

PLAN

MATERIAL STUDIES FOR PULSED HIGH-INTENSITY PROTON BEAM TARGETS

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CHALLENGES FOR THE INTEGRATED TARGET SYSTEMS AS WE GET TO 1+ MW SYSTEM

- Heat generation and removal from the target system
- Target thermo-mechanical response from energetic, high intensity protons
- Irradiation and corrosion effects on materials
- Beam window survivability

SOLUTION:

Look for new materials that are continuously being developed for other applications but seem to fit the bill as targets

There is a catch !

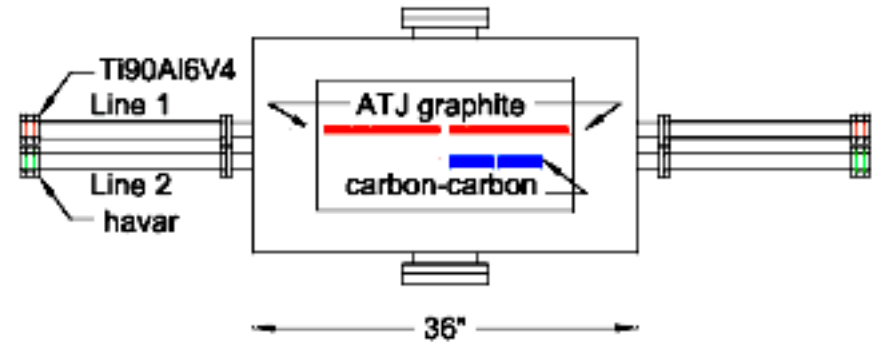
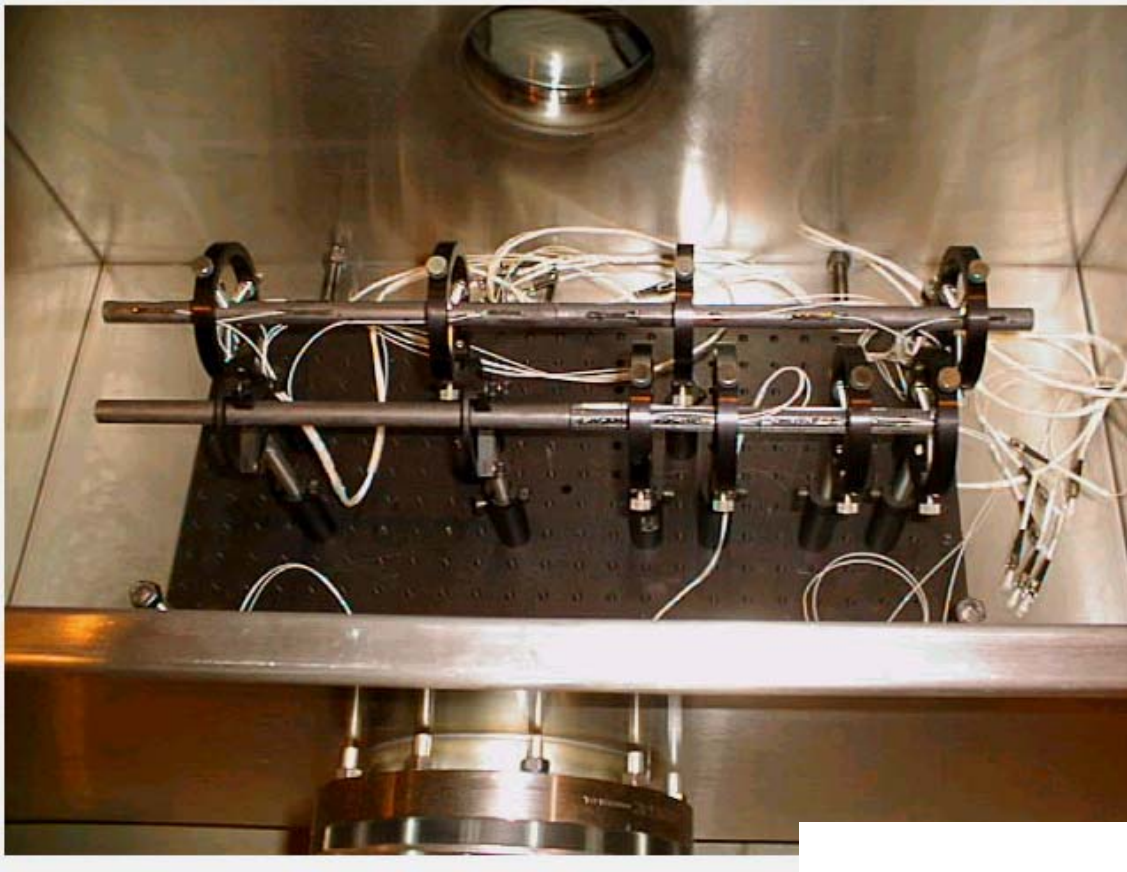
These materials have not been tested for their resilience to radiation exposure

The collaboration has been looking into these materials for some time

Candidate materials studied for applications as targets windows are:

- Inconel-718
- Aluminum-3000
- Havar
- Ti-6Al-6V
- Graphite (ATJ)
- Carbon-Carbon
- SuperInvar

PHASE I: Graphite & Carbon-Carbon Targets

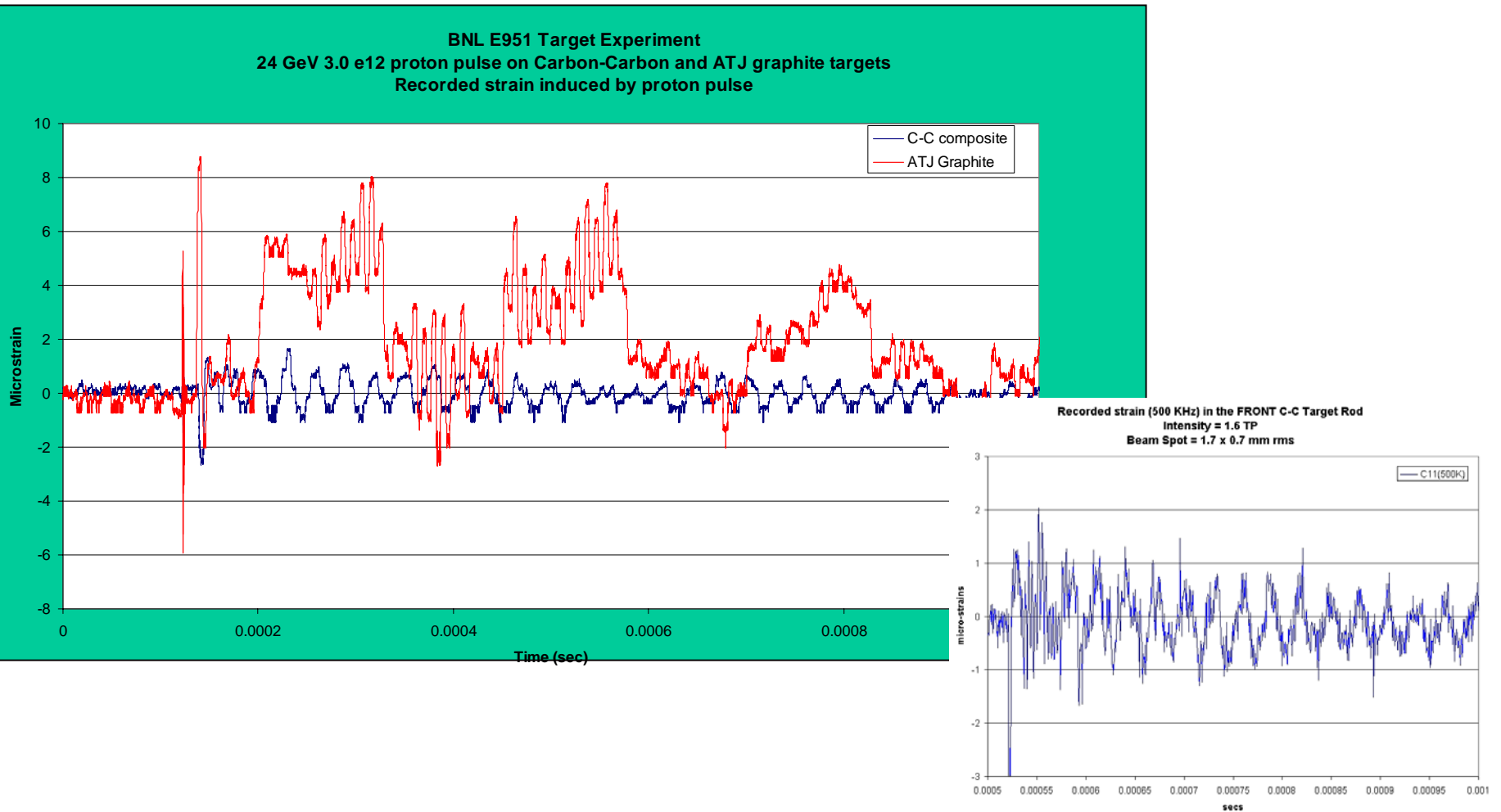


E951 Results: ATJ Graphite vs. Carbon-Carbon Composite

The results demonstrate the superiority of CC in responding to Beam SHOCK.

The question is: Will it maintain this key feature under irradiation ???

