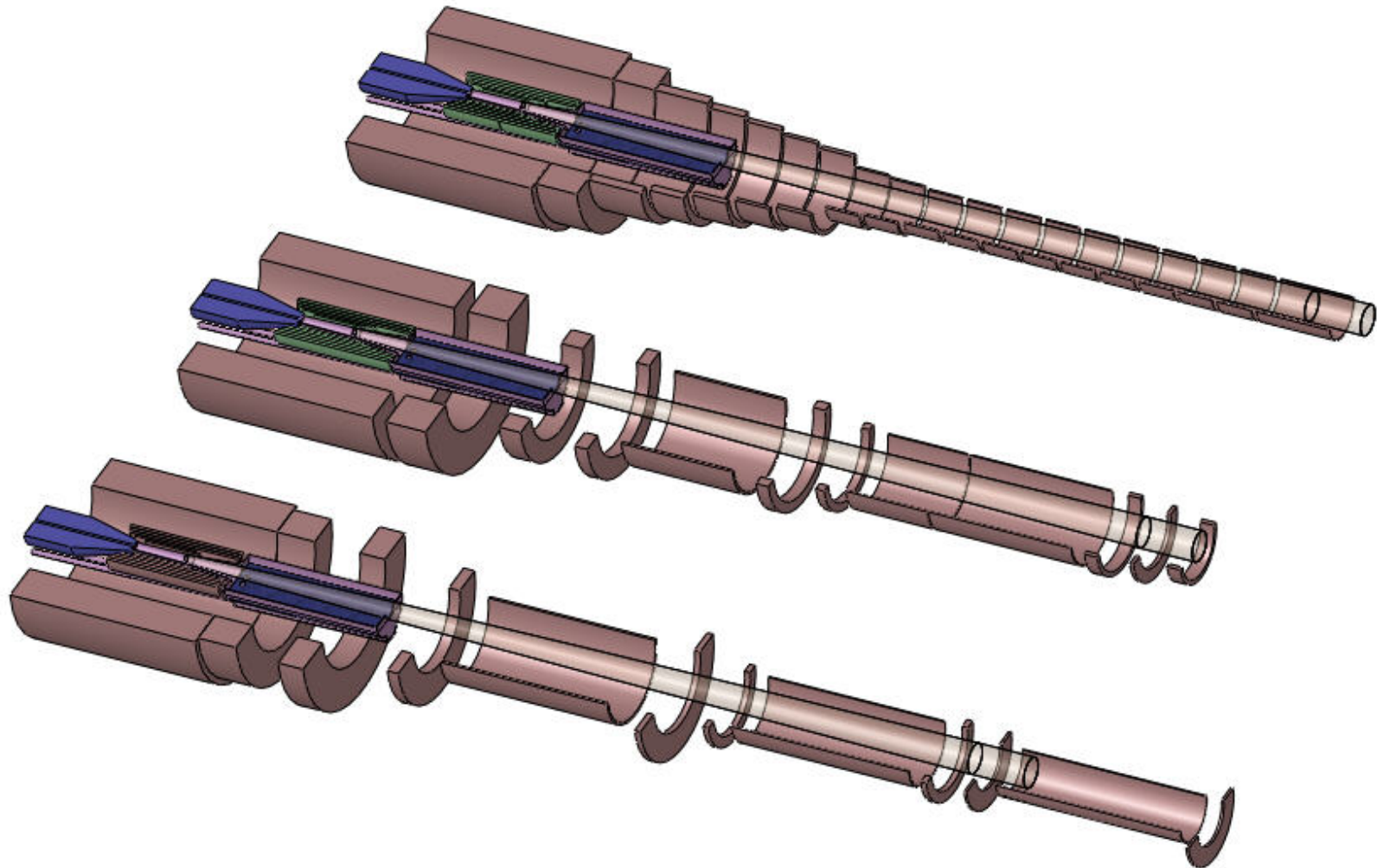


Target Magnets & Shielding

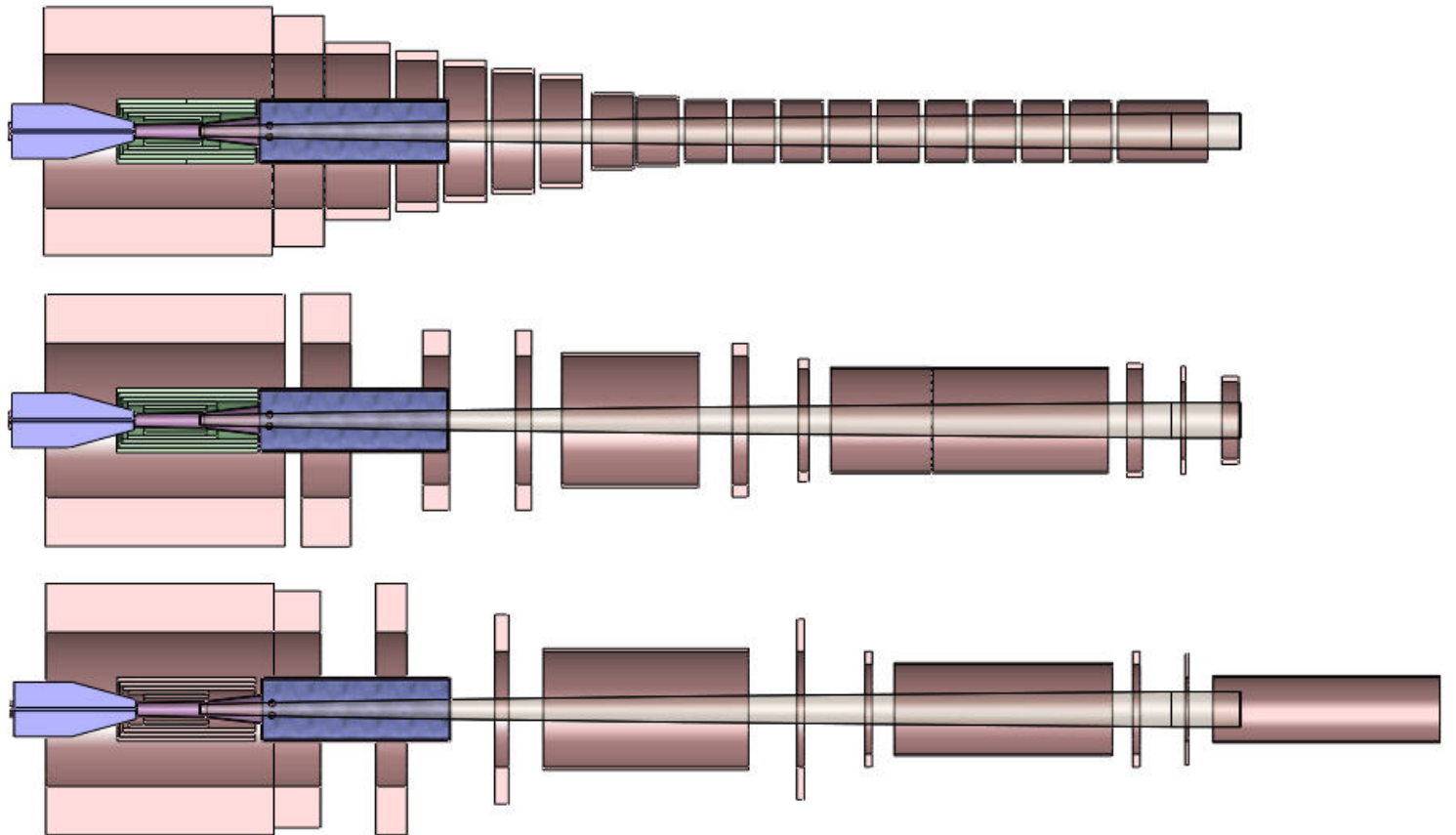
Bob Weggel
Particle Beam Lasers, Inc.
Magnet Optimization Research Engineering, LLC.
March 5, 2012

Isometric View of Three Target-Magnet Designs



Design IDS120h (top), IDS120i (middle) & IDS120j (bottom) [courtesy Van Graves]

Cross Sections of Target-Magnet Designs [courtesy Van Graves]

