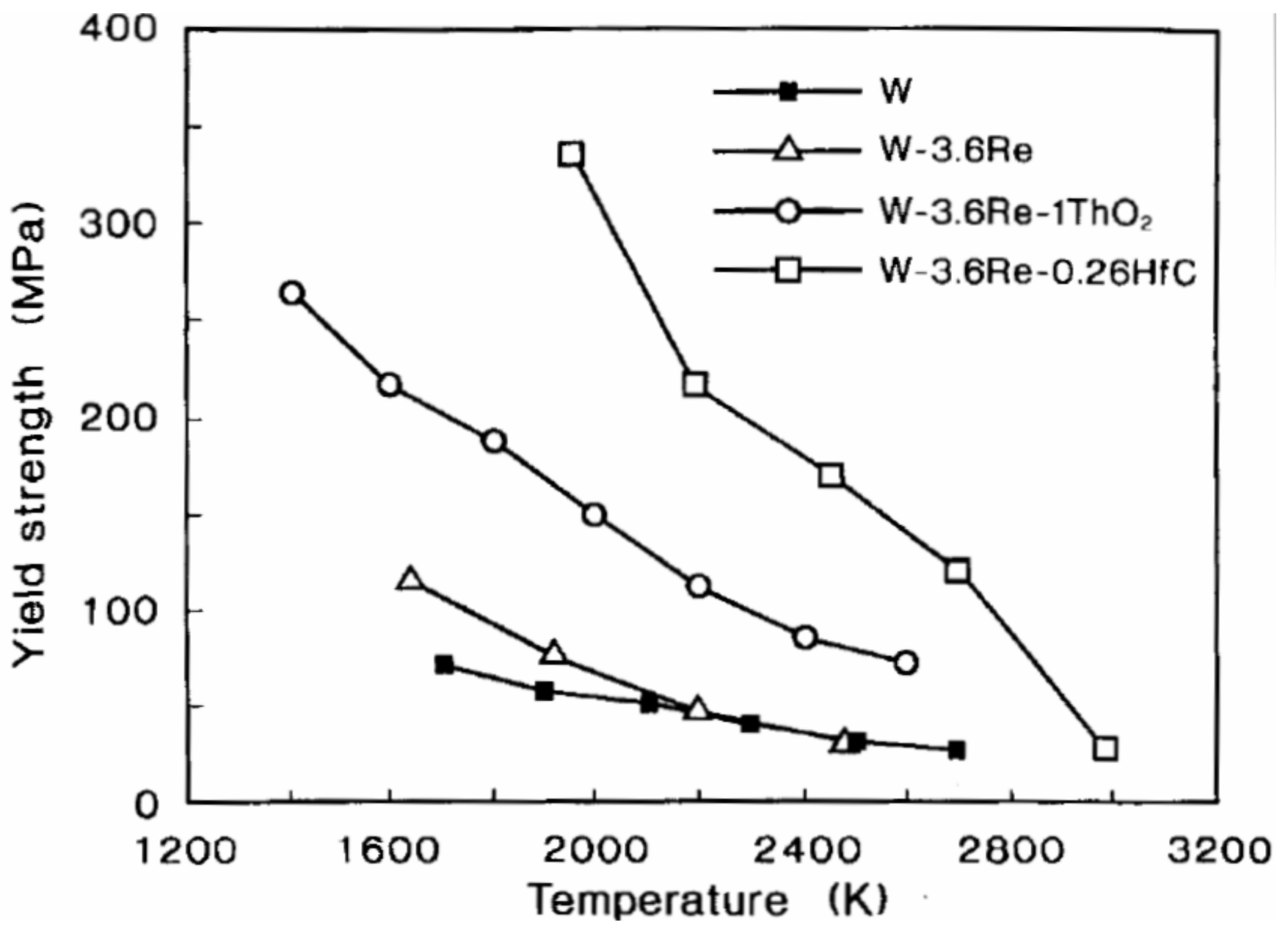
Fatigue characteristics of 1 mm thick tantalum sheet