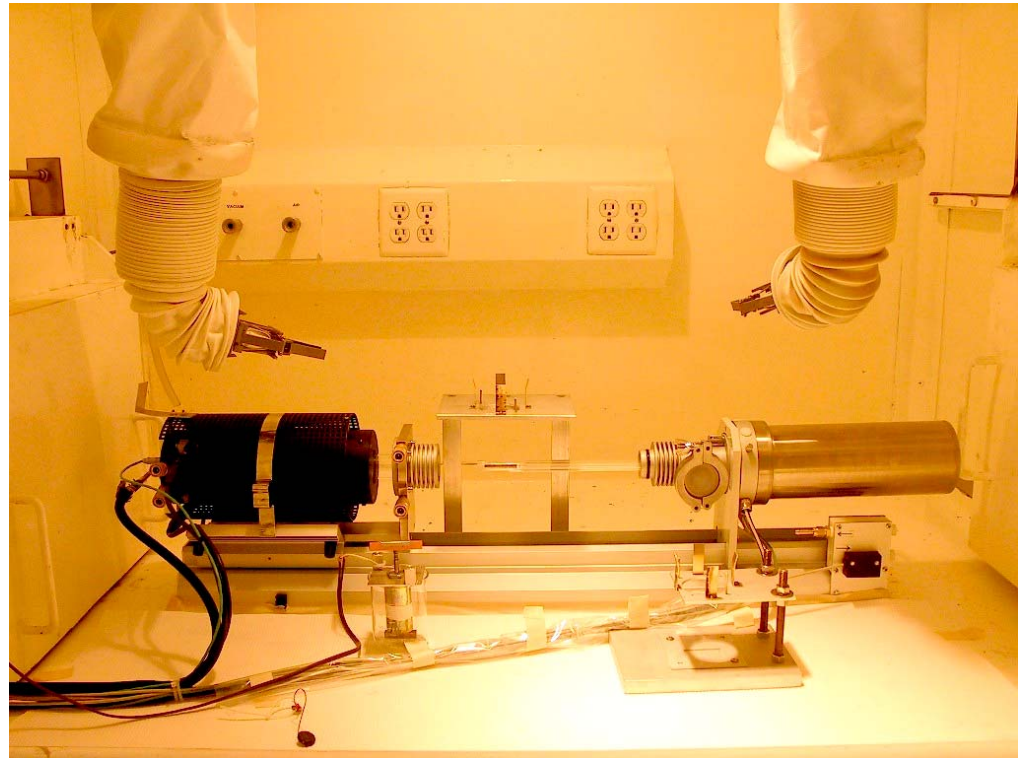
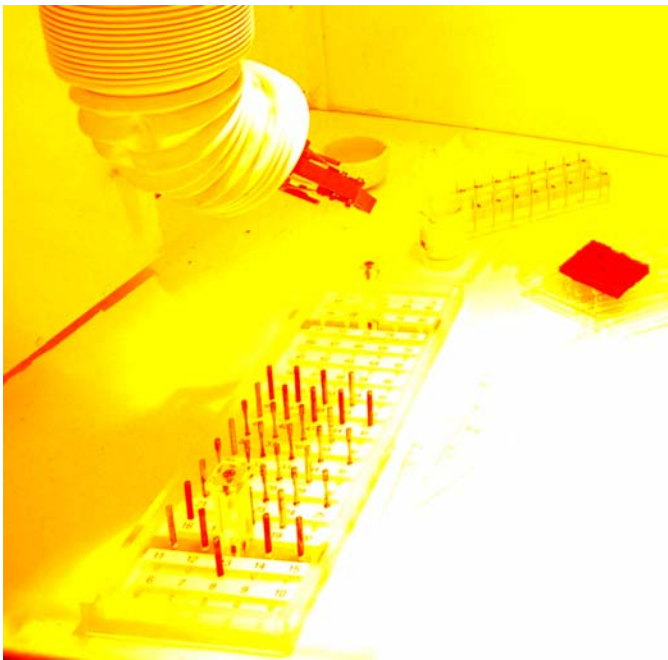
We will find out in the course of this irradiation phase



Irradiation Studies to Assess how Super-Invar responds to radiation.

Its key feature (low CTE up to 150 °C) needed to be scrutinized

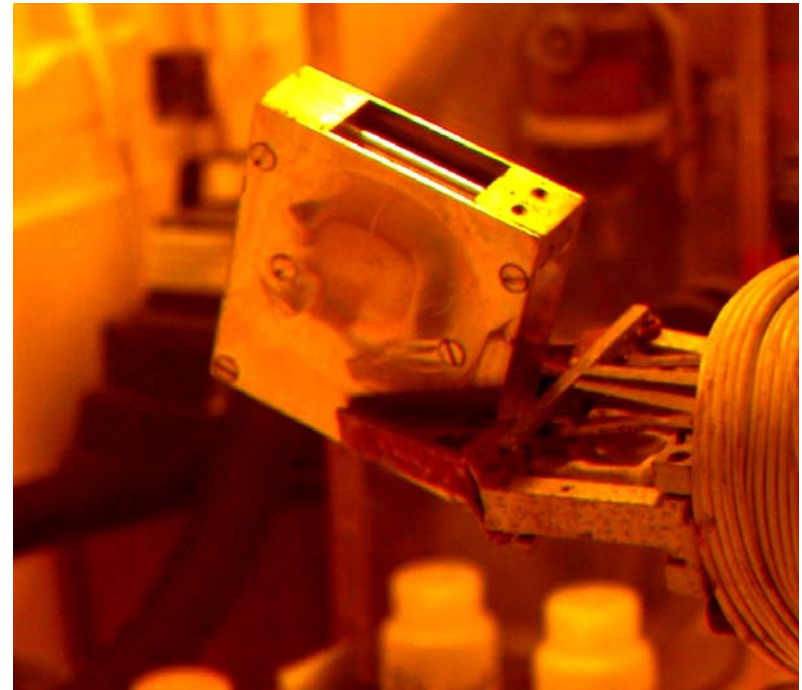
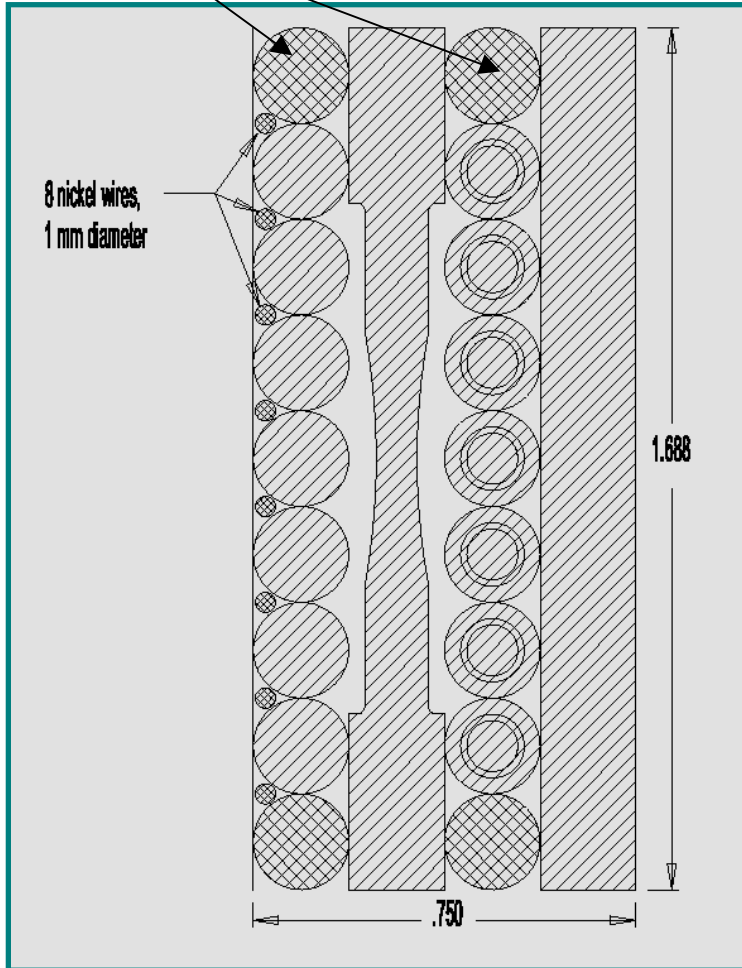
Specimens and dilatometer in hot cell

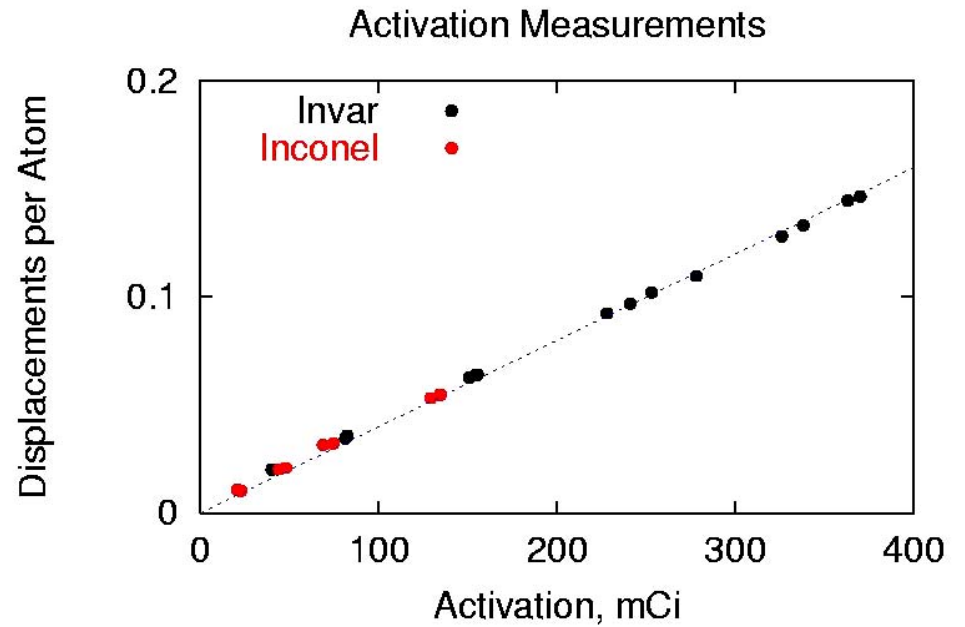
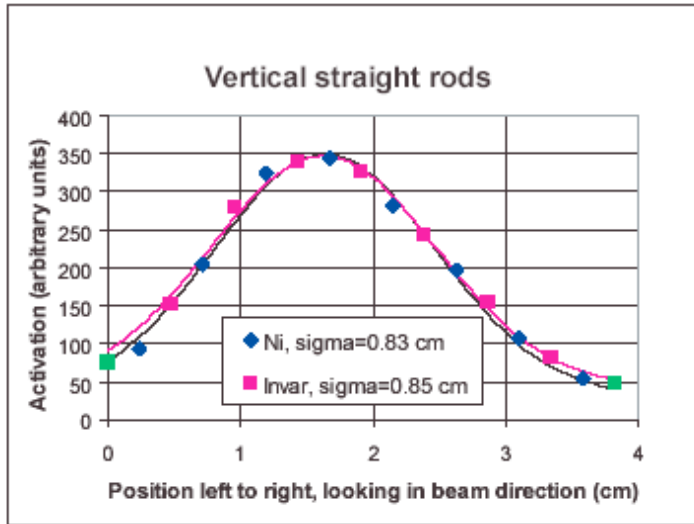