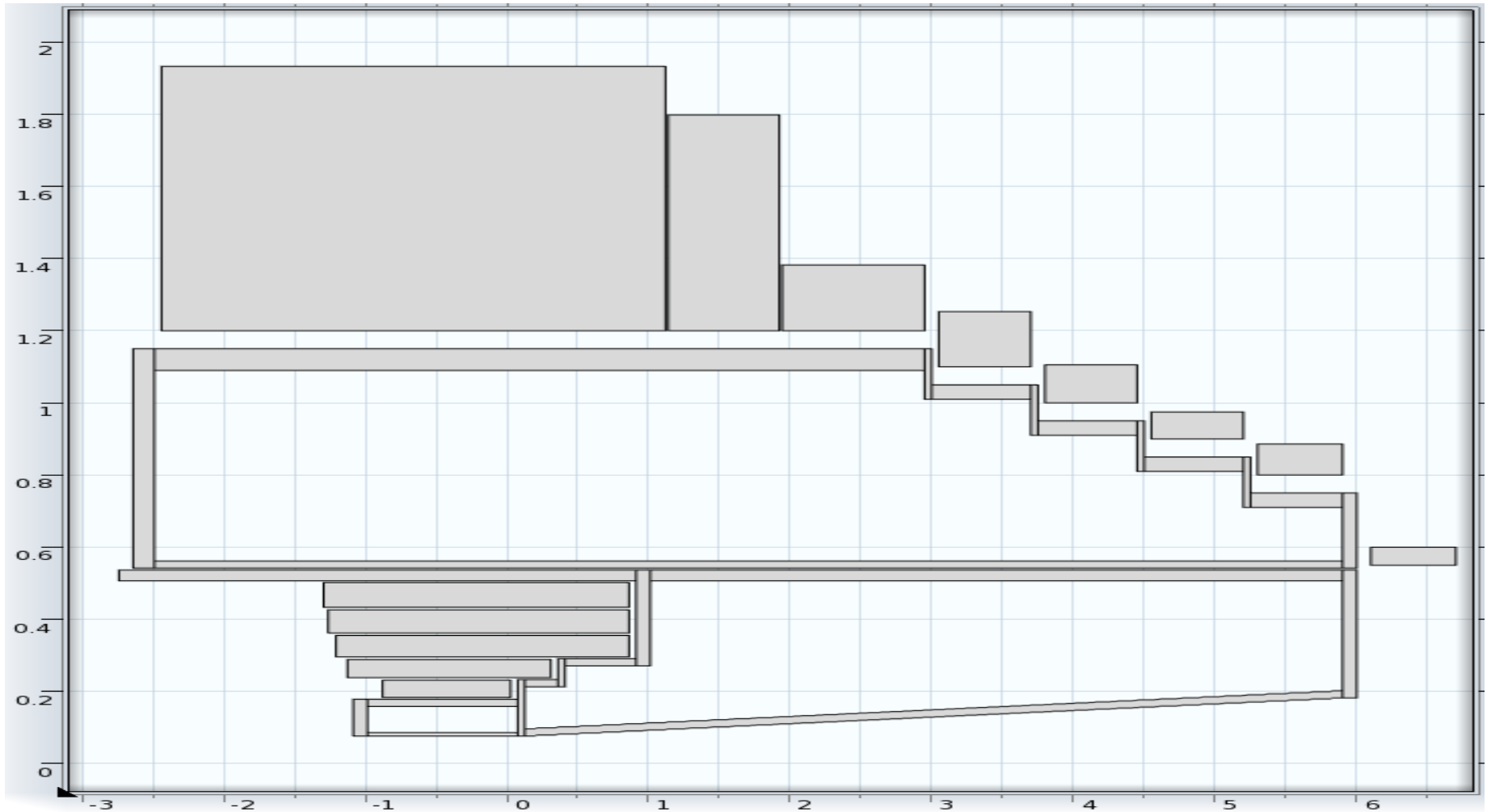


IDS120h: I.R.'s step down gradually from 120 cm to 45 cm; minimal gaps between coils

IDS120i: Large gaps between cryostats; I.R.'s = [120, 100, 80, 60] cm; gaps at [3, 9, 15] m

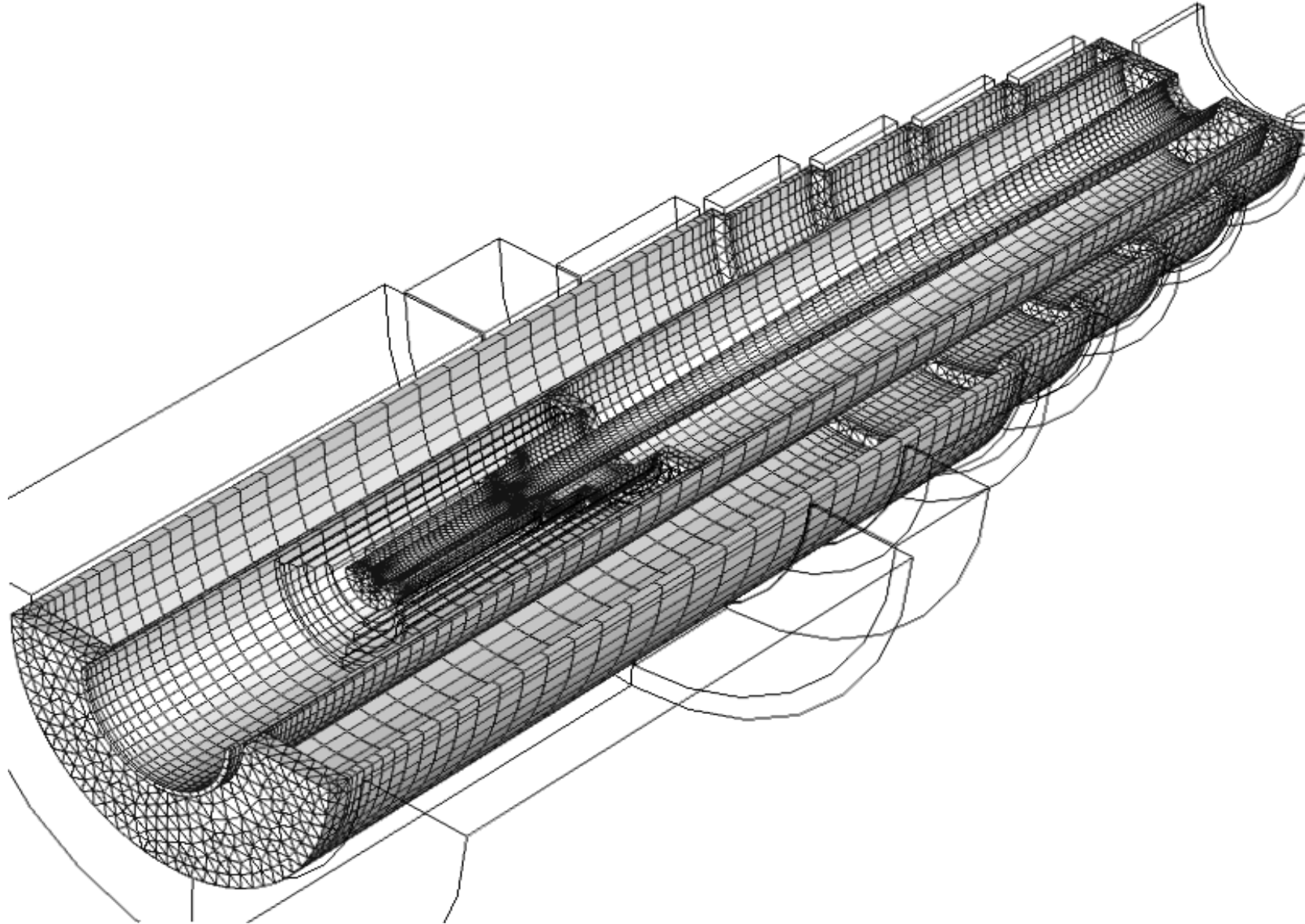
IDS120j: 3 coils per cryostat; I.R.'s = [120, 90, 70, 50] cm; gaps at [4, 10, 15] m; $z_{\max} = 20$ m