Ultimate Tensile Strength of Tungsten Rods produced by various methods

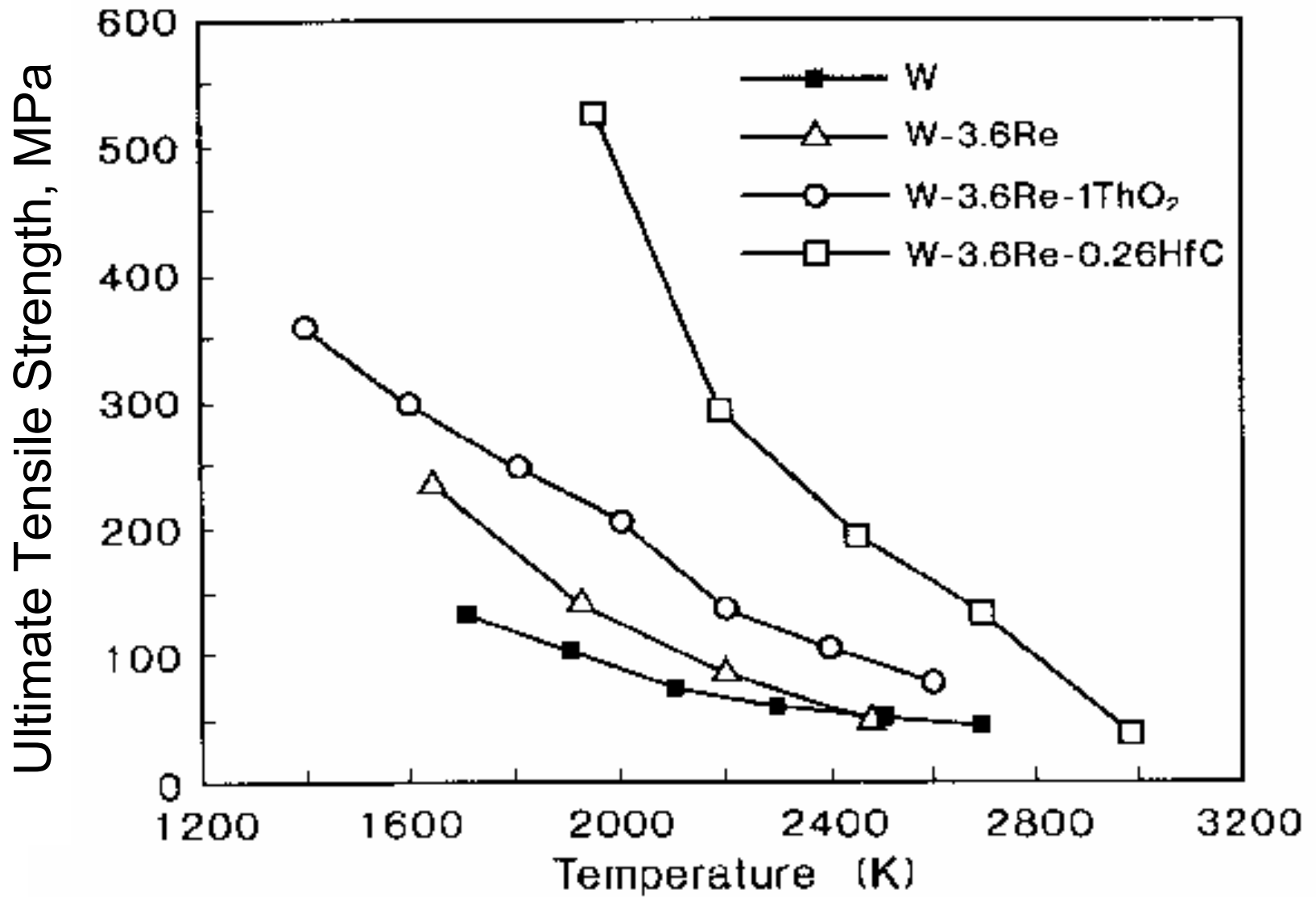


Ultimate
Tensile
Strength
versus
Temperature
of Tungsten
and some
Alloys





Yield Strength of Tungsten and some Alloys versus Temperature



Ultimate Tensile Strength of Tungsten and some Alloys versus Temperature

Tests on Tungsten Wire

Tungsten is much stronger than Tantalum particularly at high temperatures.