BNL Irradiation Studies

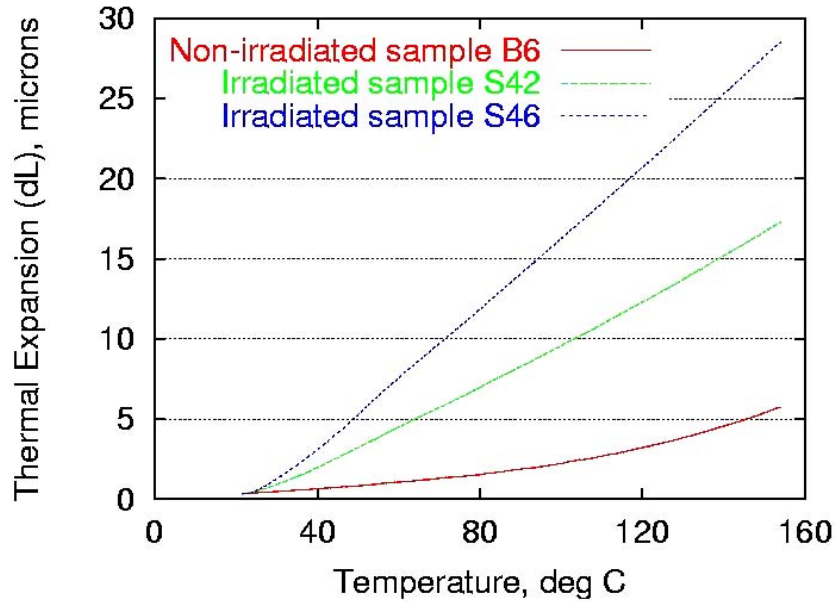
Super Invar & Inconel-718

Inconel-718 rods

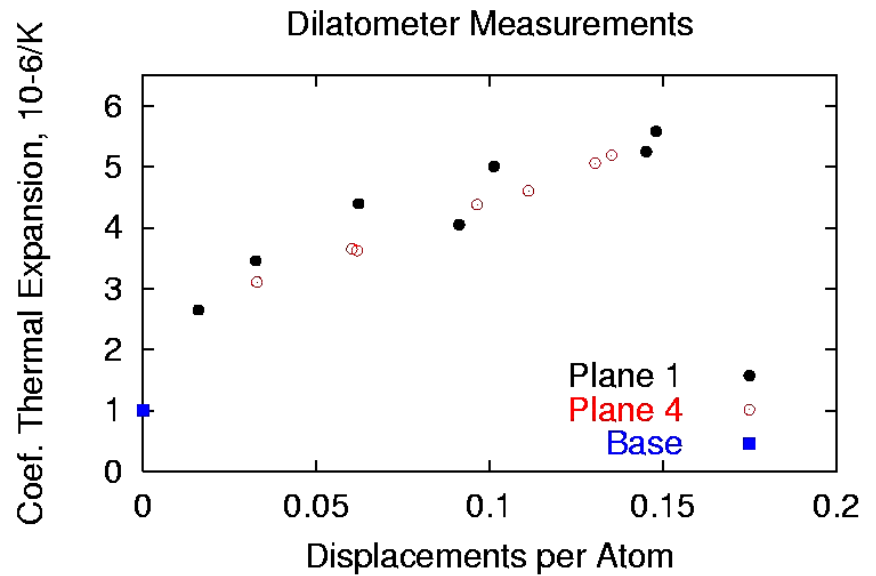




Super-Invar Irradiation Study – CTE assessment



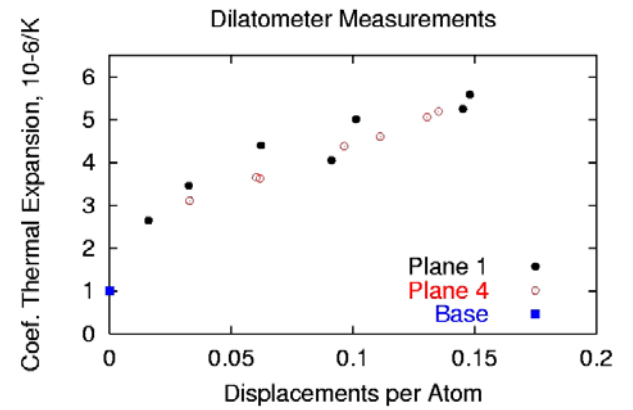
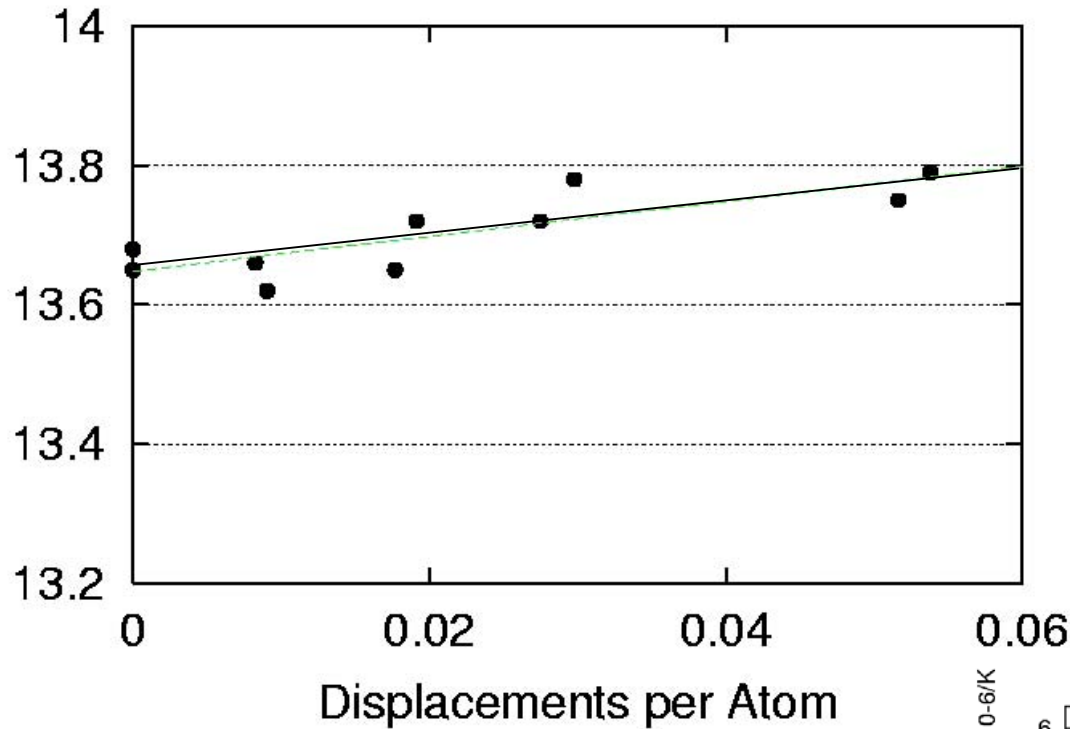
Super-Invar



Inconel-718 CTE assessment

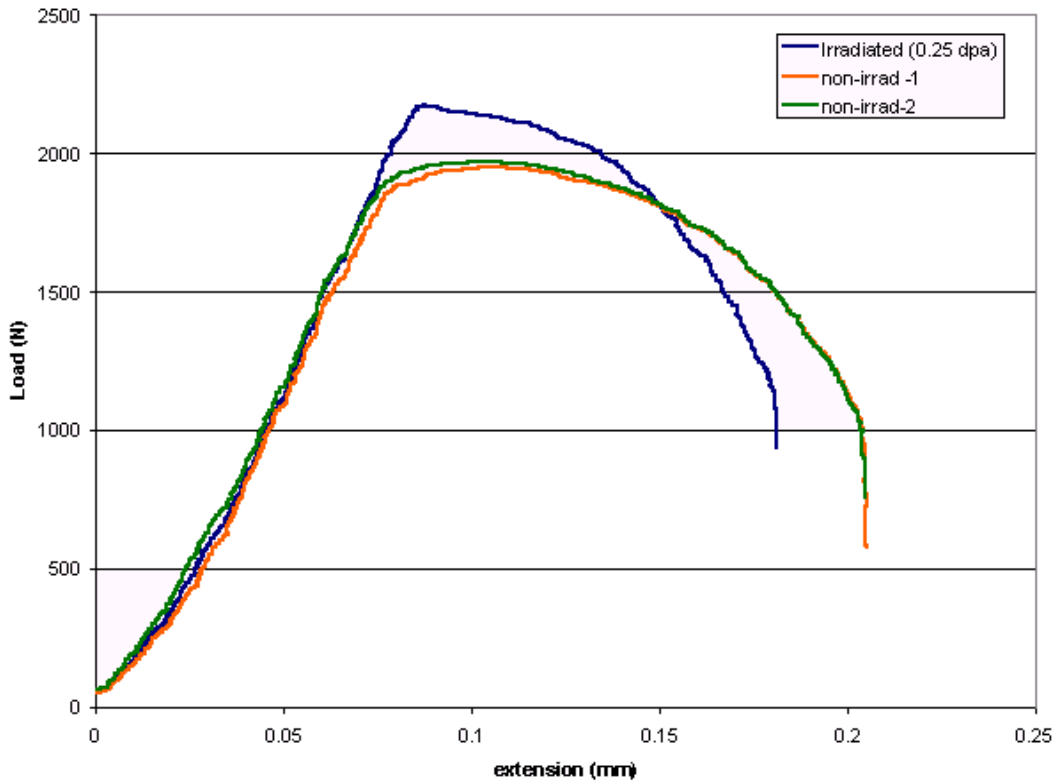
Coef. Thermal Expansion, 10⁻⁶/K

Inconel Dilatometer Measurements

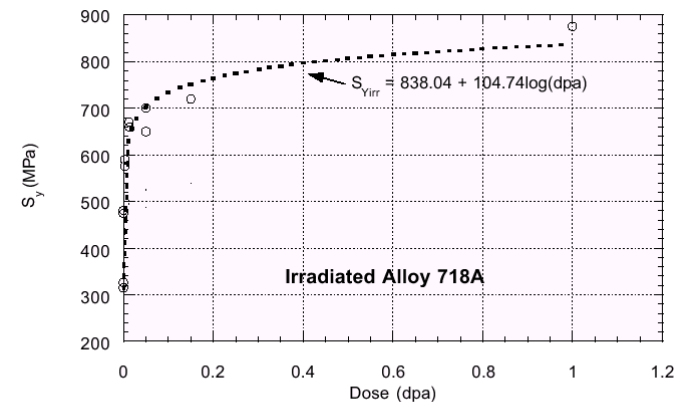


Super-Invar Irradiation Study - Effects of Irradiation on stress-strain behavior

Effects of Irradiation as Observed in the Load-Displacement Curve



While the dpa received were as high as .25, they were enough to capture the tendency of the material to change. Similar effects at such low dpa can be seen in Incinel (Figure below)