Cross section of Coils & Shielding Vessels of IDS120h

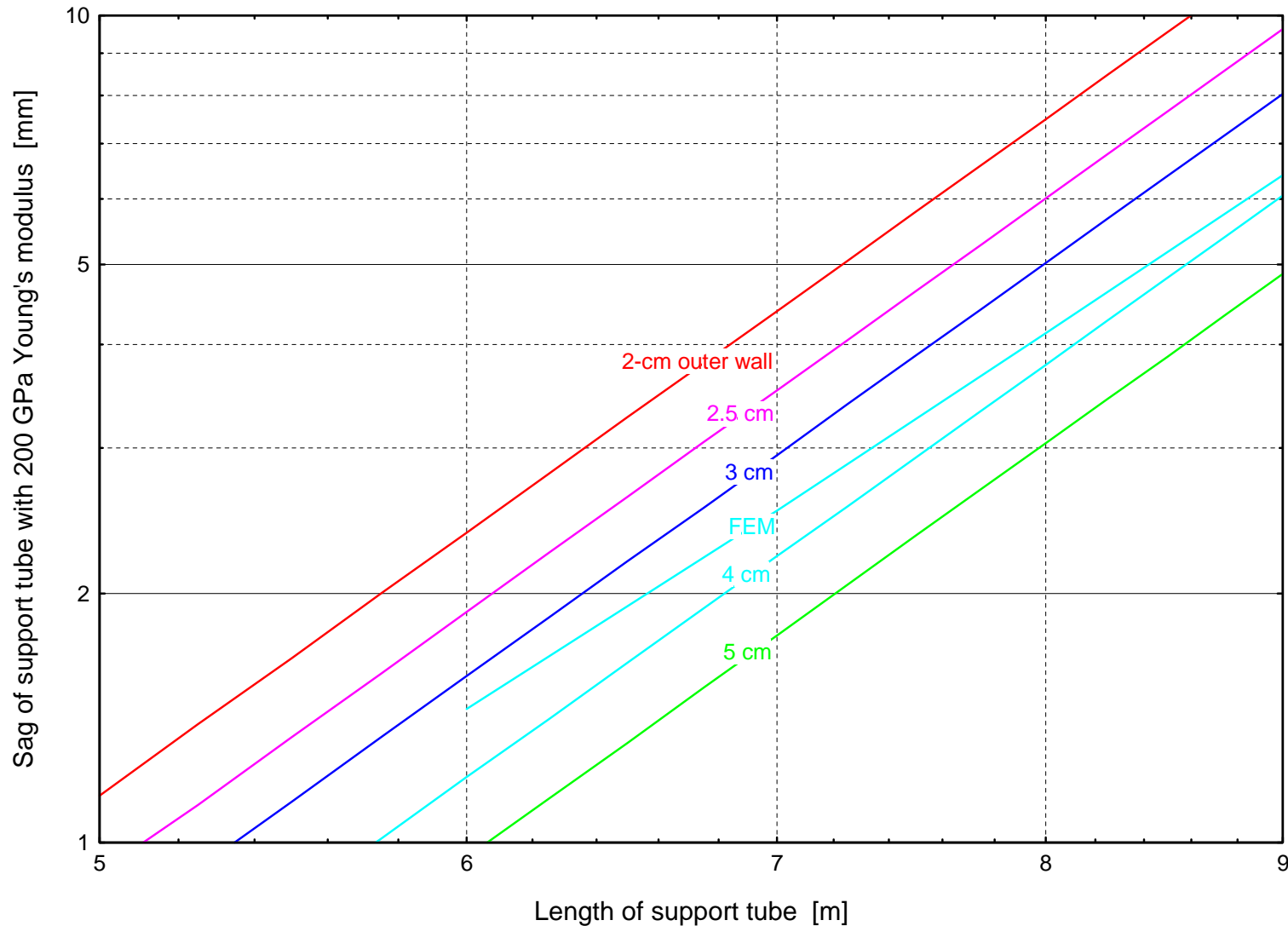


Tubes & flanges: = 7.85 g/cm^3 ; shielding = 10 g/cm^3 ; Outer $\approx 30 \text{ tons/m}$; Inner $\approx 8 \text{ tons/m}$.