So - try Tungsten

Some Results: 0.5 mm diameter Tungsten Wires

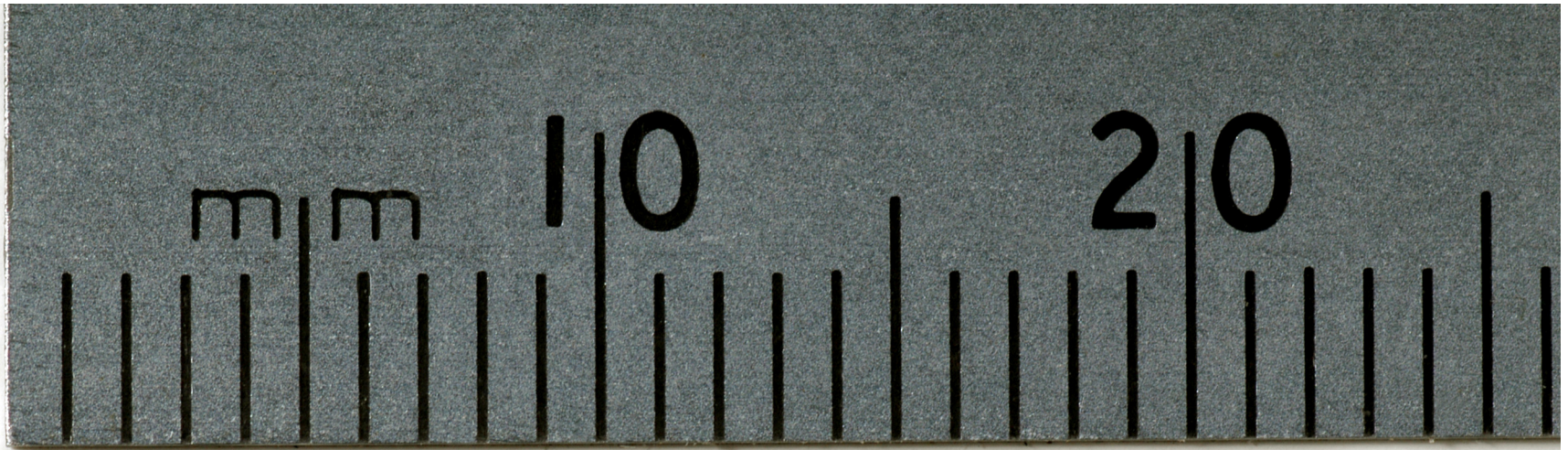
Target Number	Pulse Current A	Temp Jump K	Peak Temp K	Number of Pulses to Failure	Comments	Equivalent Power, MW, in Target Diameter	
						2 cm	3 cm
W03	4900 7200	90 200	2000 2200	$>3.4 \times 10^6$ 16,500	Broke	2.3	4.8
W08	6400	150	1900	$>1.6 \times 10^6$	Wire stuck to top connection (cu blocks)	3.9	8.4
W09	5560 5840	120 130	1900 2050	4.2×10^6 9×10^6	Top connector failed	3 3.3	6.4 7.0
W15	6400	180	1950	1.3×10^6	Wire stuck to top connection (cu blocks)	3.9	8.4
W26	6200 7520- 8000	140 ~230	2000 ~1800	10×10^6 3×10^6	Broke	3.6 ~6	7.8 ~12
W28	6560	180	1900	$>19 \times 10^6$	Still running	4.1	8.8

"Equivalent Target": This shows the equivalent beam power (MW) and target radius (cm) in a real target for the same stress in the test wire. Assumes a parabolic beam distribution and 3 micro-pulses per macro-pulse of 20 micro-s.

W26

Broken Tungsten Wire
after 13 million pulses.





W3 Tungsten Wire, after operating at 4900 A, peak temperature 1800 K, for 3.3×10^6 pulses and then a few pulses at 7200 A at >2000 K.



W5 Tungsten Wire showing "wiggles": 6200 A,
>2000 K peak temperature, 5625 pulses.

Individual pulses are not the problem.