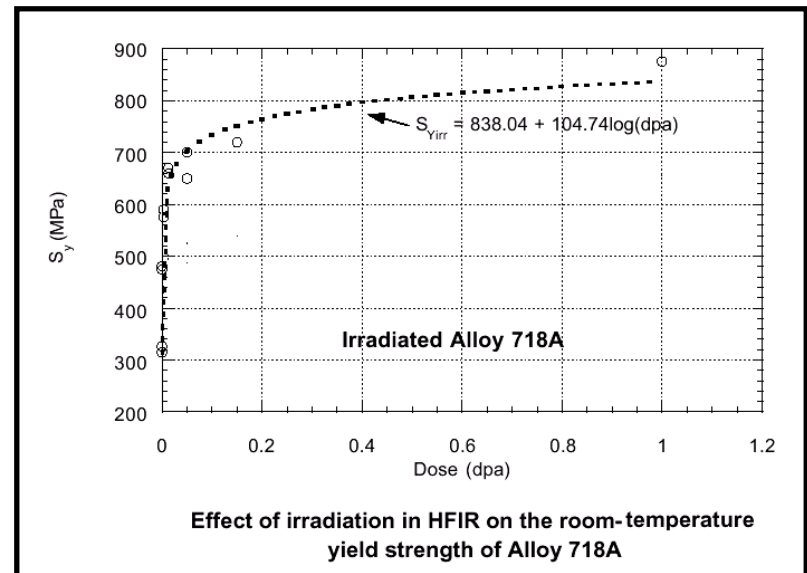
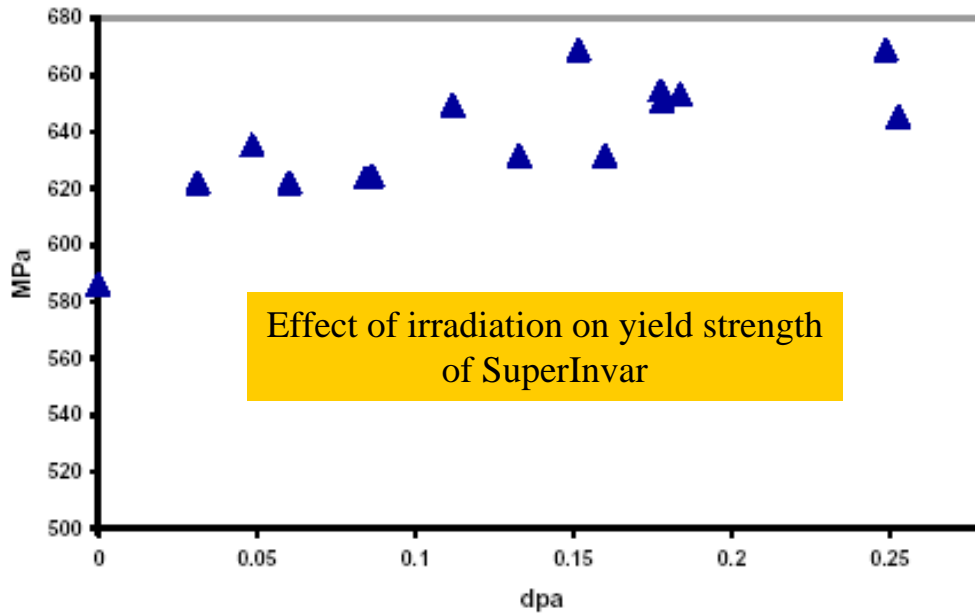


Effect of irradiation in HFIR on the room-temperature yield strength of Alloy 718A

WHY STUDY super Invar ?

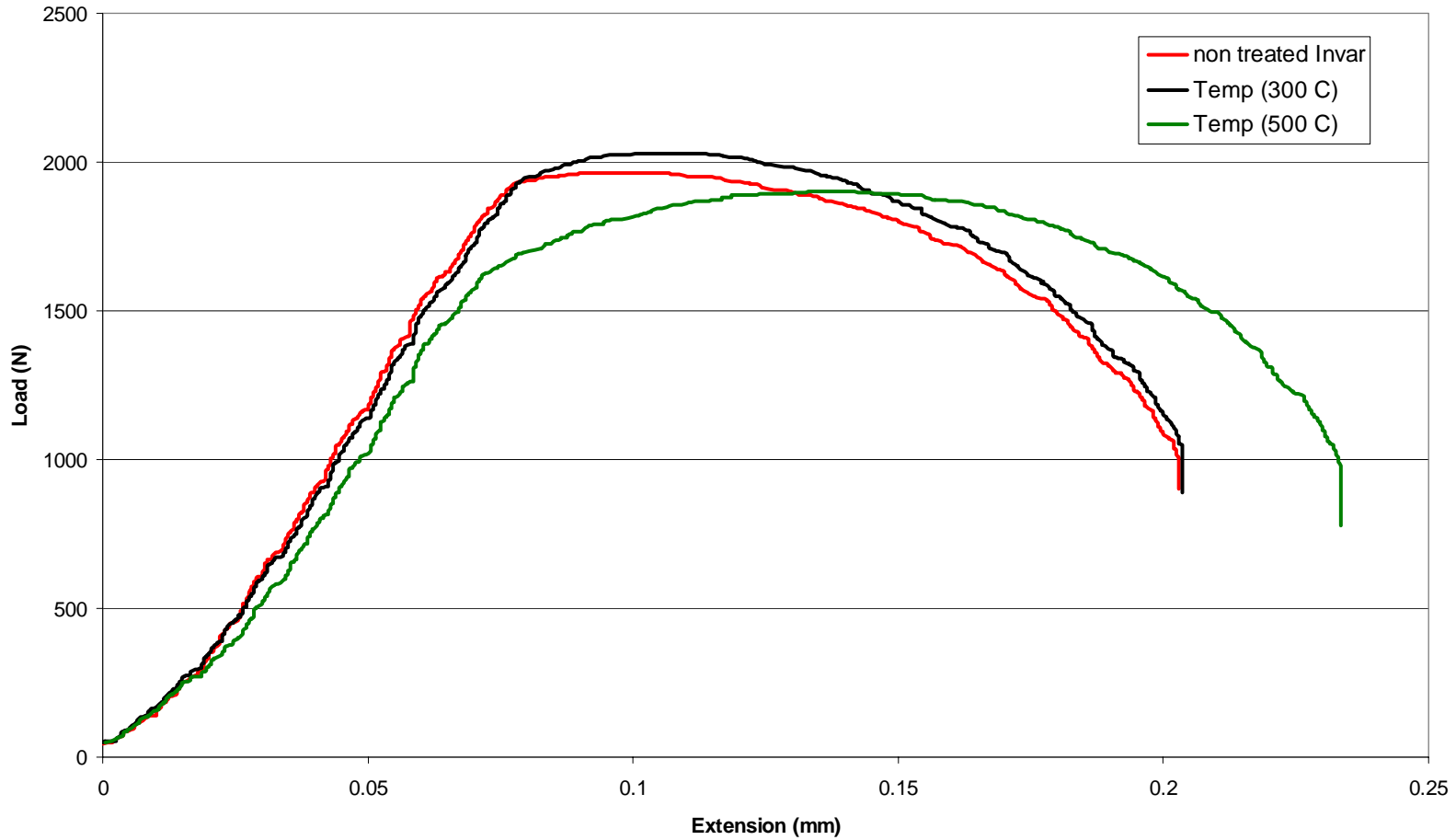
- High-Z with low CTE (0-150 °C)
- How is CTE affected by radiation?
- What happens to other important properties?