Isometric View of Meshed Shielding Vessels of IDS120h

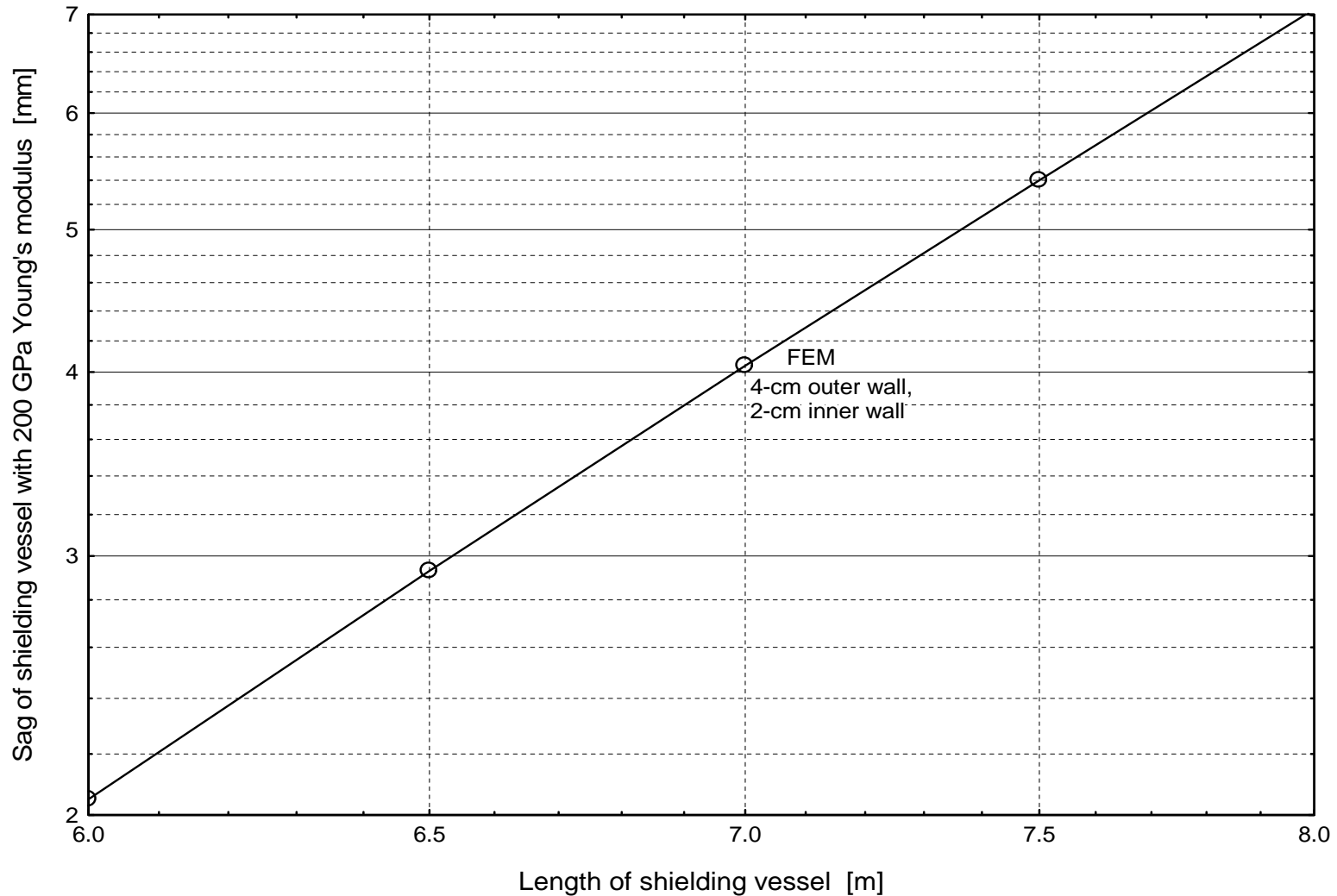


Sag of Shielding Vessel vs. Length L & Wall Thickness t



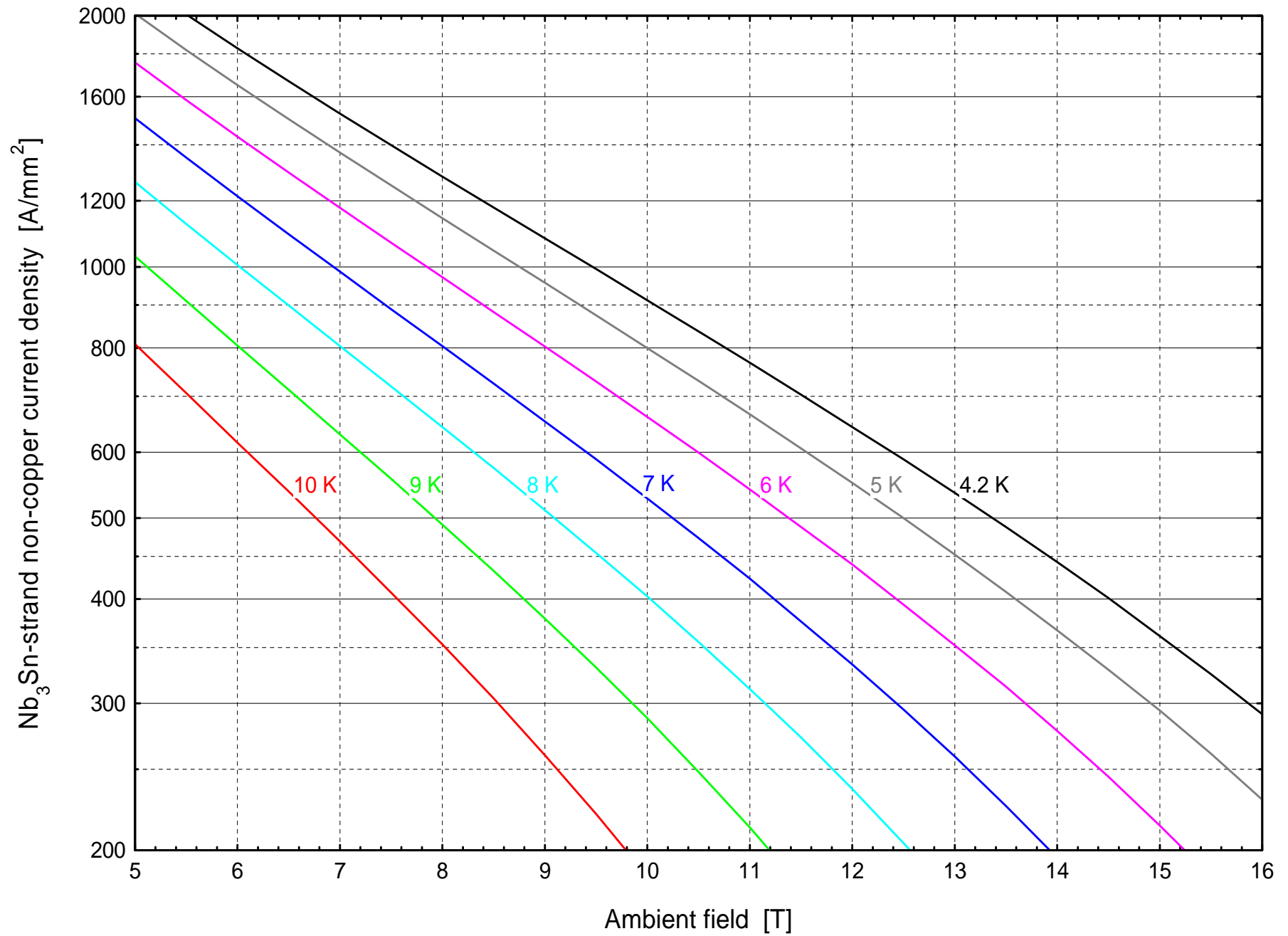
O.R._{max} = 114 cm; I.R._{min} = 60 cm; $\gamma = 7.85 \text{ g/cm}^3$; $\gamma_{\text{shielding}} = 10 \text{ g/cm}^3$; $t_{\text{in}} = \frac{1}{2}t_{\text{out}}$; $\sim 30 \text{ tons/m}$.
 With $t_{\text{out}} = 4 \text{ cm}$, $t_{\text{in}} = 2 \text{ cm}$ & $L = [6, 7, 8, 9] \text{ m}$, $\text{sag}_{\text{FEM}} = [1.5, 2.5, 4.1, 6.4] \text{ mm} \rightarrow \text{Limit } L \text{ to } 8 \text{ m}$.

Sag of Shielding Vessel vs. Length L & Wall Thickness t

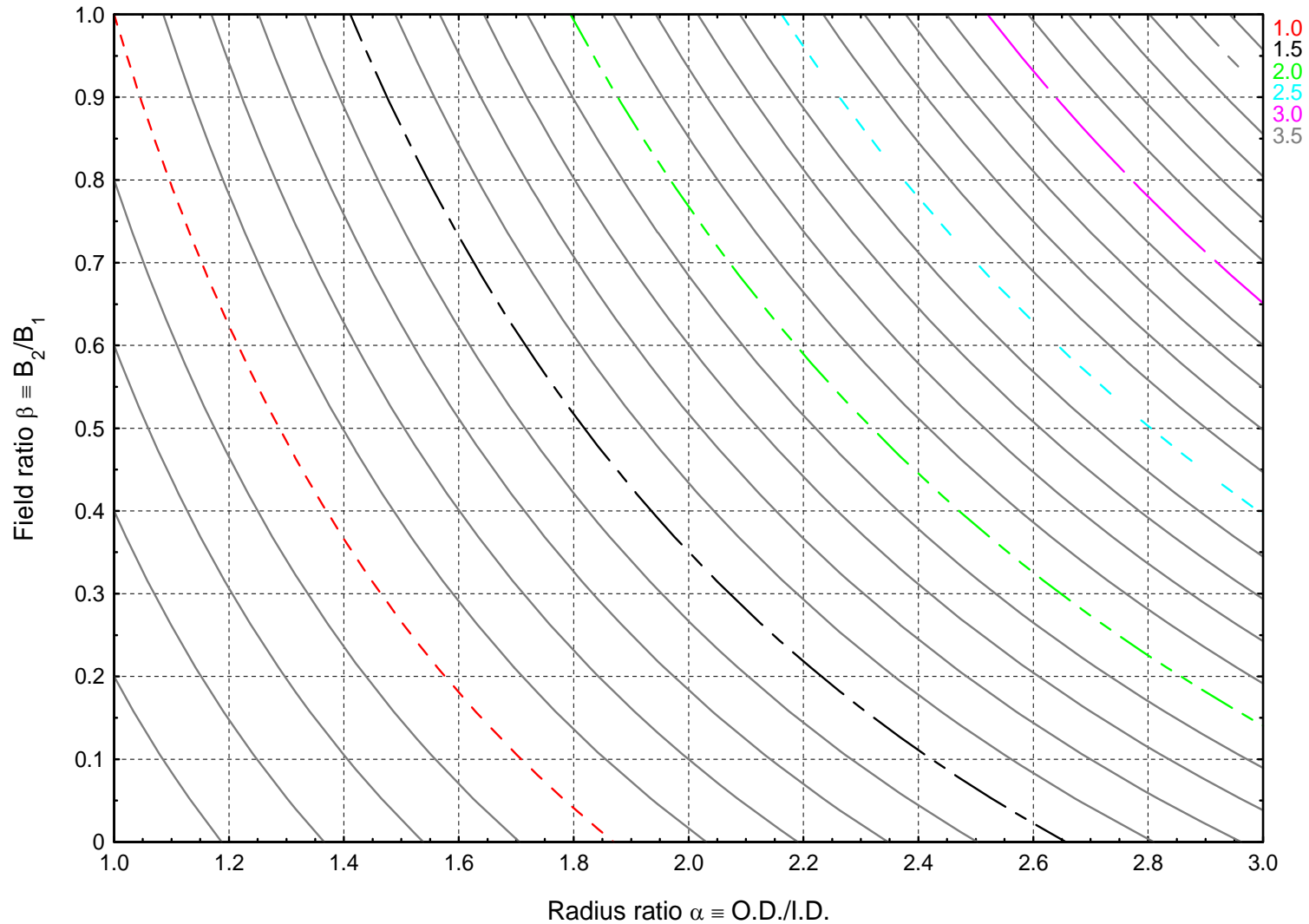


O.R._{max} = 58 cm; I.R._{min} = 16 cm; t_{out} = 4 cm; t_{in} = 2 cm; $\gamma = 7.85 \text{ g/cm}^3$; $\gamma_{shielding} = 10 \text{ g/cm}^3$; $\sim 8 \text{ tons/m}$. When $L = [6, 6\frac{1}{2}, 7, 7\frac{1}{2}, 8] \text{ m}$, sag = [2.0, 2.9, 4.0, 5.4, 8.0] mm \rightarrow Limit L to 7 m.