Failure found after **Many Pulses** - the problem is:-

Fatigue

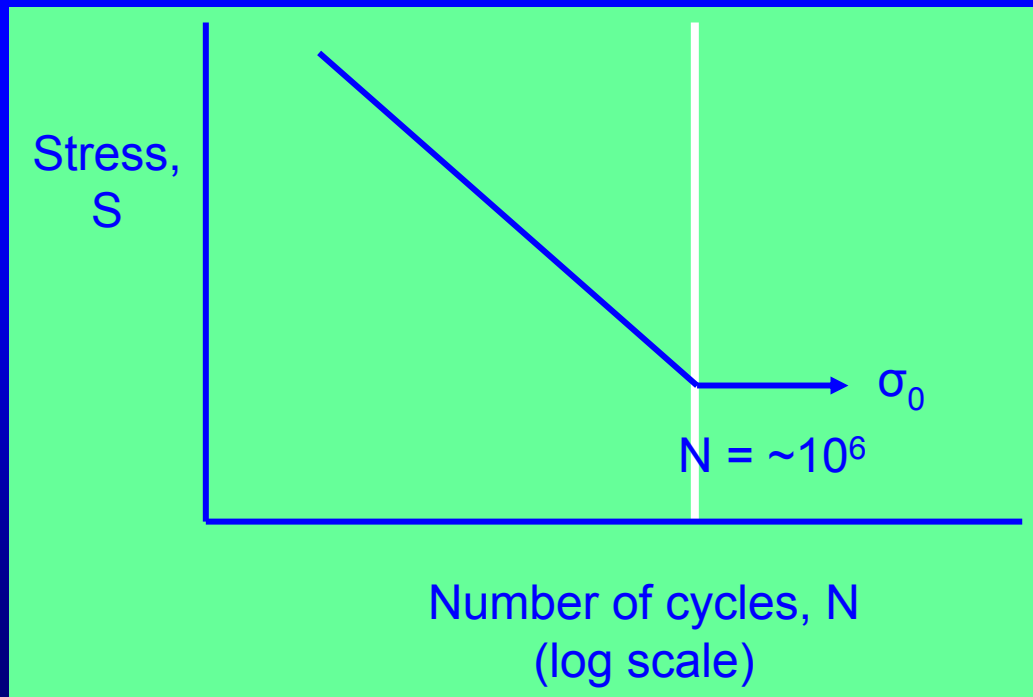
&

Creep

Fatigue and Creep

Very difficult to predict the number of cycles to failure.

S-N or Wöhler Plot - stress versus number of cycles to failure.



The Fatigue Limit Stress
can be expressed by:

$$\sigma_0 = 1.6 H_v \pm 0.1 H_v$$

H_v - Vickers Hardness in kgf mm^{-2}

For tungsten at $\sim 1800 \text{ K}$

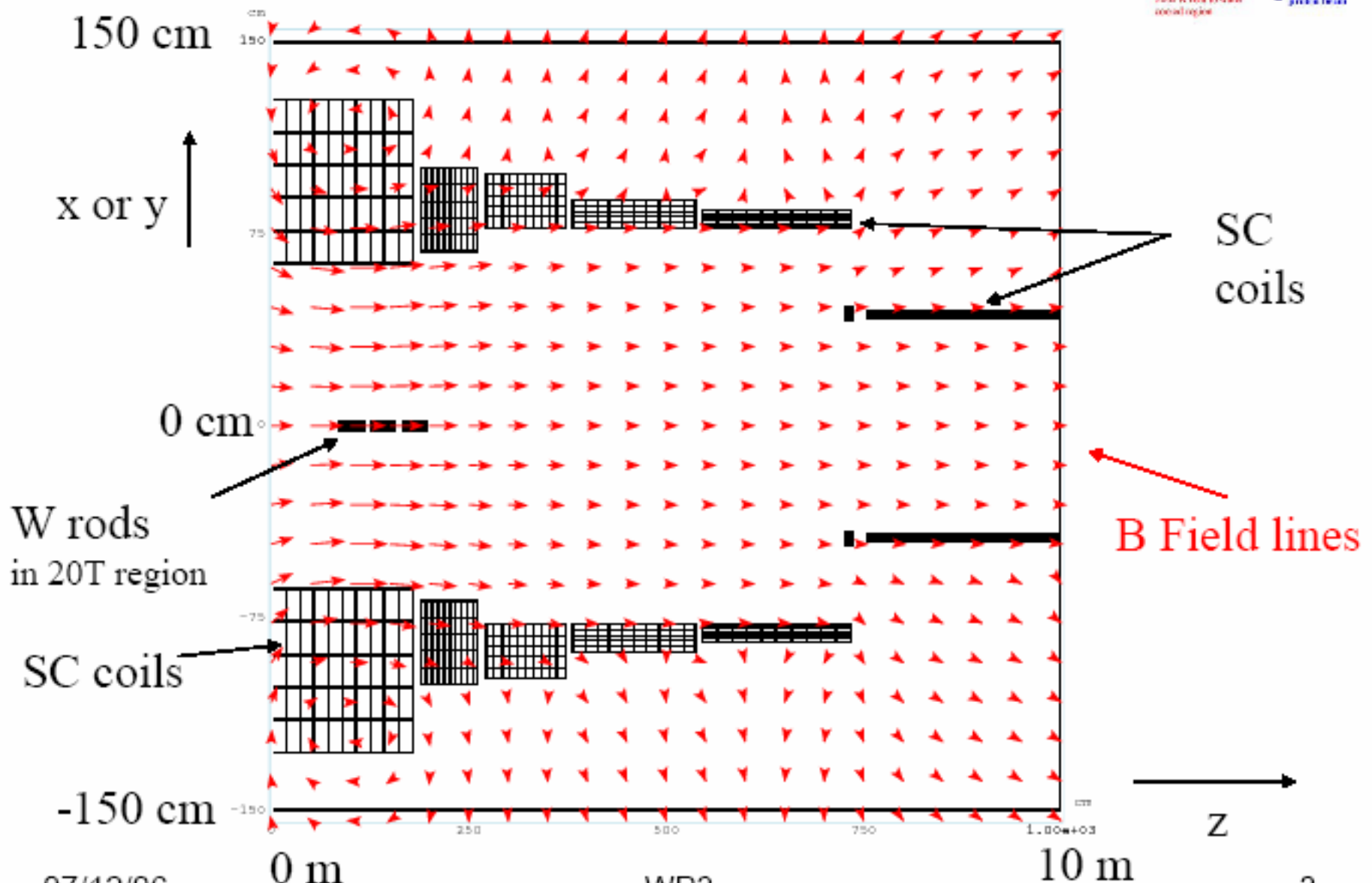
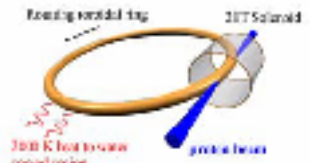
$$H_v = 50$$

so the fatigue limit stress is

$$\sigma_0 = 80 \text{ MPa}$$

Radiation Damage

1. Experience on the ISIS targets show that there is no serious problem up to ~12 dpa.
2. Tungsten pellets irradiated (~15-20 dpa) at PSI will be examined when cool enough.



π and μ re-absorption ratios for W target

	Number of π & μ per proton per GeV at plane 2 (+ve charge, -ve charge)			Number of π & μ per proton per GeV at plane 3 (+ve charge, -ve charge)		
Rod diameter	1 cm	2 cm	3 cm	1 cm	2 cm	3 cm
1 rod	0.460 0.482	1.012 1.035	0.906 0.917	0.460 0.481	1.014 1.035	0.909 0.915
3 rods	0.401 0.402	0.806 0.801	0.663 0.644	0.355 0.350	0.657 0.631	0.495 0.463
1 rod/3 rods	1.15 1.20	1.26 1.29	1.37 1.42	1.30 1.37	1.54 1.64	1.84 1.98

MARS Simulation: 10 GeV protons on 1, 2 and 3 cm diameter W rods in 20 T field.

Conclusions

I believe that the viability of solid tungsten targets at high-temperature for a long life (~10 years) has been demonstrated with respect to thermal shock and fatigue and will not suffer undue radiation damage.

Future Programme

1. Continue wire tests with Tungsten and Graphite.
2. VISAR measurements to assess the properties of tungsten, and any changes, during the wire tests. (Effect of thermal shock.)
3. Tests with a proton beam - limited number of pulses possible - to confirm wire tests and VISAR measurements.
4. Radiation damage studies.