Super-Invar Irradiation Study - Irradiation vs. Yield Strength



Super-Invar Irradiation Study – Temperature Effects

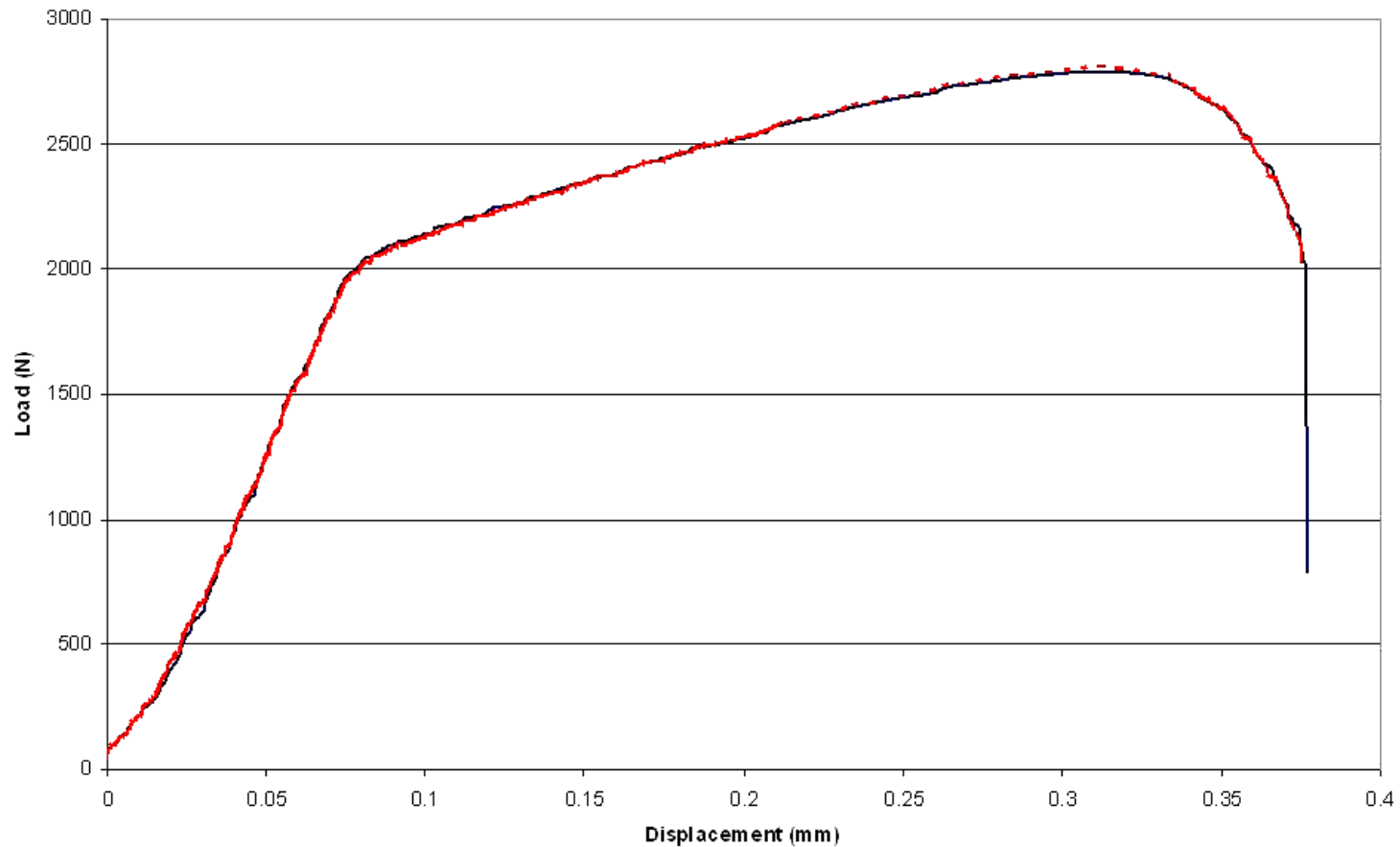
Effect of Heat Treatment in non-Irradiated Invar Samples



Super-Invar Irradiation Study

Stress-strain (load-displacement) in stainless steel samples to test system stability

Verification of System Stability on Stainless Steel Samples



PHASE-II TARGET MATERIAL STUDY

WHAT'S NEXT ? Repeat irradiation/mechanical property changes experiment for baseline materials

Carbon-Carbon composite

This low-Z composite gives the indication that it can minimize the thermal shock and survive high intensity pulses. Because of its premise it is the baseline target material for the BNL neutrino superbeam initiative. The way its key properties (such as CTE or strength) degrade with radiation is unknown.

Titanium Ti-6Al-4V alloy

The evaluation of the fracture toughness changes due to irradiation is of interest regarding this alloy that combines good tensile strength and relatively low CTE

Toyota “Gum Metal”

This alloy with the ultra-low elastic modulus, high strength, super-elastic like nature and near-zero linear expansion coefficient for the temperature range -200 °C to +250 °C to be assessed for irradiation effects on these properties.

VASCOMAX

This very high strength alloy that can serve as high-Z target to be evaluated for effects of irradiation on CTE, fracture toughness and ductility loss

AlBeMet

A low-Z composite that combines good properties of Be and Al. Effects of irradiation on CTE and mechanical properties need to be assessed

TG-43 Graphite

PHASE-II TARGET MATERIAL STUDY

WHAT'S DIFFERENT FROM PHASE-I?

~ 100 MeV of Proton Beam (200 to 100 MeV)

Challenge of inducing UNIFORM Beam degradation

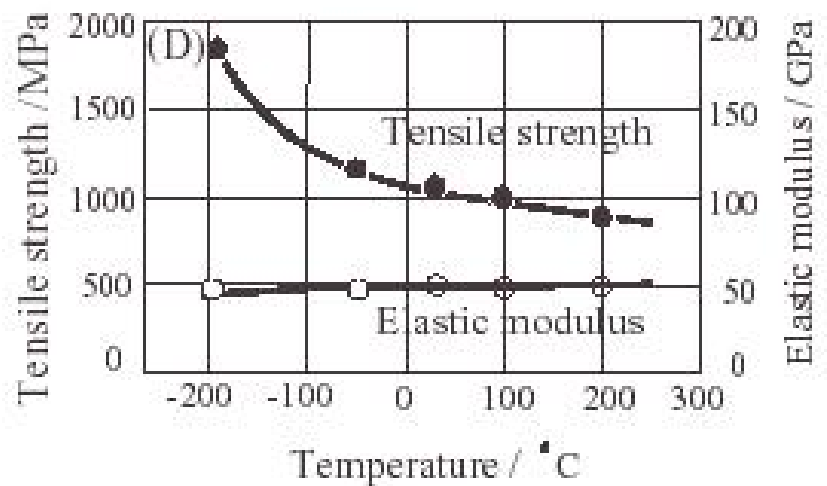
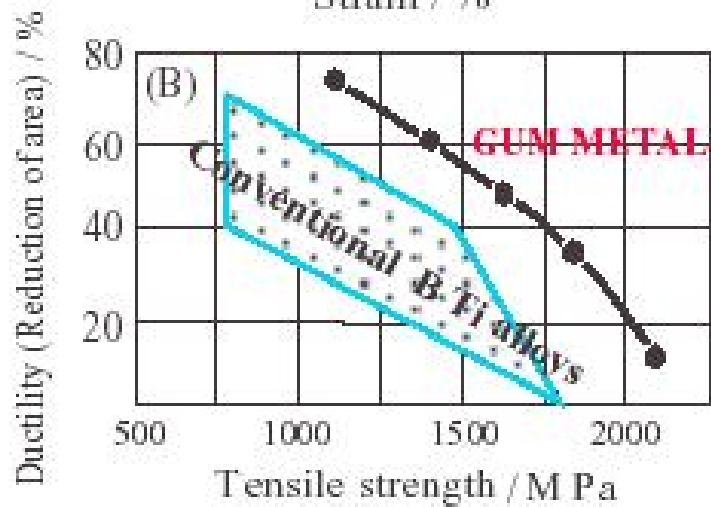
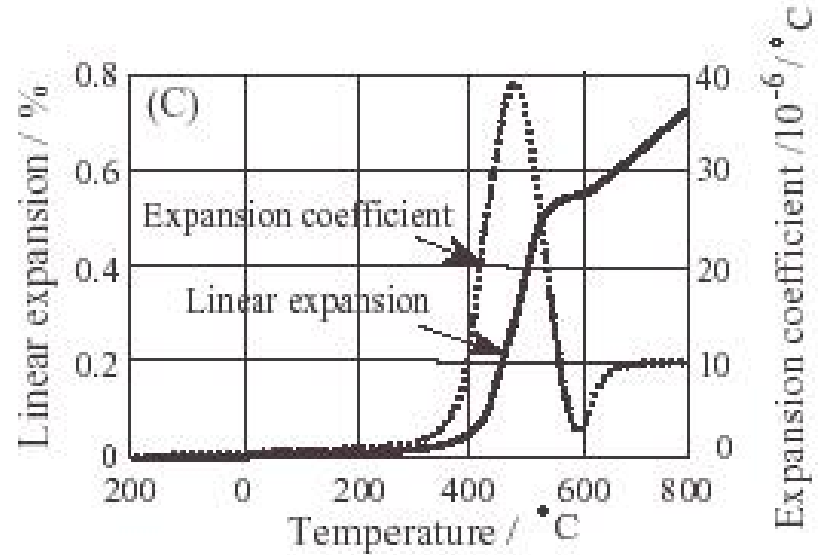
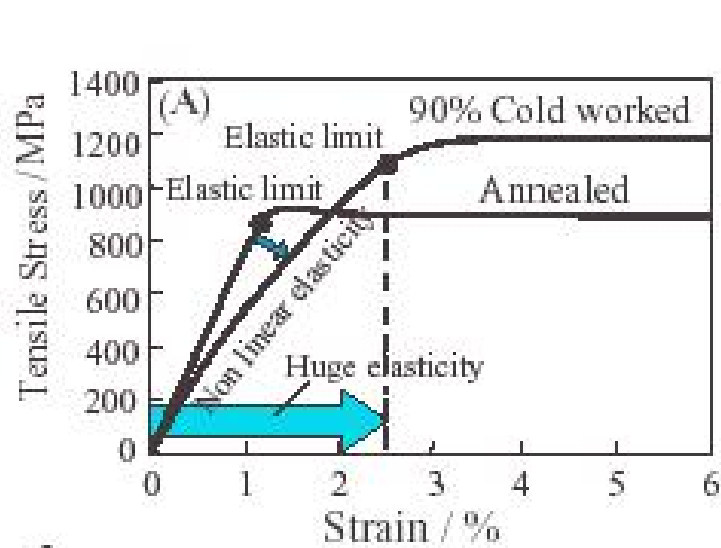
MORE Material to go in (optimization of dE/dx for range 200 MeV-100 MeV)

OPEN Issue: Study of Fracture Toughness for some materials ?

Carbon-Carbon Composite Target

Temp.	% elongation
23 ° C	0%
200 ° C	-0.023%
400° C	-0.028%
600° C	-0.020%
800° C	0%
1000° C	0.040%
1200° C	0.084%
1600° C	0.190%
2000° C	0.310%
2300° C	0.405%

Gum Metal (Toyota Ti alloy)



AlBeMet®

AM162

- By weight, contains 62% commercially pure beryllium and 38% commercially pure aluminum
- By Metallurgical definition, AlBeMet® is an alloy but can be considered a composite
- AlBeMet® sheet, plate and bar are powder metallurgy products
 - The powder is produced by a gas atomization process which yields spherical powder with a fine beryllium structure
 - The powder is densified by three consolidation processes, each resulting in different mechanical properties, while maintaining AlBeMet's unique physical properties.