Field and Temperature Dependence of Current Density of Nb₃Sn Strands

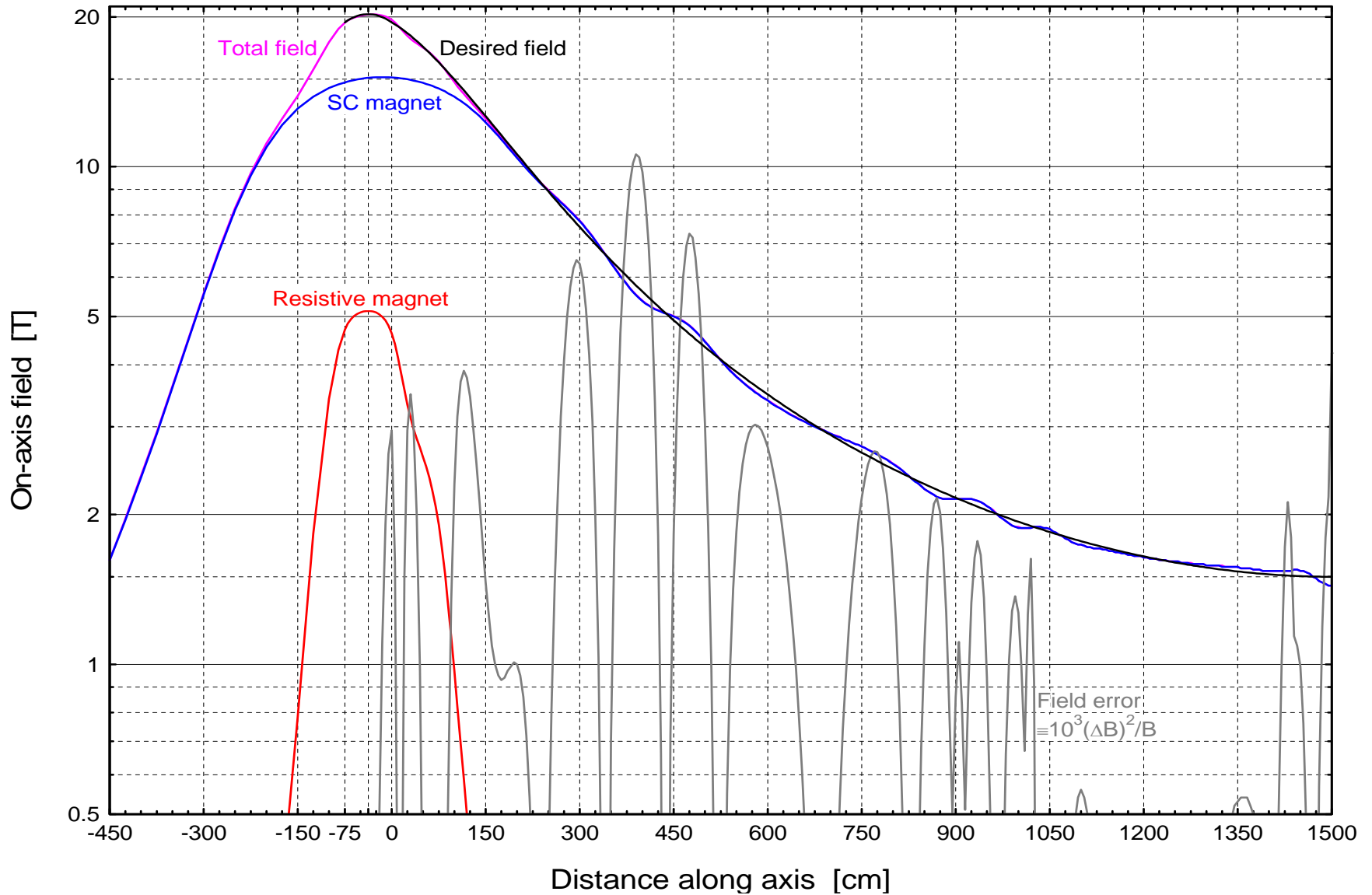


Normalized Maximum Hoop Stress $\sigma^* \equiv \sigma_{\max} / (B_1 j_1 a_1)$



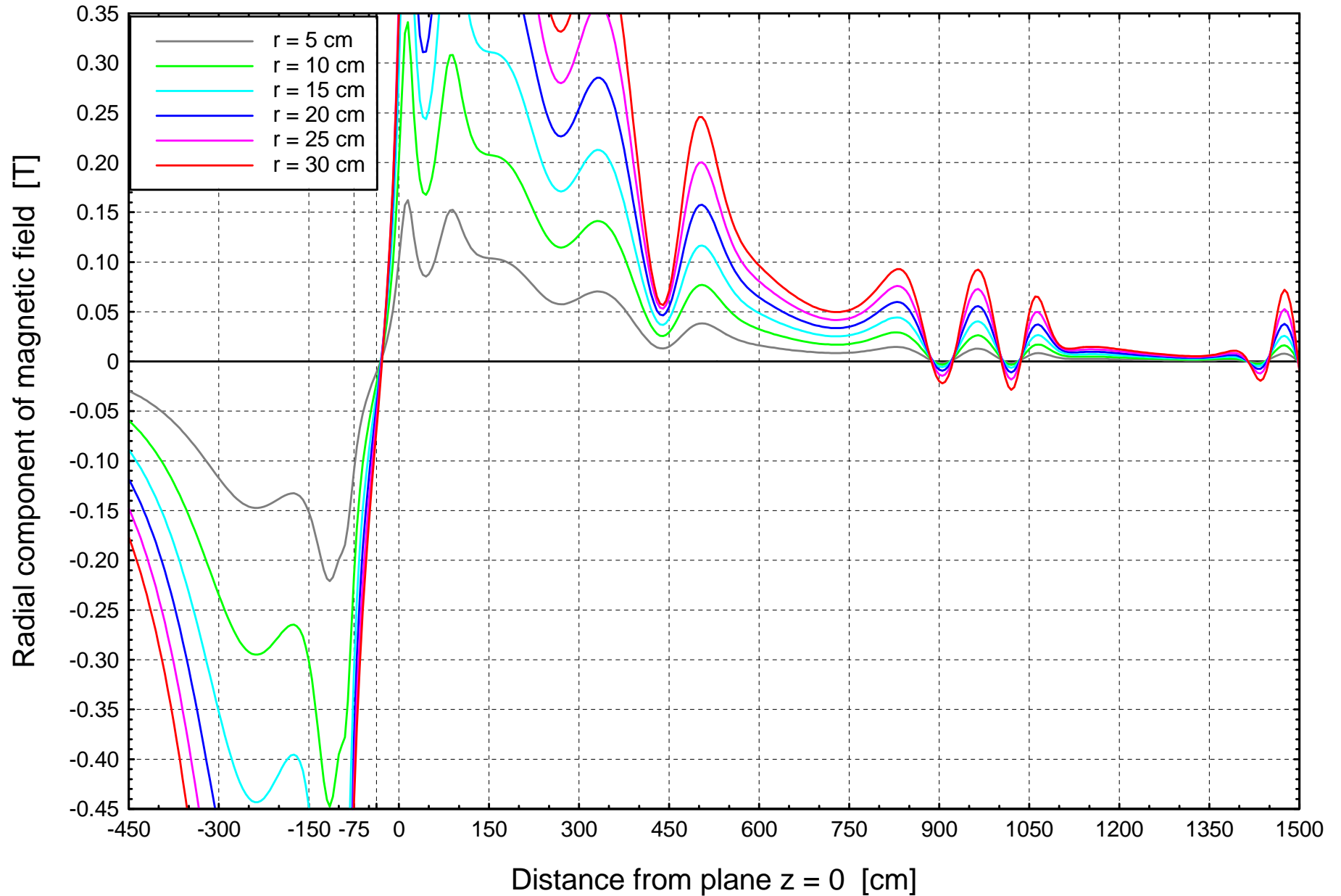
$a_1 \equiv \text{I.R. of coil}$; $a_2 \equiv \text{O.R. of coil}$; $B_1 \equiv B(r=a_1)$, $B_2 \equiv B(r=a_2)$; $j_1 \equiv \text{current density}$

On-Axis Field Profile B(z) of Target Magnet IDS120j

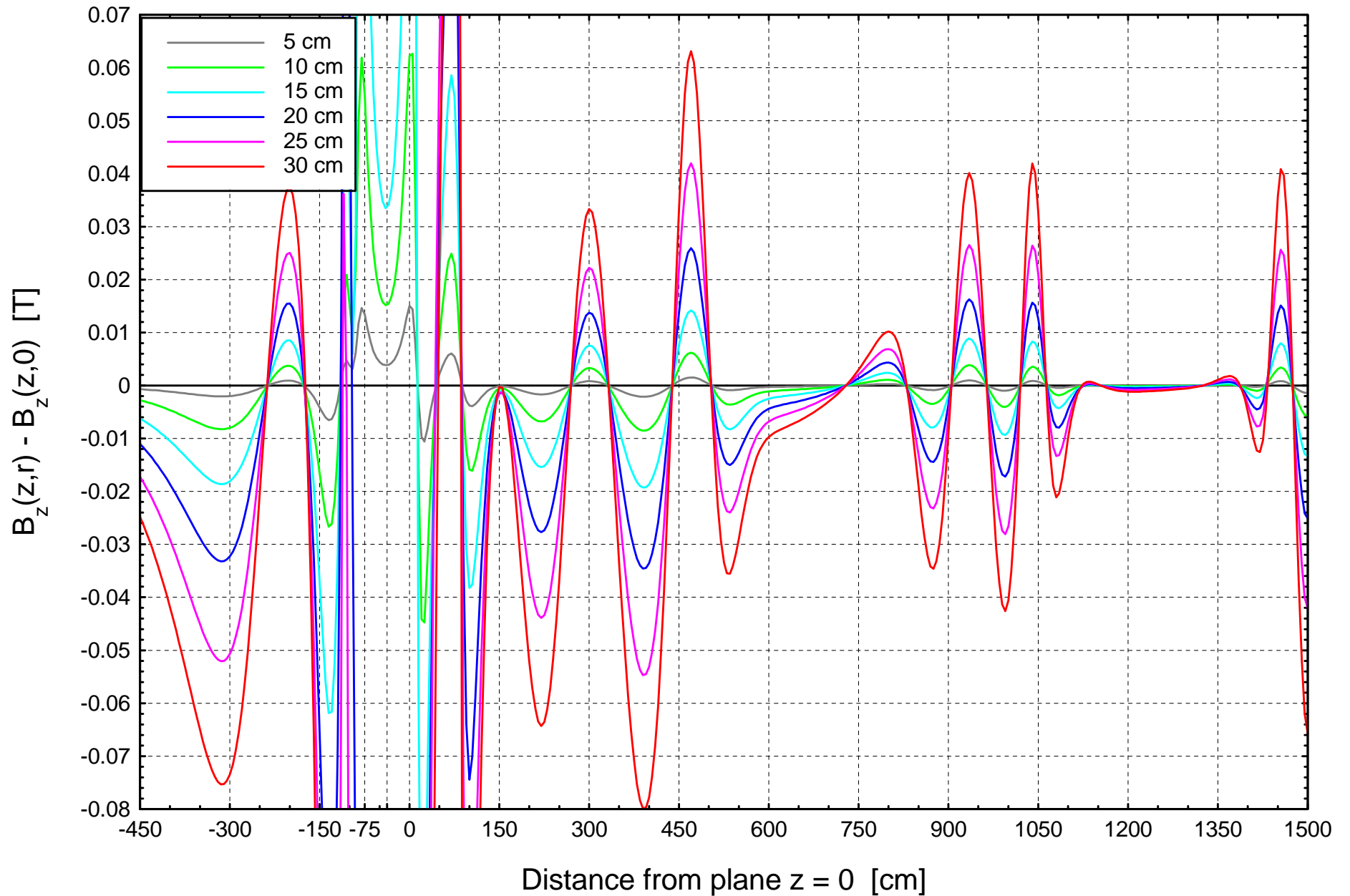


$\langle B(z) \rangle = 20$ T over the 75-cm length centered at $z = -37.5$ cm. $B(z=15 \text{ m}) \approx 1.5$ T.

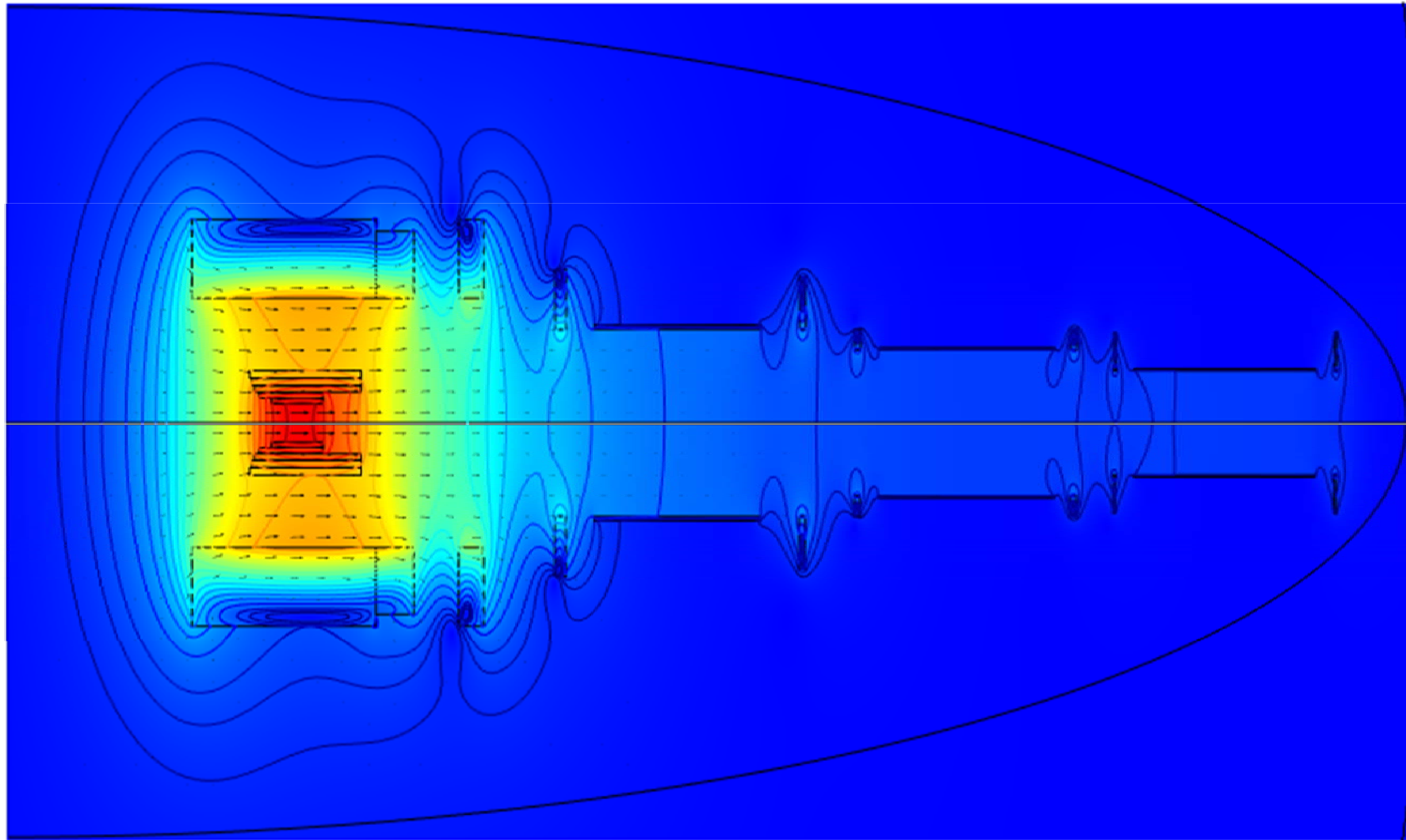
Radial Component of Off-Axis Field of Target Magnet IDS120j