AlBeMet® Property Comparison

Property	Beryllium S200F/AMS7906	AlBeMet AM16H/AMS7911	E-Material E-60	Magnesium AZ80A T6	Aluminum 6061 T6	Stainless Steel 304	Copper H04	Titanium Grade 4
Density lbs/cuin (g/cc)	0.067 (1.86)	0.076 (2.10)	0.091 (2.61)	0.066 (1.80)	0.098 (2.70)	0.29 (8.0)	0.32 (8.9)	0.163 (4.6)
Modulus MSI (Gpa)	44 (303)	28 (193)	48 (331)	6.6 (46)	10 (69)	30 (206)	16.7 (116)	16.2 (106)
UTS KSI (Gpa)	47 (324)	38 (262)	39.3 (273)	49 (340)	46 (310)	76 (516)	46 (310)	96.7 (660)
YS KSI (Gpa)	36 (241)	28 (193)	N/A	36 (260)	40 (276)	30 (206)	40 (276)	86.6 (690)
Elongation %	2	2	< .06	6	12	40	20	20
Fatigue Strength KSI (Gpa)	37.9 (261)	14 (97)	N/A	14.6 (100)	14 (96)	N/A	N/A	N/A
Thermal Conductivity btu/hr/ft/F (W/m-K)	126 (216)	121 (210)	121 (210)	44 (76)	104 (180)	9.4 (16)	226 (391)	9.76 (16.9)
Heat Capacity btu/lb-F (J/g-C)	.46 (1.96)	.373 (1.66)	.310 (1.26)	.261 (1.06)	.214 (.896)	.12 (.6)	.092 (.386)	.129 (.54)
CTE ppm/F (ppm/C)	6.3 (11.3)	7.7 (13.9)	3.4 (6.1)	14.4 (26)	13 (24)	9.6 (17.3)	9.4 (17)	4.8 (8.6)
Electrical Resistivity ohm-cm	4.2 E-06	3.6 E-06	N/A	14.6 E-06	4 E-06	72 E-06	1.71 E-06	60 E-06



VASCOMAX® C-200/C-250/C-300/C-350

Nominal Mechanical Properties of Small Diameter Bars Following Aging Heat Treatment
Figure 1

	VascoMax C-200	VascoMax C-250	VascoMax C-300	VascoMax C-350
Ultimate Tensile Strength, psi	210,000	260,000	294,000	350,000
0.2% Yield, psi	206,000	255,000	290,000	340,000
Elongation, %	12	11	11	7
Reduction of Area, %	62	58	57	35
Notch Tensile (K _t = 9.0), psi	325,000	380,000	420,000	330,000
Charpy V-Notch, ft-lb	36	20	17	10
Fatigue Endurance Limit (10 ⁶ Cycles), psi	110,000	110,000	125,000	110,000
Rockwell "C" Hardness	43/48	48/52	50/55	55/60
Compressive Yield Strength, psi	213,000	280,000	317,000	388,000

VASCOMAX® C-200

Physical Properties

Average Coefficient of Thermal Expansion (70-900° F)	5.6 × 10 ⁻⁶ in/in/°F
Modulus of Elasticity	26.2 × 10 ⁶ psi
Density	.289 lbs/cu. in. (8.0 g/cc)
Thermal Conductivity at 68° F	11.3 BTU/(ft)(hr)(°F)
at 122° F	11.6 BTU/(ft)(hr)(°F)
at 212° F	12.1 BTU/(ft)(hr)(°F)

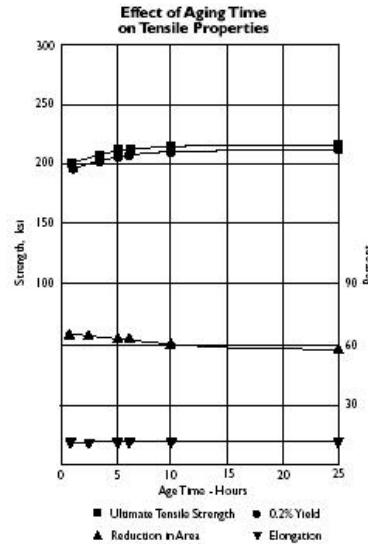
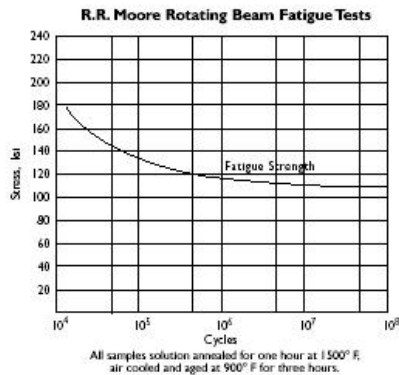
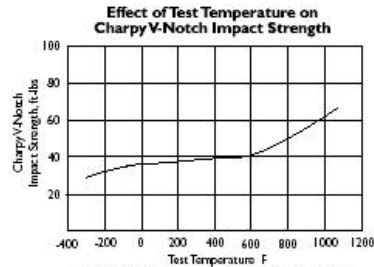
Nominal Annealed Properties

Hardness	30 Rc
Yield Strength	100 ksi
Ultimate Strength	140 ksi
Elongation	18%
Reduction of Area	72%

Nominal Room Temperature Properties after Aging

Size	Direction	Hardness Rockwell "C"	Tensile Strength ksi	0.2% Yield Strength ksi	Elongation in 4.5√A %	Reduction of Area %
5/8" Round	Longitudinal	43.4	212.0	207.7	12.5	61.7
1/2" Round	Longitudinal	43.0	214.3	208.5	12.0	60.6
3" Round	Longitudinal	42.8	210.0	204.2	11.9	60.4
6" Square	Longitudinal	43.5	208.4	202.6	11.6	58.8
	Transverse	43.9	206.9	200.1	8.9	41.7
.250" Sheet	Transverse	42.9	218.1	213.0	11.0	45.0

VASCOMAX® C-200



Mechanical Properties**Titanium Ti-6Al-4V (Grade 5), Annealed**

Hardness, Brinell	334	334	Estimated from Rockwell C.
Hardness, Knoop	363	363	Estimated from Rockwell C.
Hardness, Rockwell C	36	36	
Hardness, Vickers	349	349	Estimated from Rockwell C.
Tensile Strength, Ultimate	<u>950 MPa</u>	138000 psi	
Tensile Strength, Yield	<u>880 MPa</u>	128000 psi	
Elongation at Break	14 %	14 %	
Reduction of Area	36 %	36 %	
Modulus of Elasticity	<u>113.8 GPa</u>	16500 ksi	
Compressive Yield Strength	<u>970 MPa</u>	141000 psi	
Notched Tensile Strength	<u>1450 MPa</u>	210000 psi	K_t (stress concentration factor) = 6.7
Ultimate Bearing Strength	<u>1860 MPa</u>	270000 psi	e/D = 2
Bearing Yield Strength	<u>1480 MPa</u>	215000 psi	e/D = 2
Poisson's Ratio	0.342	0.342	
Charpy Impact	<u>17 J</u>	12.5 ft-lb	V-notch
Fatigue Strength	<u>240 MPa</u>	34800 psi	at 1E+7 cycles. K_t (stress concentration factor) = 3.3
Fatigue Strength	<u>510 MPa</u>	74000 psi	Unnotched 10,000,000 Cycles
Fracture Toughness	<u>75 MPa-m^{1/2}</u>	68.3 ksi-in ^{1/2}	
Shear Modulus	<u>44 GPa</u>	6380 ksi	
Shear Strength	<u>550 MPa</u>	79800 psi	

Electrical Properties**Titanium Ti-6Al-4V (Grade 5), Annealed**

Electrical Resistivity	<u>0.000178 ohm-cm</u>	0.000178 ohm-cm	
Magnetic Permeability	1.00005	1.00005	at 1.6kA/m
Magnetic Susceptibility	3.3e-006	3.3e-006	cgs/g

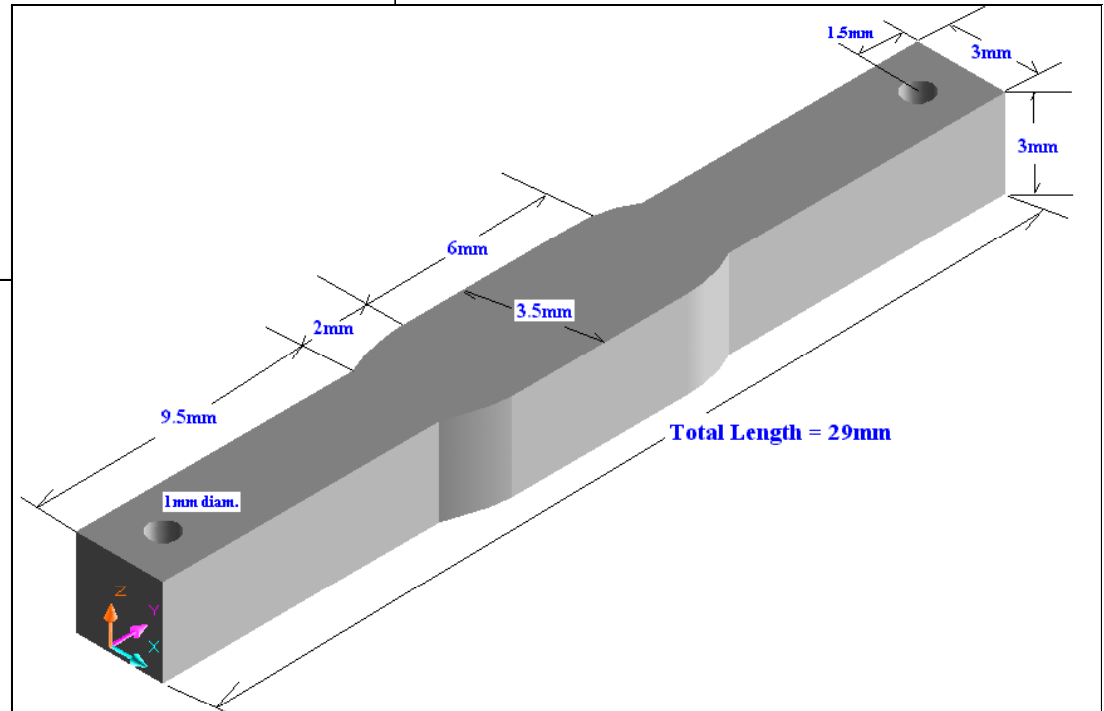
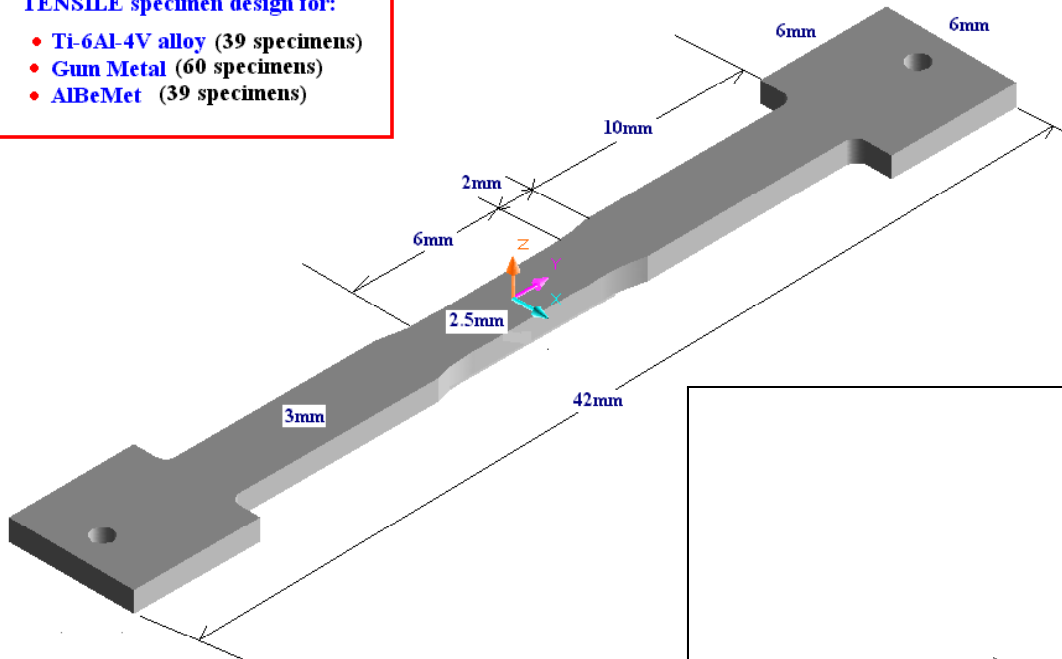
Thermal Properties