$B_z(z,r) - B_z(z,0)$ of Off-Axis Field of Target Magnet IDS120j

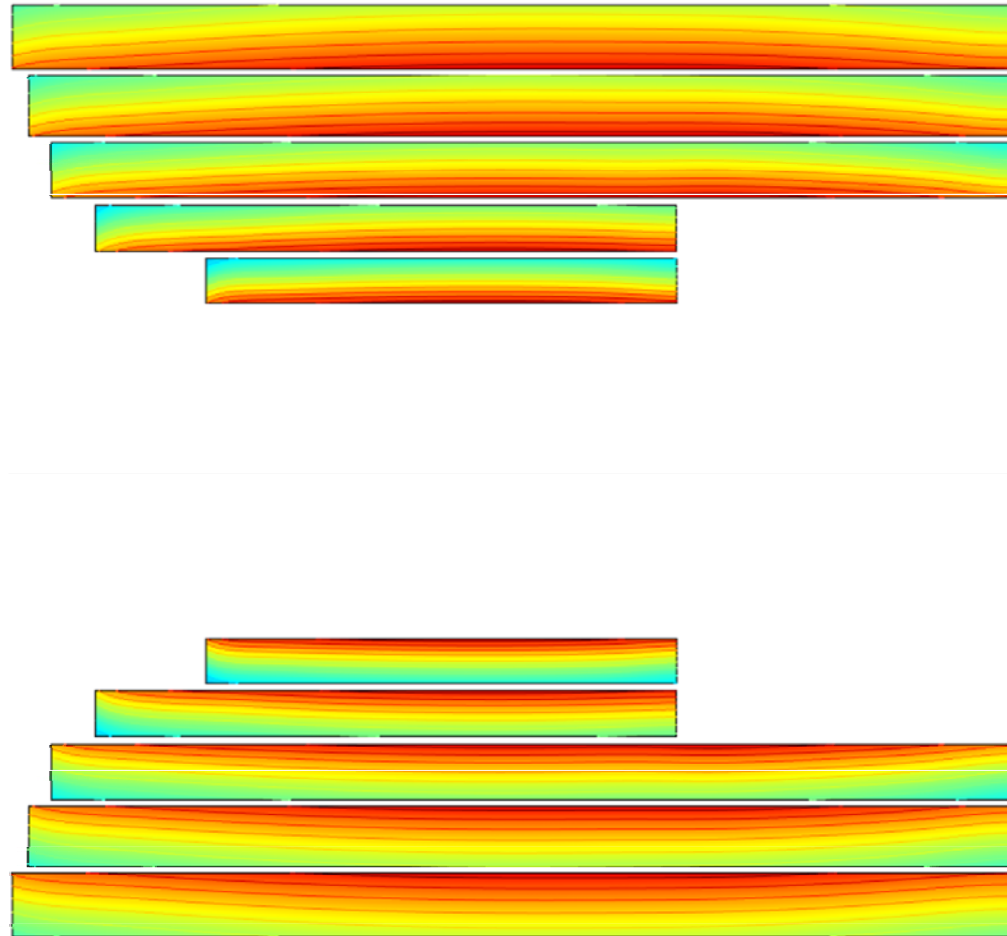


Field Magnitude $|B| \equiv (B_r^2 + B_z^2)^{1/2}$ of Target Magnet IDS120j



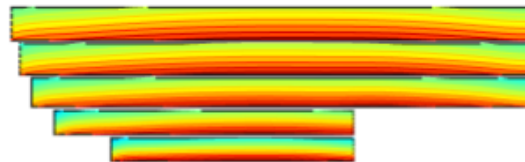
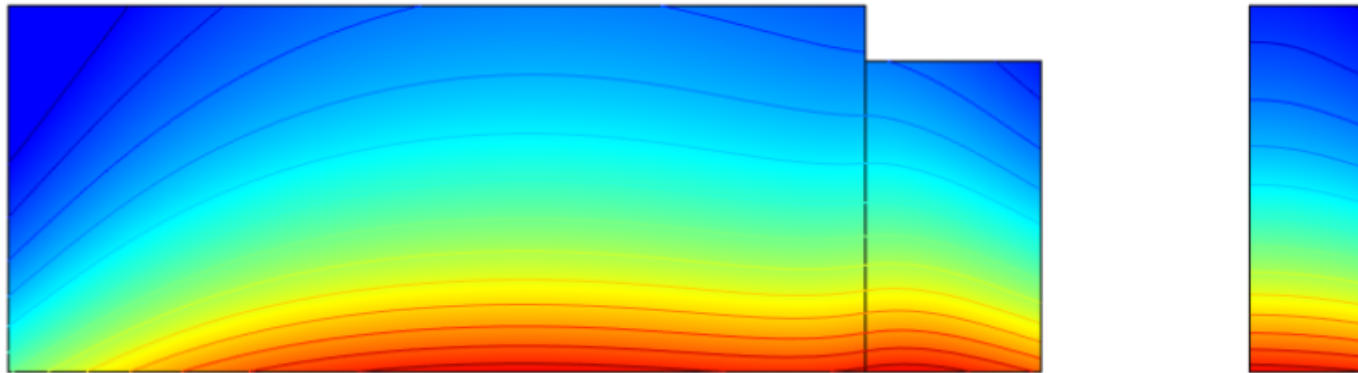
Maximum field = 20.4 T; contours at 1.5 T and integer values from 1 T through 20 T

Hoop Strain σ_{hoop} in Magnet of Copper Hollow Conductor



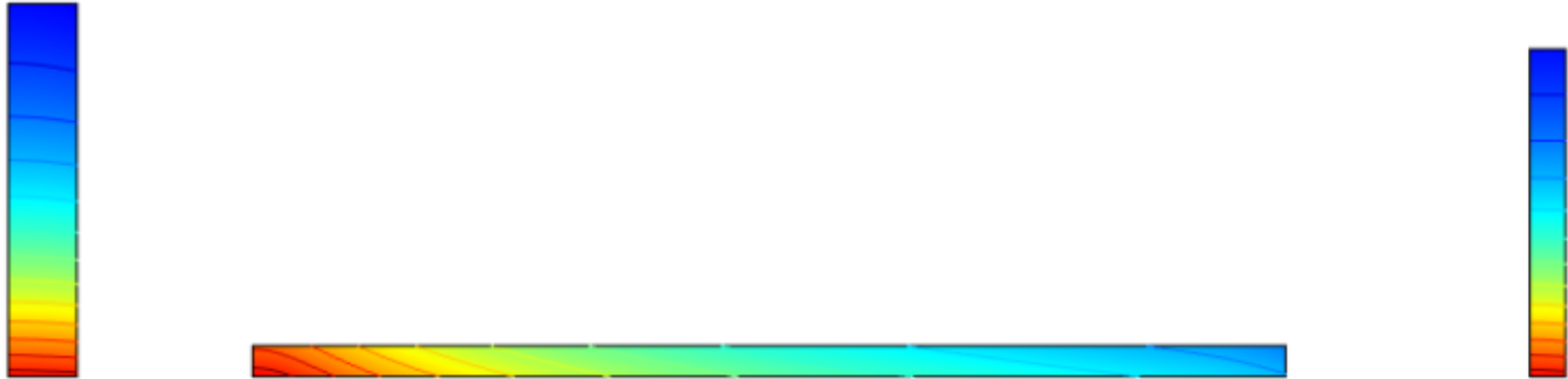
700-MPa coil banding limits σ_{hoop} in each coil to 0.35%; contour interval = 0.02%.