CTE, linear 20°C	<u>8.6 $\mu\text{m}/\text{m}\cdot^\circ\text{C}$</u>	4.78 $\mu\text{in}/\text{in}\cdot^\circ\text{F}$	20-1001C
CTE, linear 250°C	<u>9.2 $\mu\text{m}/\text{m}\cdot^\circ\text{C}$</u>	5.11 $\mu\text{in}/\text{in}\cdot^\circ\text{F}$	Average over the range 20-3151C
CTE, linear 500°C	<u>9.7 $\mu\text{m}/\text{m}\cdot^\circ\text{C}$</u>	5.39 $\mu\text{in}/\text{in}\cdot^\circ\text{F}$	Average over the range 20-6501C
Heat Capacity	<u>0.5263 J/g$\cdot^\circ\text{C}$</u>	0.126 BTU/lb $\cdot^\circ\text{F}$	
Thermal Conductivity	<u>6.7 W/m-K</u>	46.5 BTU-in/hr-ft ² $\cdot^\circ\text{F}$	
Melting Point	1604 - 1660 °C	2920 - 3020 °F	
Solidus	<u>1604 °C</u>	2920 °F	
Liquidus	<u>1660 °C</u>	3020 °F	
Beta Transus	<u>980 °C</u>	1800 °F	

Tensile & CTE Specimen Design for Upcoming Irradiation Study

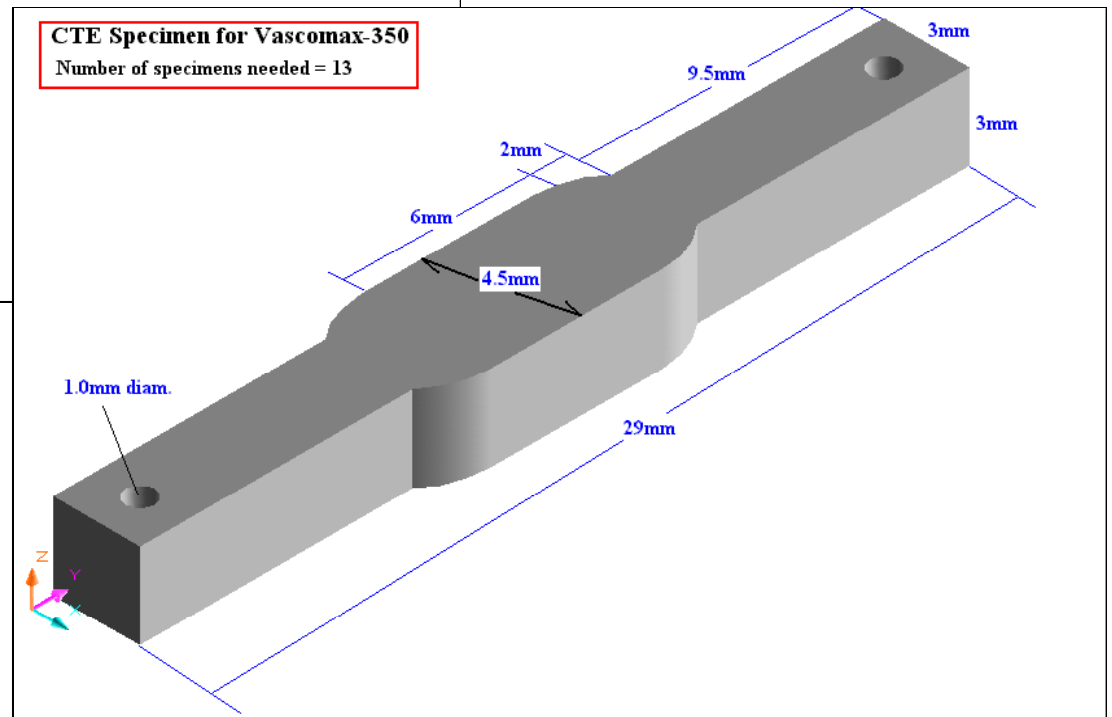
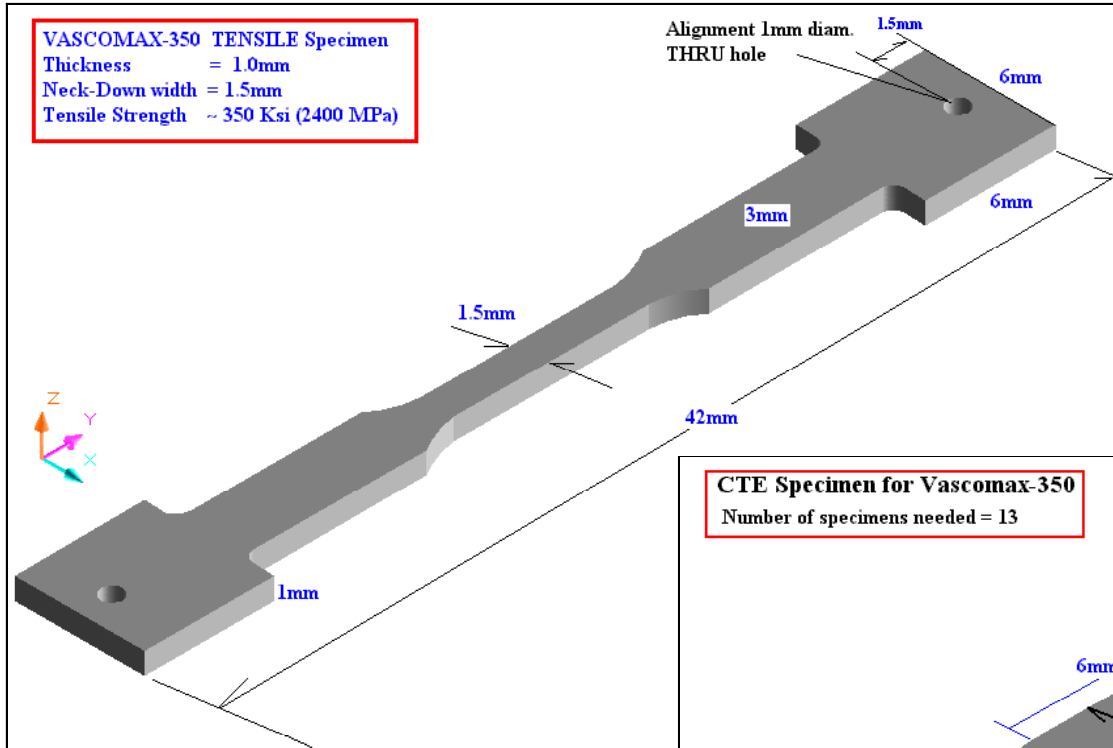
TENSILE specimen design for:

- Ti-6Al-4V alloy (39 specimens)
- Gum Metal (60 specimens)
- AlBeMet (39 specimens)



Tensile & CTE Specimen Design for Upcoming Irradiation Study

Vascomax-350 specimen variation due to its high strength



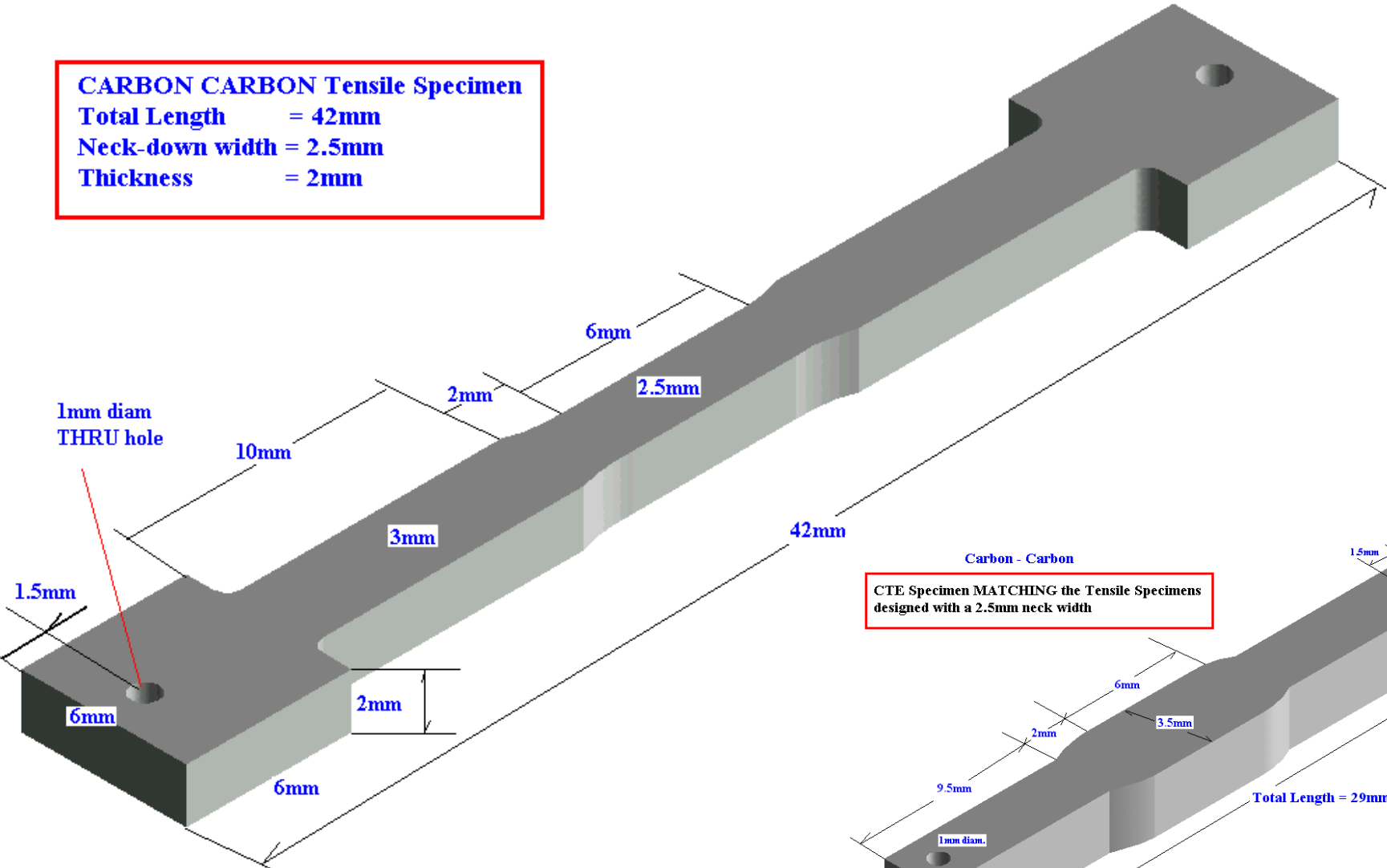
Tensile & CTE Specimen Design for Carbon-Carbon and TG-43 Graphite

CARBON CARBON Tensile Specimen

Total Length = 42mm

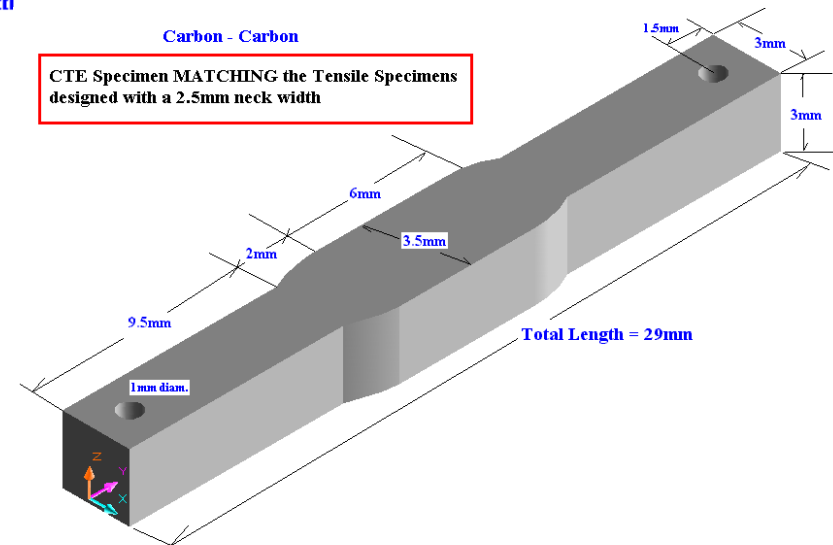
Neck-down width = 2.5mm

Thickness = 2mm

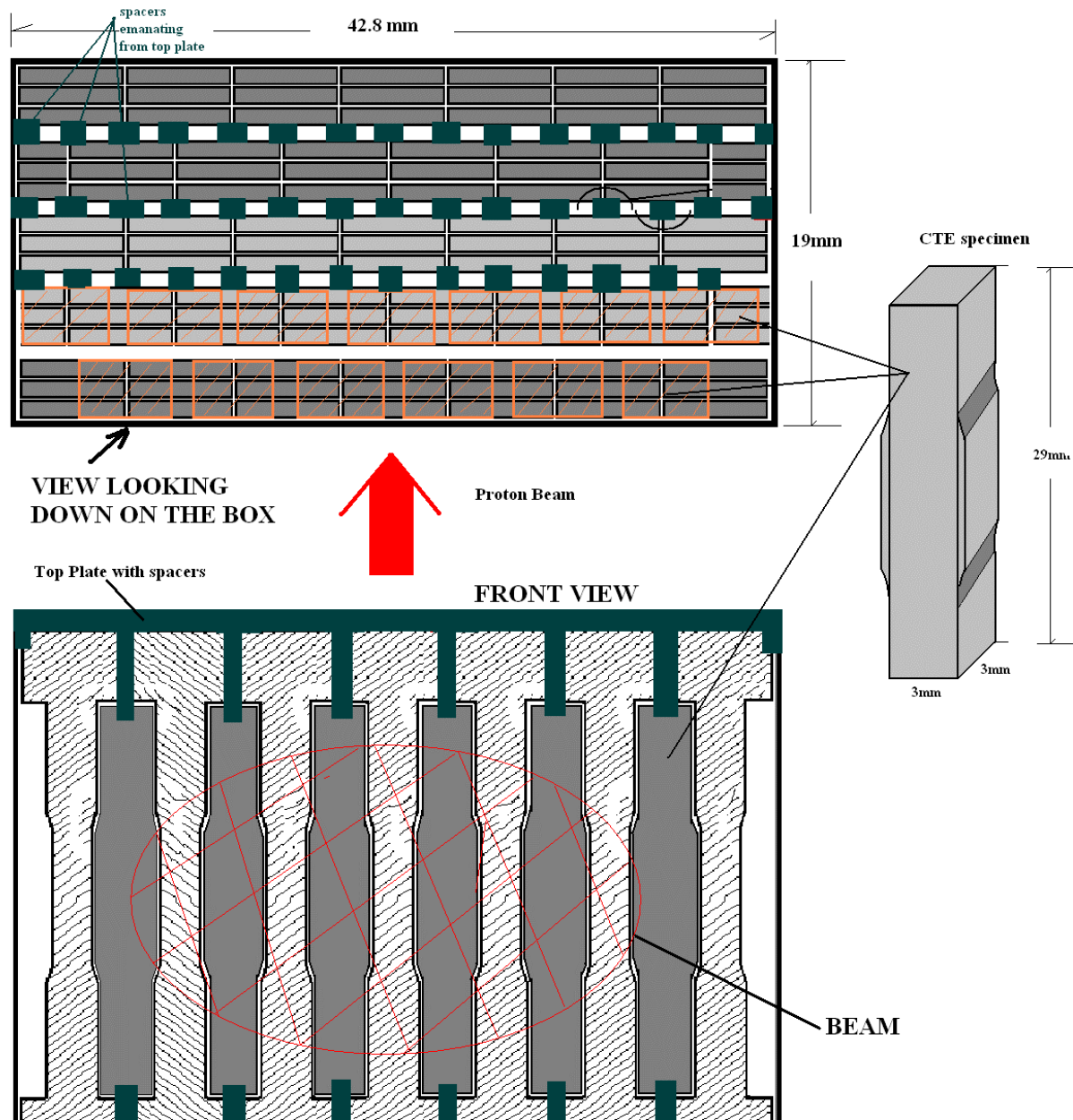


Carbon - Carbon

CTE Specimen MATCHING the Tensile Specimens designed with a 2.5mm neck width



LAYOUT OF Specimen Assembly



Tentative Sample Identification Scheme

~0.5mm diam. blind hole(s)
indicating the column of the specimen
0 = dead center
1 = 1st to right (hole at position 1)
2 = 2nd to right (holes at 1 & 2)
3 = 3rd to right (holes at 1, 2 & 3)

- For RHS (going into BOX) holes on same face as LAYER indication
- For LHS on opposite face

**SPECIMEN SHOWN
is at position:**

- Layer-5 (4 chamfers)
- Back specimen in triplet
- Two (2) positions to the right from specimen at centerline

Alignment hole (1mm diam.)
in all specimens and at both
sides

~0.5mm blind hole(s) designating the position
of the specimen within a triplet (LAYER)
Zero holes = front
One hole = middle
Two holes = back

Chamfer denotes LAYER in Box (layer consists of 3 specimens in depth)

NO Chamfer = 1st layer into box

- 1 chamfer = layer 2
- 2 chamfers = layer 3
- 3 chamfers = layer 4
- 4 chamfers = layer 5

CTE specimen marking for Vasco-Ti-Gum

- LAYER - 1
- #3 RHS

Alignment Thru Hole (1mm diam)
present at both sides and ALL CTE
specimens

~0.5mm diam. blind
hole indicating Right
or Left side
Hole in figure is RHS

~0.5 diam blind hole indicating
position from center.

- NO hole = #1
- 1 hole = #2
- 2 holes = #3

CHAMFER indicating LAYER (Boxes with Vascomax, Ti,
Gum have 5 layers, CC and Graphite have 3 layers)

- NO chamfer = 1st layer
- 1 chamfer = 2nd layer
- 2 chamfers = 3rd layer
- 3 chamfers = 4th layer
- 4 chamfers = 5th layer