σ_{hoop} in Copper & Nb₃Sn Magnets (Most-Upstream Cryostat)



Maximum hoop strain in each coil is 0.35%; contour interval = 0.02%.

σ_{hoop} in Coils of Cryostat #2 (NbTi Conductor)



Maximum hoop strain in each coil is 0.35%; contour interval = 0.02%.

σ_{hoop} in in Coils of Cryostat #3 (NbTi Conductor)



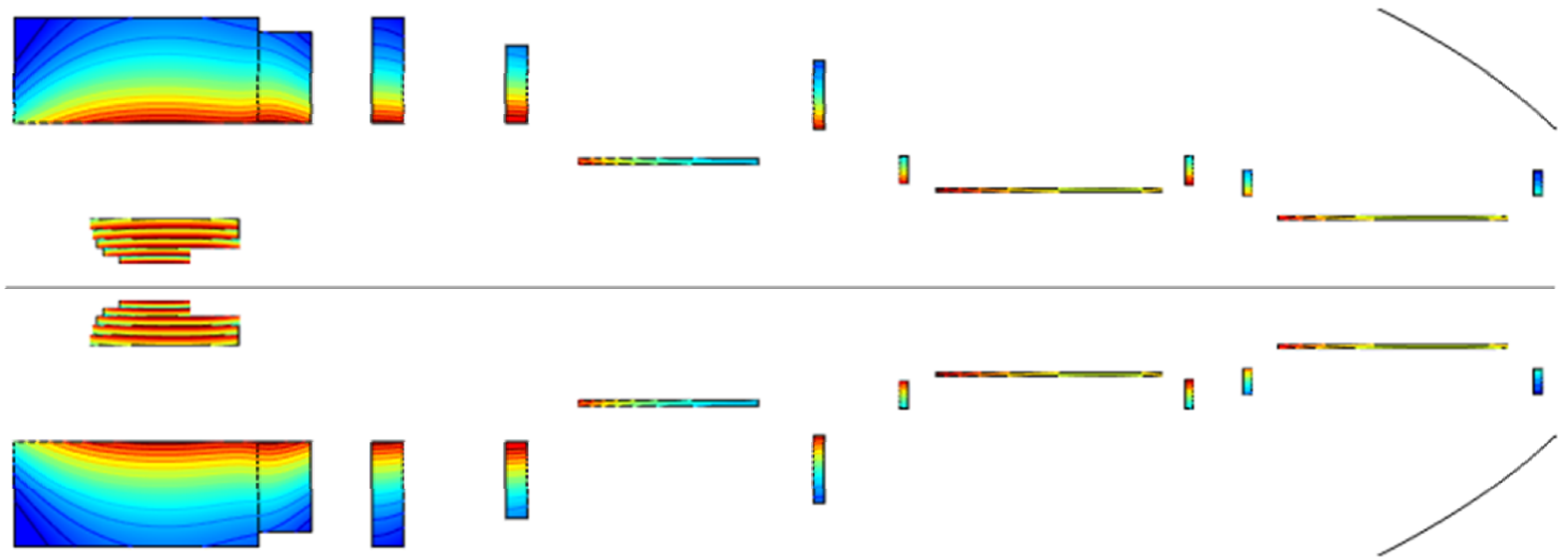
Maximum hoop strain in each coil is 0.35%.

σ_{hoop} in Coils of Cryostat #4 (NbTi Conductor)



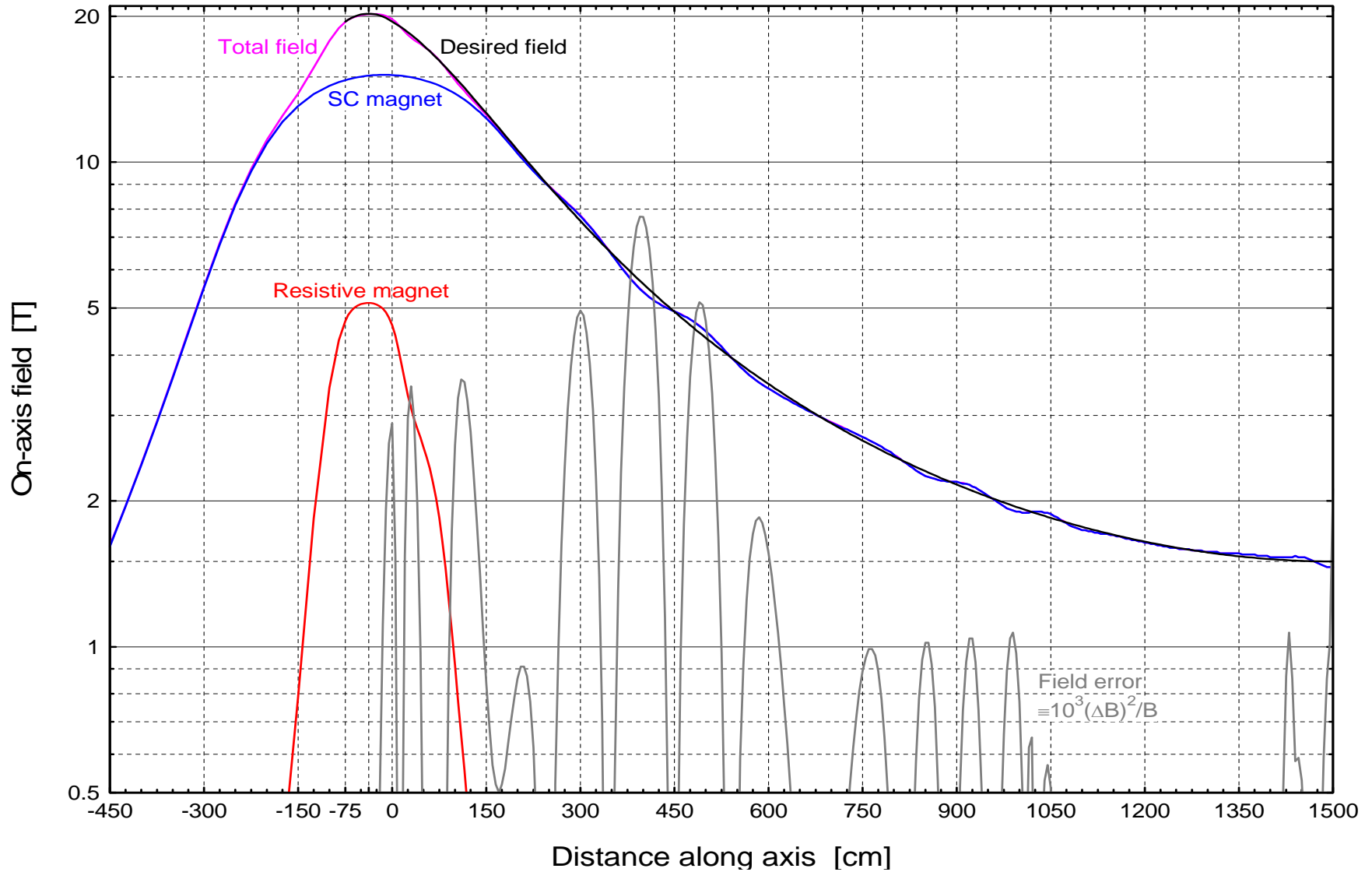
Maximum hoop strain in two upstream coils = 0.35%; max. (σ_{hoop}) in downstream coil also is 0.35% if one adds an identical set of coils downstream.

Target Magnet “DS120j5”: Optimized I.R. of Flanking Coils



I.R.'s of coils in cryostats #2-#4 are [120, 90, 116] cm, [76, 70, 75] cm & [67, 50, 67] cm.

On-Axis Field Profile B(z) of Target Magnet IDS120j5



Maximum field error is nearly 30% less than in design IDS120j.